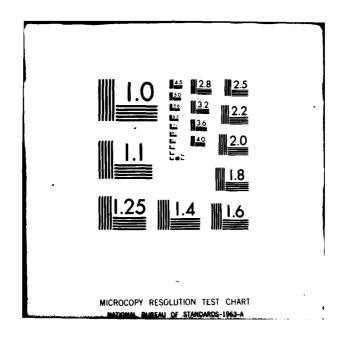
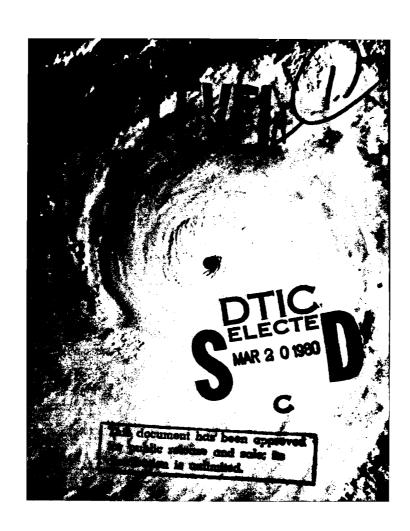
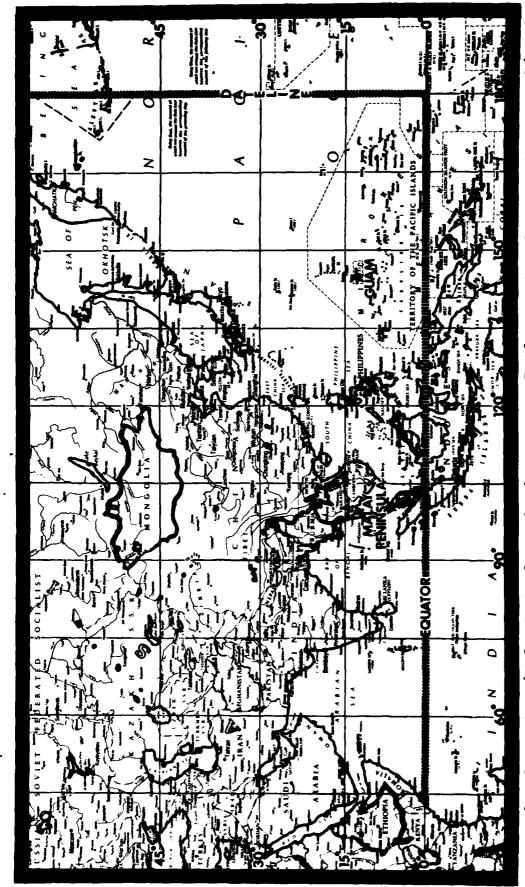
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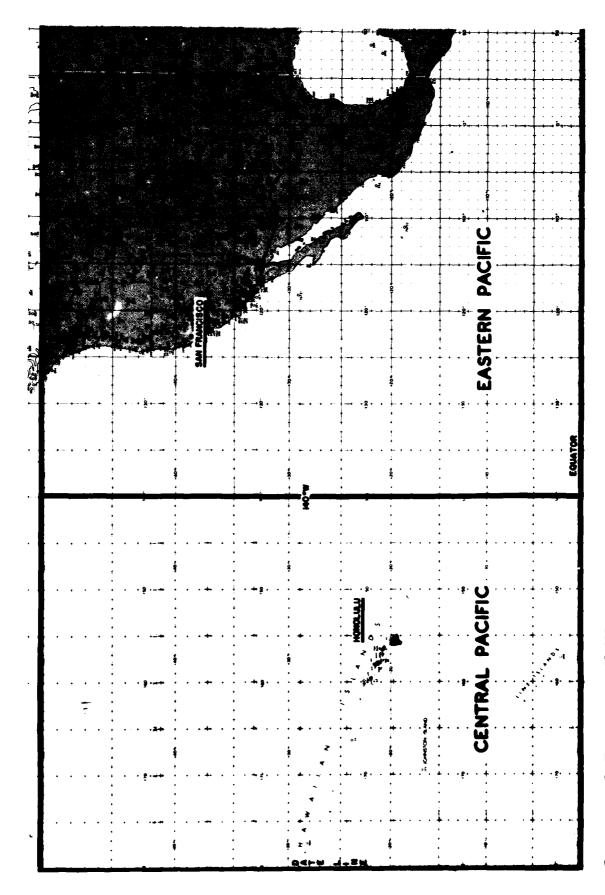




Indian Ocean Area (Malay Peninsula to Africa)

Pacific Area (Dateline to Malay Peninsula)

AREA OF RESPONSIBILITY - JOINT TYPHOON WARNING CENTER, GUAM



Areas of Responsibility - Central and Eastern Pacific Hurricane Centers

# **DISCLAIMER NOTICE**

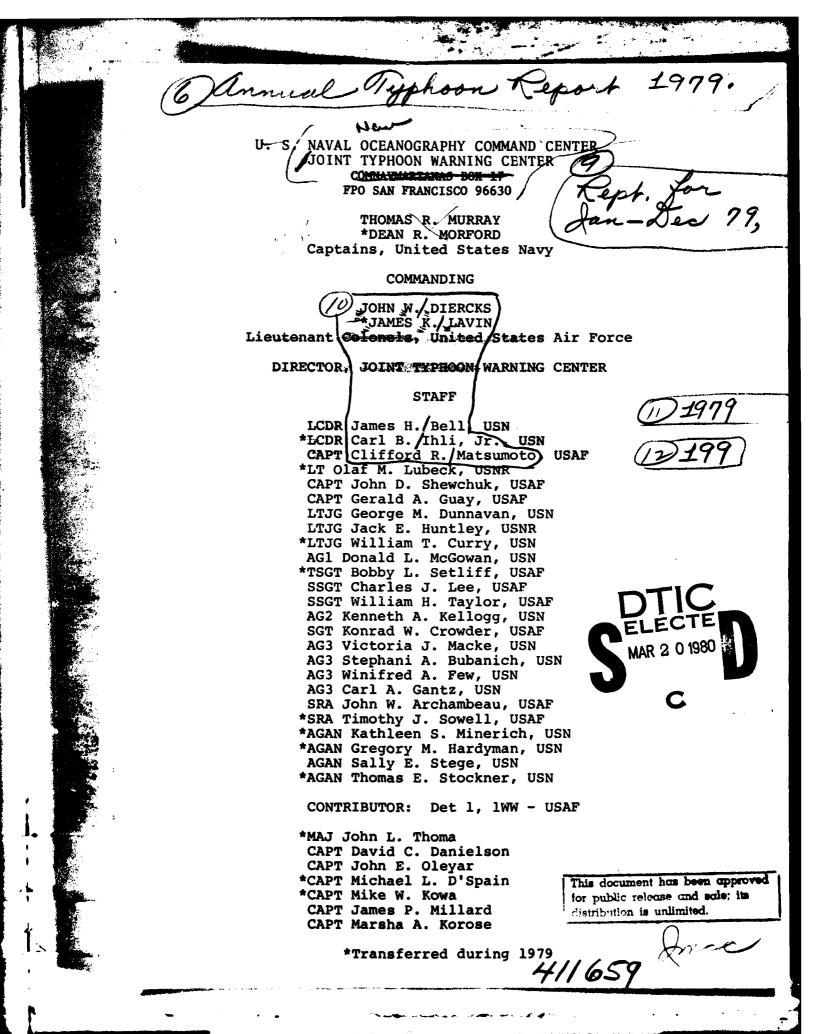
THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DTIC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

CORRECTIONS TO ANNEX B - for 1978 and 79 Annual Typhoon Reports (ATR)

1. The following tropical cyclones have aircraft fix data (eye characteristics) listed incorrectly:

1978 ATR	<u> 1979</u>	ATF
RITA	<b>V</b> E	RA
VIOLA	TI:	P
	OW	EN

2. The diameters of circular and concentric eye walls are incorrectly listed under the EYE ORIENTATION column. (Only elliptical eye walls have an orientation specified. These are specified correctly.) The misplaced diameters must be divided by 10 to obtain the correct figure and located in the EYE DIAMETER column.



FRONT COVER: Super Typhoon Tip near maximum intensity of 160 kt (82 m/sec), 11 October 1979, 21272. The minimum sea-level pressure was 870 mb and the associated circulation pattern was 1200 nm (2222 km) in diameter at that time. Details on Tip can be found on page 72. (DMSP imagery)

### **FOREWORD**

The Annual Typhoon Report is prepared by the staff of the Joint Typhoon Warning Center (JTWC) Two is a combined USAF/USN entity operating under the command of the U. S. Naval Oceanography Command Or the Guam., The senior Air Force Officer assigned is designated as Director, JTWC and is re-sponsible to the Commanding Officer, U. S. Naval Oceanography Command Center, Guam for the operation of the JTWC. The senior Naval Officer of the JTWC is designated as the Deputy Director/Operations Officer. TWC was established by CINCPACFLT message 280208Z April 1959 when directed by CINCPAC message 230233Z April 1959. Its operation is guided by the CINCPACINST 3140.1 (series).

- The Naval Oceanography Command Center/
  Joint Typhoon Warning Center, Guam has the
  responsibility to:

  1) Provide continuous meteorological watch of all tropical activity north of the equator, west of the Date Line, and east of the African coast (JTWC area of responsibility) for potential tropical responsibility) for potential tropical cyclone development.
  - 2) Provide warnings for all significant tropical cyclones in the assigned area of responsibility.
  - 3) Determine tropical cyclone reconnaissance requirements and assign priorities.

(4) Conduct an annual post-analysis of all tropical cyclones occurring within the JTWC area of responsibility; and prepare an Annual Typhoon Report for issuance to interested agencies.

(5) Conduct tropical cyclone fore-casting and detection research as practicable.

In the event of incapacitation of the JTWC, the alternate (AJTWC) assumes the responsibility for issuing warnings. The U. S. Naval Western Oceanography Center, Pearl Harbor, Hawaii is designated as the AJTWC. Assistance in determining tropical cyclone reconnaissance requirements and in obtaining reconnaissance data is provided by Detachment 4, 1st Weather Wing, Hickam AFB, Hawaii.

The meteorological services of the United States are planning to implement the metric system of measurement over the next few years. Some civilian and military rew years. Some civilian and military agencies have started the education program by showing the metric equivalents to current units of measure. This Annual Typhoon Report includes metric equivalents to most

Unless otherwise stated, all satellite data used in this ATR are Air Force Air Weather Service DMSP Data as acquired by OL-C, 27CS personnel and analyzed by Det 1, 1WW personnel colocated with the JTWC at Nimitz Hill, Guam.

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### CHAPTER I - OPERATIONAL PROCEDURES

### 1. GENERAL

Routine services provided by the Joint Typhoon Warning Center (JTWC) include the following: (1) Significant Tropical Weather Advisories issued daily describing all tropical disturbances and their potential for further development; (2) Tropical Cyclone Formation Alerts issued whenever interpre tation of satellite and synoptic data indicates likely formation of a significant tropical cyclone; (3) Tropical Cyclone Warn-ings issued four times daily for significant replical cyclones; and (4) Prognostic Reasoning messages issued twice daily for tropical storms and typhoons in the Pacific area.

JTWC responds to changing requirements of activities serviced. Therefore, contents of routine services are subject to change from year to year usually as a result of deliberations at the Tropical Cyclone Conference.

### 2. DATA SOURCES

#### a. COMPUTER PRODUCTS:

The Naval Oceanography Command Center (NAVOCEANCOMCEN) Guam provides computerized meteorological/oceanographic products for JTWC. In addition, the standard array of synoptic-scale computer analyses and prognostic charts are available from the Fleet Numerical Oceanography Center (FLENUMOCEANCEN) at Monterey, California. With the installation of the Naval Environmental Display Stations (NEDS) during 1978, JTWC now has very timely access to necessary FLENUMOCEANCEN products and is thereby able to more efficiently and effectively use this information.

### b. CONVENTIONAL DATA:

Conventional meteorological data are defined as surface and upper-air observations from island, ship and land stations plus weather observations from commercial and weather observations from commercial and military aircraft (AIREPS). Conventional data charts are prepared daily at 00002 and 12002 for the surface, 700 mb, and 500 mb levels. A chart of upper-air data is prepared which utilizes 200 mb rawinsonde data and AIREPS above 29,000 ft within 6 hours of the 0000Z and 1200Z synoptic times.

### c. AIRCRAFT RECONNAISSANCE:

Aircraft weather reconnaissance data are invaluable in the positioning of centers of developing systems and essential for the accurate determination of the eye/center, maximum intensity, minimum sea-level pressure and radius of significant winds exhibited by tropical cyclones. Winds and pressure-height data at the 500 and/or 400 mb level, provided by reconnaissance aircraft while enroute to, or returning from, fix missions, are also used to supplement the sparse data in the tropics and subtropics. These data are plotted on large-scale sectional charts for each mission flown. A comprehensive discussion of aircraft weather reconnaissance is presented in Chapter II.

#### d. SATELLITE RECONNAISSANCE:

Meteorological satellite data from the Defense Meteorological Satellite Program (DMSP) and the National Oceanic and Atmospheric Administration played a major role in the early detection and tracking of tropical cyclones in 1979. A discussion of this role is presented in Chapter II.

#### e. RADAR RECONNAISSANCE:

During 1979, as in recent years, land radar coverage was utilized extensively when available. Once a storm moved within the range of a land radar site, reports were usually received hourly. Use of radar during 1979 is discussed in Chapter II.

#### 3. COMMUNICATIONS

- a. JTWC currently has access to three primary communications circuits:
- (1) The Automated Digital Network (AUTODIN) is used for dissemination of warnings and other related bulletins to Department of Defense installations. These messages are relayed for further trans-mission over U. S. Navy Fleet Broadcasts, U. S. Coast Guard CW (continuous wave morse code) and voice communications. Inbound message traffic for JTWC is received via AUTODIN addressed to NAVOCEANCOMCEN GUAM.
- (2) The Air Force Automated Weather Network (AWN) provides weather data to JTWC through a dedicated circuit from the automated digital weather switch (ADWS) at Clark AB, R.P. The ADWS selects and routes the large volume of meteorological reports necessary to satisfy JTWC requirements for the right data at the right time. Weather bulletins prepared by JTWC are inserted into the AWN circuit by the Nimitz Hill Naval Tele-communications Center (NTCC) of the Naval Communications Area Master Station Western Pacific.
- (3) The Naval Environmental Data Network (NEDN) provides the communications link with the computers at FLENUMOCEANCEN. JTWC is able to both receive environmental data from FLENUMOCEANCEN and access the computers directly to run various programs.
- Besides providing forecasters with the ability to rapidly access computer products, the NEDS has recently become the AUTODIN and AWN message tapes can now be prepared by JTWC personnel for insertion into the AUTODIN and AWN circuits by the NTCC. The NEDS is also used by the TDO to request forecast aids which are processed by the computers at Monterey and transmitted back to the TDO over the NEDN circuit.

### 4. ANALYSES

A composite surface/gradient level (3000 ft) manual analysis is accomplished on the 00002 and 12002 conventional data. Analysis of the wind field using streamlines is stressed for tropical and subtropical

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regions. Analysis of the pressure field is stressed for higher latitudes and in the vicinity of tropical cyclones.

Manual analysis of the 500 mb level is accomplished on the 0000Z and 1200Z data. Although the analysis of the 500 mb height field is stressed, knowledge of the wind field to more clearly delineate steering currents is equally important.

A composite upper-tropospheric manual analysis, utilizing rawinsonde data from 300 mb through 100 mb, wind directions extracted from satellite data by Det 1, 1WW and AIREPS (plus or minus 6 hours) at or above 29,000 feet is accomplished on 0000Z and 1200Z data daily. Wind and height data are used to arrive at a representative analysis of tropical cyclone outflow patterns, of steering currents and of areas that may indicate tropical cyclone intensity change. All charts are hand plotted over areas of tropical cyclone activity to provide all available data as soon as possible to the TDO. These charts are augmented by the computer-plotted charts for the final analyses.

Additional sectional charts at intermediate synoptic times and auxiliary charts such as checkerboard diagrams and pressure-change charts are also analyzed during periods of significant tropical cyclone activity.

#### 5. FORECAST AIDS

#### a. CLIMATOLOGY:

Climatological publications utilized during the 1979 typhoon season include previous JTWC Annual Typhoon Reports and climatic publications from local sources, Naval Environmental Prediction Research Facility, Naval Postgraduate School, Air Weather Service, First Weather Wing and Chanute Technical Training Center. Publications from other Air Force and Navy activities, various universities and foreign countries are also used by the JTWC.

### b. OBJECTIVE TECHNIQUES:

The following objective techniques were employed in tropical cyclone forecasting during 1979. A description of these techniques is presented in Chapter IV.

- (1) TYFN75 (Analog)
- (2) MOHATT (Steering)
- (3) 12 HR EXTRAPOLATION
- (4) CLIMATOLOGY
- (5) HPAC (Combined extrapolation and climatology)
- (6) TROPICAL CYCLONE MODEL (Dynamic)
- (7) INJAH74 (Analog)
- (8) CYCLOPS (Steering)
- (9) TYAN78 (Analog)

### 6. FORECASTING PROCEDURES

#### a. INITIALIZATION:

In the preparation of each warning, the actual surface location (fix) of the tropical cyclone eye/center just prior to (within three hours of) warning time is of prime importance. JTWC uses the Selective Reconnaissance Program (SRP) to levy an optimum mix of aircraft, satellite and radar resources to obtain fix information. When tropical cyclones are either poorly defined or the actual surface location cannot be determined, or when conflicting fix information is received, the "best estimate" of the surface location is subjectively determined from the analysis of all available data. If fix data are not available due to reconnaissance platform malfunctions or communication problems, synoptic data or extrapolation from previous fixes are used. The initial forecast (warning time) position is then obtained by extrapolation using the current fix and a "best track" of the cyclone movement to date.

#### b. TRACK FORECASTING:

An initial forecast track is developed based on the previous forecast and the objective techniques. This initial track is subjectively modified based on the following:

- (1) The prospects for recurvature are evaluated. This evaluation is based primarily on present and forecast position and amplitude of middle tropospheric midlatitude troughs from the latest 500 mb analysis and numerical prognoses.
- (2) Determination of steering level is partly influenced by maturity and vertical extent of the system. For mature cyclones located south of the 500 mb subtropical ridge, forecast changes in speed of movement are closely correlated with forecast changes in the intensity of the ridge. When steering currents are very weak, the tendency for cyclones to move northward due to their internal forces is an important consideration.
- (3) The proximity of the tropical cyclone to other tropical cyclones is evaluated to determine if there is a possibility of Fujiwhara interaction.
- (4) Over the 12- to 72-hr forecast spectrum, speed of movement during the early time frame is biased toward persistence (12-hr extrapolation) while that near the end of the time frame is biased towards objective techniques and climatology.
- (5) A final check is made against climatology to determine the likelihood of the forecast track. If the forecast deviates greatly from climatology, the forecast rationale is reappraised and the track adjusted as necessary.

#### c. INTENSITY FORECASTING:

In forecasting intensity, heavy reliance is placed on aircraft reconnaissance reports, the Dvorak satellite interpretation model, wind and pressure data from ships and land stations in the vicinity of the cyclone, and the objective techniques. Additional considerations are the position and intensity of the tropical upper-tropospheric trough (TUTT), extent and intensity of upper-level outflow, sea-surface temperature, terrain influences, speed of movement and proximity to an extratropical environment.

### 7. WARNINGS

Tropical cyclone warnings are issued when a definite closed circulation is evident and maximum sustained wind speeds are forecast to increase to 34 or more knots within 48 hours, or the cyclone is in such a position that life or property may be endangered within 72 hours. Warnings are also issued in other situations if it is determined that there is a need to alert military and civil interests to conditions which may become hazardous in a short period of time. Each tropical cyclone warning is numbered sequentially and includes the initial warning time, eye/center position, intensity, the radial extent of 30, 50 and 100 knot surface winds (when applicable), the levied reconnaissance platform used, the instantaneous speed and direction of movement of the cyclone's surface center at warning time and the forecast information. The forecast intervals for all tropical cyclones, regardless of intensity, are 12-, 24-, 48- and 72-hr. Warnings within the of 0000Z, 0600Z, 1200Z and 1800Z with the constraint that two consecutive warnings may not be more than seven hours apart. Warnings in the JTWC Indian Ocean area are issued within two hours of 0200Z, 0800Z, 1400Z and 2000Z with the constraint that two consecu-2000Z with the constraint that two consecutive warnings may not be more than seven hours apart. These variable warning times allow for maximum use of all available reconnaissance platforms and more effectively distribute the workload in multiple cyclone situations. If warnings are discontinued and a cyclone reintensifies, warnings are numbered consecutively from the last warning issued. Warning forecast positions are verified against the corresponding postanalysis "best track" positions. A summary of the verification results for 1979 is presented in Chapter IV.

#### 8. PROGNOSTIC REASONING MESSAGE

In the Pacific Area, prognostic reasoning messages are transmitted based on the 0000Z and 1200Z warnings or whenever the previous reasoning is no longer valid. This plain language message is intended to provide users with the reasoning behind the latest JTWC forecast. Prognostic reasoning messages are not prepared for tropical depressions nor for cyclones in the Indian Ocean area.

For the 1979 season, JTWC included confidence statements for the 24 and 48-hour forecasts. The confidence values were percentage probabilities that the 24-hour forecast position error would be less than 100 nm and less than 150 nm, respectively, and that the 48-hour error would be less than 200 nm and less than 300 nm, respectively. These probabilities were based on objective data from error analysis studies of past cyclones and were a function of latitude, longitude, storm intensity, organization and the number of western Pacific storms in existence.

Prognostic reasoning information applicable to all customers is provided in the remarks section of warnings when significant forecast changes are made or when deemed appropriate by the TDO.

### 9. SIGNIFICANT TROPICAL WEATHER ADVISORY

This plain language message, summarizing significant weather in the entire JTWC area of responsibility, is issued by 0600Z daily. It contains a detailed, non-technical description of all significant tropical disturbances and the JTWC evaluation of potential for significant tropical cyclone development within the 24-hour forecast period.

### 10. TROPICAL CYCLONE FORMATION ALERT

Alerts are issued whenever interpretation of satellite and other meteorological data indicates significant tropical cyclone formation is likely. These alerts will specify a valid period not to exceed 24 hours and must either be cancelled, reissued or superseded by a warning prior to expiration of the valid period.

### CHAPTER II RECONNAISSANCE AND FIXES

#### 1. GENERAL

The Joint Typhoon Warning Center depends on reconnaissance to provide necessary, accurate and timely meteorological information in support of each warning. JTWC relies primarily on three sources of reconnaissance: aircraft, satellite and radar. Optimum utilization of all available reconnaissance resources is obtained through use of the Selective Reconnaissance Program (SRP) whereby various factors are considered in selecting a specific reconnaissance platform for each warning. These factors include: cyclone location and intensity, reconnaissance platform capabilities and limitations, and the cyclone's threat to life/property afloat and ashore. A summary of reconnaissance fixes received during 1979 is included in Section 6.

#### 2. RECONNAISSANCE AVAILABILITY

#### a. Aircraft:

Aircraft weather reconnaissance is performed in the JTWC area of responsibility by the 54th Weather Reconnaissance Squadron (54 WRS). The squadron, presently equipped with six WC-130 aircraft, is located at Andersen Air Force Base, Guam. From July through October, augmentation by the 53rd WRS at Keesler Air Force Base, Mississippi brings the total number of available aircraft to nine. The JTWC reconnaissance requirements are provided daily throughout the year to the Tropical Cyclone Aircraft Reconnaissance Coordinator (TCARC). These requirements include area(s) to be investigated, tropical cyclone(s) to be fixed, fix times and forecast positions of fixes. The following priorities are utilized in acquiring meteorological data from aircraft, satellite and land-based radar in accordance with CINCPACINST 3140.1N:

- "(1) Investigative flights and vortex or center fixes for each scheduled warning in the Pacific area of responsibility. One aircraft fix per day of each cyclone of tropical storm or typhoon intensity is desirable.
- (2) Center or vortex fixes for each scheduled warning of tropical cyclones in the Indian Ocean Area of responsibility.
  - (3) Supplementary fixes.
  - (4) Synoptic data acquisition."

As in previous years, aircraft reconnaissance provided direct measurements of height, temperature, flight-level winds, sea level pressure, estimated surface winds (when observable) and numerous additional parameters. The meteorological data are gathered by the Aerial Reconnaissance Weather Officers

(ARWO) and dropsonde operators of Detachment 4, Hq AWS who flew with the 54th. These data provide the Typhoon Duty Officer (TDO) indications of changing cyclone characteristics, radius of cyclone associated winds, and present cyclone position and intensity. Another important aspect of this data is its availability for research in tropical cyclone analysis and forecasting. Aircraft reconnaissance will become even more important in years to come when high-resolution tropical cyclone dynamic steering programs will require a dense input of wind and temperature data.

#### b. Satellite

Satellite fixes from USAF ground sites and USN ships provide day and night coverage in the JTWC area of responsibility. Interpretation of this satellite imagery provides cyclone positions and estimates of storm intensities through the Dvorak technique (for daytime passes).

Detachment 1, 1st Weather Wing, which receives and processes DMSP data, is the primary fix site for the northwestern Pacific. DMSP fix positions received at JT:/C from the Air Force Global Weather Central (AFGWC), Offutt Air Force Base, Nebraska were the major source of satellite data for the Indian Ocean. GOES fixes were also provided by the National Environmental Satellite Service, Honolulu, Hawaii for tropical cyclones near the dateline.

### c. Radar

Land radar provides positioning data on well developed cyclones when in proximity (usually within 175 nm of the radar site) of the Republic of the Philippines, Taiwan, Hong Kong, Japan, the Republic of Korea, Kwajalein, and Guam.

### d. Synoptic

In 1979, the JTWC also determined tropical cyclone positions based on the analysis of the surface/gradient level synoptic data. These positions were helpful in situations where the vertical structure of the tropical cyclone was weak or accurate surface positions from aircraft were not available due to flight restrictions.

### 3. AIRCRAFT RECONNAISSANCE SUMMARY

During the 1979 tropical season, the JTWC levied 289 six-hourly vortex fixes and 52 investigative missions. In addition to the levied vortex fixes, 150 supplemental fixes were also obtained. The number of levied investigative missions has increased steadily over the past four years in response to JTWC's increased efforts to detect initial tropical cyclone development.

Of 1979's 28 tropical cyclones, investigative missions were not flown on four. The average vector error for all aircraft fixes received at the JTWC during 1979 was 13.0 nm (24.1 km).

Reconnaissance effectiveness is summarized in Table 2-1 using the criteria as set forth in CINCPACINST 3140.1N.

TABLE 2-1. AIRCRA	FT RECONNAIS	SANCE EFFE	CTIVENESS
EFFECTIVENESS		ER OF D FIXES	PERCENT
COMPLETED ON TIME EARLY LATE MISSED		58 2 15 14 39	89.3 0.7 5.2 4.8 100.0
FEAIE	D VS. MISSED	FIXES	
	LEVIED	MISSED	PERCENT
AVERAGE 1965-1970 1971 1972 1973 1974 1975 1976 1977 1978 1978	507 802 624 227 358 217 317 203 290 289	10 61 126 13 30 7 11 3 2	2.0 7.6 20.2 5.7 8.4 3.2 3.5 1.5 0.7 4.8

### 4. SATELLITE RECONNAISSANCE SUMMARY

The Air Force provides satellite reconnaissance support to JTWC using imagery data from DMSP polar orbiting spacecraft. from similar NOAA spacecraft (TIROS-N/NOAA-6) were not available to the tactical sites of the network but could be processed on a backup basis by the Air Force Global Weather Central (AFGWC).

The DMSP network consists of both tactical and centralized facilities. DMSP sites are located at Nimitz Hill, Guam; Clark AB, Philippines; Kadena AB, Japan; Osan AB, Korea; and Hickam AFB, Hawaii. These sites provide a combined coverage that blankets the JTWC area of responsibility in the western Pacific from near the dateline westward to the Malay Peninsula.

The centralized member of the DMSP network is the Air Force Global Weather Central located at Offutt AFB, Nebraska. AFGWC receives worldwide satellite imagery coverage four times daily from two DMSP spacecraft. In addition, AFGWC has the capability to process either TIROS-N or NOAA-6 should one of the primary DMSP space-craft fail. Imagery taken over the JTWC area of responsibility is recorded on board

the spacecraft and later downlinked to AFGWC via command/readout sites and communications satellites. With their coverage, AFGMC is able to fix a storm anywhere within the JTWC area of responsibility. As the only site in the network that receives coverage over the entire Indian Ocean, AFGWC has the primary responsibility for satellite reconnaissance in this area as well as a small portion of the central Pacific near the dateline. On occasion, AFGWC is tasked to provide storm positions in the western Pacific as backup to the tactical sites.

The thread that ties the network The thread that thes the network together is Det 1, lWW colocated with JTWC atop Nimitz Hill, Guam. Based on available satellite coverage, Det 1 coordinates satellite reconnaissance requirements with JTWC and tasks the individual DMSP sites to provide the necessary storm fixes. The tasking concept is to fix every storm or tropical disturbance (alert area) once from each satellite pass over the area of the When a satellite position is required as the basis for a warning (levy), a dualsite tasking concept is applied. Under concept, two sites are tasked to fix the Under this storm off the same satellite pass. This provides the necessary redundancy to vir tually guarantee JTWC a successful satellite fix of the storm. Using the dual-site tasking concept, the satellite reconnaissance network was able to meet 98 percent of JTWC's satellite fix requirements. Dual-site tasking is not available over the Indian Ocean since only AFGWC receives the satellite Dual-site taskcoverage for most of that area.

The network provides JTWC with several products and services. The main service is one of surveillance. With the exception of Osan, each site reviews its daily coverage for any indications of development. If an area shows indications of development, JTWC is notified. Once JTWC issues either an alert or warning, the network is tasked to provide three products: storm positions, storm intensity estimates, and 24-hour storm intensity forecasts. Satellite storm positions are assigned position code numbers (PCN) depending on the availability of geography for precise gridding and the degree of organization of the storm's circulation center (Table 2-2). During 1979, the network provided JTWC with 1970 satellite fixes of tropical cyclones in warning status. comparison of those fixes made on numbered tropical cyclones with their corresponding JTWC best track positions is shown in Table

TABLE 2-2. POSITION CODE NUMBERS

METHOD OF CENTER DETERMINATION/GRIDDING

- EYE/GEOGRAPHY
- EYE/EPHEMERIS

- WELL DEFINED CC/GEOGRAPHY
  WELL DEFINED CC/EPHEMERIS
  POORLY DEFINED CC/GEOGRAPHY
  POORLY DEFINED CC/EPHEMERIS

CC=Circulation Center

TABLE 2-3. MEAN DEVIATIONS (NM) OF DMSP DERIVED TROPICAL CYCLONE POSITIONS FROM JTWC BEST TRACK POSITIONS.

NUMBER OF CASES SHOWN IN PARENTHESIS.

PCN	WESTPAC 1974-1978 AVERAGE (ALL SITES)	WESTPAC 1979 (ALL SITES)	INDIAN OCEAN 1979 (ALL SITES)
1	13.3 (178)	14.4 (268)	13.5 ( 7)
2	18.5 (68)	17.9 (61)	23.1 (7)
3	21.2 (270)	18.6 (341)	23.4 (16)
4	25.6 (101)	20.5 ( 70)	18.0 (8)
5	37.1 (368)	37.8 (605)	34.1 (22)
6	47.2 (190)	43.3 (232)	42.2 (66)
1&2	14.8 (246)	15.0 (329)	18.3 (14)
364	22.0 (371)	18.9 (411)	21.6 (24)
546	40.6 (558)	39.4 (837)	40.2 (88)

2-3. Estimates of the storm's current and 24-hour forecast intensity are made once each day by applying the Dvorak technique (NOAA Technical Memorandum NESS 45 as revised) to daylight visual data. Satellite derived storm positions, intensity estimates, and forecasts constitute the satellite portion of the JTWC forecast data base.

The availability of satellite data varied during the year. At the start, the network had access to three DMSP spacecraft: F-1 (late-morning), F-2 (mid-morning), and F-3 (sunrise). In June, a fourth DMSP spacecraft, F-4, was launched into a late morning orbit. The network had access to these four spacecraft until mid-September when F-1 failed. Three months later, in early December, F-3 failed reducing the active DMSP fleet to only two spacecraft with similar mid- to late-morning coverages. The network was able to partially compensate for this loss by depending on AFGWC to provide fixes for the entire network based on its unique ability to process TIROS-N as a replacement for F-3. Therefore, the 1979 season ended with available satellite coverage at its lowest point for the entire year.

Besides the network provided fixes, JTWC also receives satellite-derived storm positions from several secondary sources. These include: U.S. Navy ships equipped for satellite direct readout; the National Environmental Satellite Service using NOAA and GOES data; and the Naval Polar Oceanography Center, Suitland, Maryland using stored DMSP and NOAA data. Fixes from these secondary sources are not included in the network statistics.

### 5. RADAR RECONNAISSANCE SUMMARY

Sixteen of the 28 significant tropical cyclones occurring over the western North Pacific during 1979 passed within range of land based radars with sufficient cloud pattern organization to be fixed. The hourly and oftentimes, half-hourly land radar fixes that were obtained and transmitted to JTMC totaled 1143.

The WMO radar code defines three categories of accuracy: good (within 10 km (5.4 nm)), fair (within 10-30 km (5.4-16.2 nm)) and poor (within 30-50 km (16.2-27 nm)).

This year, 1139 radar fixes were coded in this manner; 25% were good, 29% fair and 46% poor. Compared to the JTWC best track, the mean vector deviation for land radar sites was 15 nm (28 km).

Of the 16 tropical cyclones which were monitored with land radar, 11 were typhoons: Alice, Cecil, Ellis, Hope, Irving, Judy, Mac, Owen, Sarah, Tip and Vera. These 11 typhoons accounted for 898 of all radar fixes received for this season. Excellent support through timely and accurate radar fix positioning allowed JTWC to track and forecast tropical cyclone movement through even the most difficult and erratic tracks.

The 54 WRS made four radar center fixes from their WC-130 aircraft when actual penetration was restricted. One ship radar center fix was received on Typhoon Bess. No radar fixes were received on Indian Ocean tropical cyclones.

### 6. TROPICAL CYCLONE FIX DATA

A total of 3318 fixes on 28 northwest Pacific tropical cylones and 166 fixes on 7 northern Indian Ocean tropical cyclones were received at JTWC. Table 2-4, Fix Platform Summary, delineates the number of fixes per platform for each individual tropical cyclone. Season totals and percentages are also indicated.

Annex B lists individual fixes sequentially for each tropical cyclone. Fix data is divided into four categories: Satellite, Aircraft, Radar and Synoptic. Those fixes labeled with an asterisk (\*) were determined to be unrepresentative of the surface center and were not used in determining the best tracks. Within each category, the first three columns are as follows:

FIX NO. - Sequential fix number

TIME (z) - GMT time in day, hours and minutes

FIX POSITION - Latitude and longitude to the nearest tenth of a degree

Depending upon the category, the remainder of the format varies as follows:

TABLE 2-4. FIX SUMMARY FOR 1979

	FIX SUPPARY									
	AIRCRAFT	DMSP	TIROS-N	<u>G0ES3</u>	RADAR	SYNOPTIC	TOTAL			
WESTERN PACIFIC										
TY ALICE TY BESS TY CECIL TS DOT TD 05	43 17 29 7	80 47 87 71 20	• • •	5 - - -	42 1* 51 12	- - - 3	170 65 167 93 33			
TY ELLIS TS FAYE TD 08 ST HOPE	12 14 1 22	66 48 29 78	- - -	:	11 14 - - 44	3 2 7 5 7 1	99 67 37 145			
TS GORDON TD 11 TY IRVING ST JUDY TD 14	8 6 25 26 3 5	40 33 124 140 23		:	25 - 148** 177 -	- 2 - 2	73 41 297 345 28	ļ		
TS KEN TY LOLA TY MAC TS NANCY TY OWEN	17 14 - 34	41 63 86 33 87	- - -	:	73 55*** 312	2 - - - 15 8	119 80 155 48 441			
TS PAMELA TS ROGER TY SARAH ST TIP ST VERA	5 6 13 59 14	9 32 112 99 54	-	:	5 5 109 60***	6	14 44 134 267 137			
TS MAYNE TD 26 TY ABBY TS BEN	11 2 40 4	44 11 66 20	7 2	-	7	1 1 3 -	56 14 116 33			
TOTAL	437	1643	9	5	1146	78	3318			
% OF TOTAL NO. OF FIXES	13.1	49.5	.3	.2	34.6	2.3	100	ļ		
INDIAN OCEAN		DMSP	TIROS-N			SYNOPTIC	TOTAL			
TC 17-79 TC 18-79 TC 22-79 TC 23-79 TC 24-79 TC 25-79 TC 25-79		28 16 8 30 19 17 20	5 4 2 6 3			5 2 1 -	33 25 12 37 22 17	;		
TOTAL	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	138	20			8	166			
% OF TOTAL NO. OF FIXES		83	13			4	100			

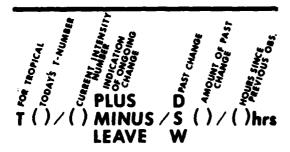
SHIP RADAR FIX INCLUDES TWO ACFT RADAR FIXES INCLUDES ONE ACFT RADAR FIX

### a. Satellite

(1) ACCRY - Position Code Number (PCN) (see Sec. 5) or Confidence (CONF) number (see table 2-5) is listed depending on method used to determine the fix position.

OF DV	DENCE (CONF) DRAK T NUMBER BILITY AREA (	AND RADIUS	
TROPICAL CYCLONE INTENSITY	CONF (1)	CONF (2)	CONF (3)
T1.5	60	120	170
T2.0	60	120	170
T2.5	60	120	170
T3.0	50	100	150
T3.5	45	90	140
T4.0	45	90	140
T4.5	45	90	140
T5.0	40	90	130
T5.5	40	80	130
T6.0	40	80	130
T6.5	30	70	120
T7.0	30	70	120
17.5	30	60	100
T8.0	30	60	100

(2) DVORAK CODE - Intensity evaluation and trend utilizing DMSP visual satellite data. (For specifics refer to NOAA TM; NESS-45)



EXAMPLE: T5/6 MINUS/W1.5/24hrs.

- (3) SAT Specific satellite used for fix position (DMSP 35, 36, 37 or 39, TIROS-N or Geostationary Operational Environmental Satellite (GOES, 135W)).
- (4) COMMENTS For explanation of abbreviations see Appendix.
- (5) SITE ICAO call sign of the specific satellite tracking station.

### b. Aircraft

(1) FLT LVL - The constant pressure surface level, in mb, maintained during the penetration. 700 mb is the normal level flown in developed cyclones due to turbulence factors with low-level missions flown at 1500 ft.

- (2) 700 MB HGT Minimum height of the 700 mb pressure surface within the vortex recorded in meters.
- (3) OBS MSLP If the surface center can be visually detected (e.g., in the eye), the minimum sea level pressure is obtained by a dropsonde released above the surface vortex center. If the fix is made at the 1500-foot level, the sea level pressure is extrapolated from that level.
- (4) MAX-SPC-WND The maximum surface wind (knots) is an estimate made by the ARMO based on sea state. This observation is limited to the region of the flight path, and may not be representative of the entire cyclone. Availability of data is also dependent upon the absence of undercast conditions and the presence of adequate illumination. The positions of the maximum flight level wind and the maximum observed surface wind do not necessarily coincide.
- (knots) at flight level is measured by the AN/APN 147 doppler radar system aboard the WC-130 aircraft. Values entered in this category represent the maximum wind measured prior to obtaining a scheduled fix. This measurement may not represent the maximum flight level wind associated with the tropical cyclone because the aircraft only samples those portions of the tropical cyclone along the flight path. In many instances the flight path may be through the weak sector of the cyclone. In areas of heavy rainfall, the doppler radar may track energy reflected from precipitation rather than from the sea surface; thus preventing accurate wind speed measurement. In obvious cases, such erroneous wind data will not be reported. In addition, the doppler radar system on the WC-130 restricts wind measurements to drift angles less than or equal to 27 degrees if the wind is normal to the aircraft heading.
- (6) ACCRY Fix position accuracy. Both navigational (OMEGA and LORAN) and meteorological (by the ARWO) estimates are given in nautical miles.
- (7) EYE SHAPE Geometrical representation of the eye based on the aircraft radar presentation. Reported only if center is 50% or more surrounded by wall cloud.
- (8) EYE DIAM/ORIENTATION Diameter of the eye in nautical miles. In case of an elliptical eye, the lengths of the major and minor axes and the orientation of the major axis are respectively listed.

### c. Radar

- (1) RADAR Specific type of platform utilized for fix (land radar site, aircraft or ship).
- (2) ACCRY Accuracy of fix position (good, fair or poor) as given in the MMO ground radar weather observation code (FM20-V).
- (3) EYE SHAPE Geometrical representation of the eye given in plain language (circular, elliptical, etc.).

- (4) EYE DIAM Diameter of eye given in nautical miles.
- (5) RADOB CODE Taken directly from WHO ground weather radar observation code PM20-V. First group specifies the vortex parameters, while the second group describes the movement of the vortex center.
- (6) RADAR POSITION Latitude and longitude of tracking station given in tenths of a degree.
- (7) SITE WMO station number of the specific tracking station.

### d. Synoptic

- (1) INTENSITY ESTIMATE TDO's analysis of low-level synoptic data to determine a cyclone's maximum sustained surface wind (knots).
- (2) MEAREST DATA Accuracy of fix based on distance (nautical miles) from the fix position to the nearest synoptic report or to the average distance of reports in data sparse cases.

### CHAPTER III SUMMARY OF TROPICAL CYCLONES

March Tipe 1

## 1. WESTERN NORTH PACIFIC TROPICAL CYCLONES

During 1979, the western North Pacific experienced a below normal year of tropical cyclone activity with a total of 28 cyclones (Table 3-1). By comparison, 1978 was a near normal year with 32 cyclones and 1977 was a near record low year with a total of 21 cyclones. Five significant tropical cyclones never developed beyond tropical depression (TD) stage, and nine developed into tropical storms (TS). Of the 14 cyclones that devel-

oped to typhoon (TY) stage, only 4 reached the 130 kt (67 m/sec) intensity necessary to be classified as a super typhoon (ST). This season, beginning with Typhoon Bess, tropical cyclones attaining tropical storm strength or greater were assigned names on an alternating male/female basis. This change was a result of the 1979 Tropical Cyclone Conference, and the list of names can be found in CINCPACINST 3140.1N CH-1. A similar but different series of cyclone names is used for eastern North Pacific and North Atlantic cyclones. Each tropical cyclone's

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### WESTERN NORTH PACIFIC

1979 SIGNIFICANT TROPICAL CYCLONES

CYCLONE	TYPE	NAME	PERIOD OF WARNING	CALENDAR DAYS OF WARNING	MAX SFC WIND	MIN OBS SLP	NUMBER OF WARNINGS	DISTANCE TRAVELLED
01	TY	ALICE	O1 JAN-14 JAN	14	110	930	51	2597
02	TY	BESS	20 MAR-25 MAR	6	90	958	21	1804
03	ŦΥ	CECIL	11 APR-20 APR	10	80	965	40	2535
04	TS	DOT	10 MAY-16 MAY	7	40	984	24	2876
05	TD	TD-05	23 MAY-24 MAY	2	30	998	6	2170
06	TY	ELLIS	01 JUL-06 JUL	6	85	955	22	1612
07	TS	FAYE	01 JUL-06 JUL	6	40	998	20	1837
08	TD	TD-08	24 JUL-25 JUL	2	20	1004	5	1264
09	ST	HOPE	27 JUL-03 AUG	10	130	898	33	3928
10	TS	GORDON	26 JUL-29 JUL	4	60	980	13	1058
11	TD	TD-11	03 AUG-06 AUG	4	25	997	14	1088
12	TY	IRVING	09 AUG-18 AUG	10	90	954	38	2732
13	ST	JUDY	16 AUG-26 AUG	11	135	887	39	2502
14	TD	TD-14	18 AUG-20 AUG	3	20	1006	9	605
15	TS	KEN	01 SEP-04 SEP	5	60	985	13	1418
16	ŢY	LOLA	O2 SEP-08 SEP	7	90	950	23	1298
17	TY	MAC	15 SEP-24 SEP	10	70	984	35	1831
18	TS	NANCY	19 SEP-22 SEP	4	45	993	14	528
19	TY	OWEN	22 SEP-01 OCT	10	110	918	37	2151
20	TS	PAMELA	25 SEP-26 SEP	3	45	1002	6	984
21	TS	ROGER	03 OCT-07 OCT	6	45	985	16	1920
22	TY	Sarah	04 OCT-15 OCT	12	110	929	43	1194
23	ST	TIP	05 OCT-19 OCT	16	165	870	60	3972
24	ST	VERA	02 NOV-07 NOV	6	140	915	23	1868
25	TS	WAYNE	08 NOV-13 NOV	6	50	990	22	1559
26	TO	TD-26	OT DEC-02 DEC	2	30	998	6	1070
27	TY	ABBY	01 DEC-14 DEC	14	110	951	52	4044
28	TS	BEN	21 DEC-23 DEC	3	60	990	10	2245
			1979 TOTALS	149*			695	

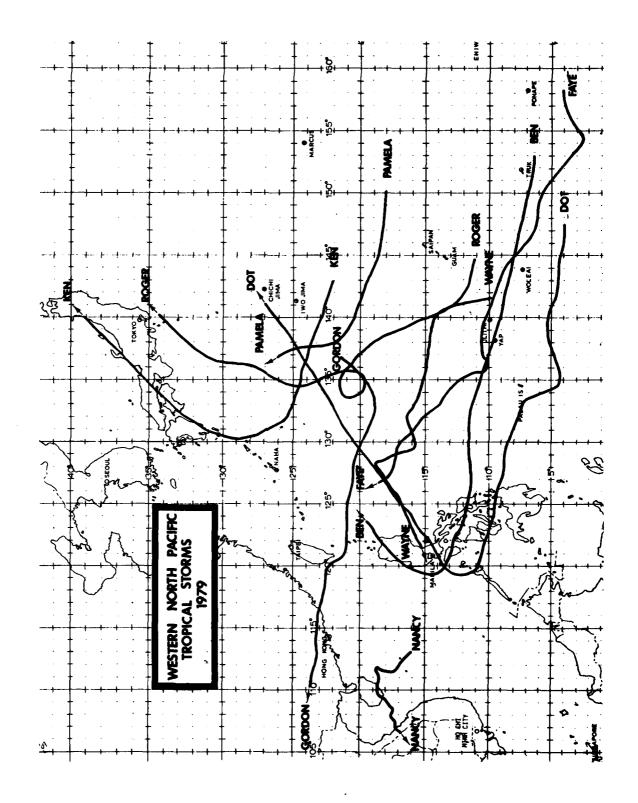
\*OVERLAPPING DAYS INCLUDED ONLY ONCE IN SUM.

maximum surface wind (MAX SFC WND), in knots, and minimum observed sea-level pressure (MIN OB; SLP), in millibars, were obtained from best estimates of all available data. The distance travelled, in nautical miles, was calculated from the JTWC official best track (see Annex A).

Table 3-2 provides further information on the monthly distribution of tropical cyclones and statistics on Tropical Cyclone Formation Alerts and Warnings. Even though there were 4 fewer cyclones this season compared to last season, there were 18 more warning days.

TABLE 3-2.														
}			197	9 SIG	NIFI CAN	T TROF	ICAL C	YCLONE	STATI	STICS				
WESTERN NORTH PACIFIC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	ост	NOV	DEC	TOTAL	(1959~78) AVERAGE
TROPICAL DEPRESSIONS	0	0	0	0	1	0	1	2	0	0	0	1	5	4.8
TROPICAL STORMS	0	0	0	0	1	0	2	0	4	1	1	1	10	10.0
TYPHOONS	1	0	1	1	0	0	2	2	2	2	1	1	13	18.0
ALL CYCLONES	1	0	ì	1	2	0	5	4	6	3	2	3	28	32.8
(1959-78) AVERAGE	0.6	0.4	0.6	0.9	1,4	2.1	5.2	6.8	6.0	4.8	2.7	1.3	32.8	
FORMATION ALERTS 23 of the 27 (85%) Formation Alert Events developed into tropical cyclones.  5 of the 28 (18%) tropical cyclones did not have a Formation Alert.														
WARNINGS Number of warning days: 149  Number of warning days with 2 cyclones: 38  Number of warning days with 3 or more cyclones: 5														

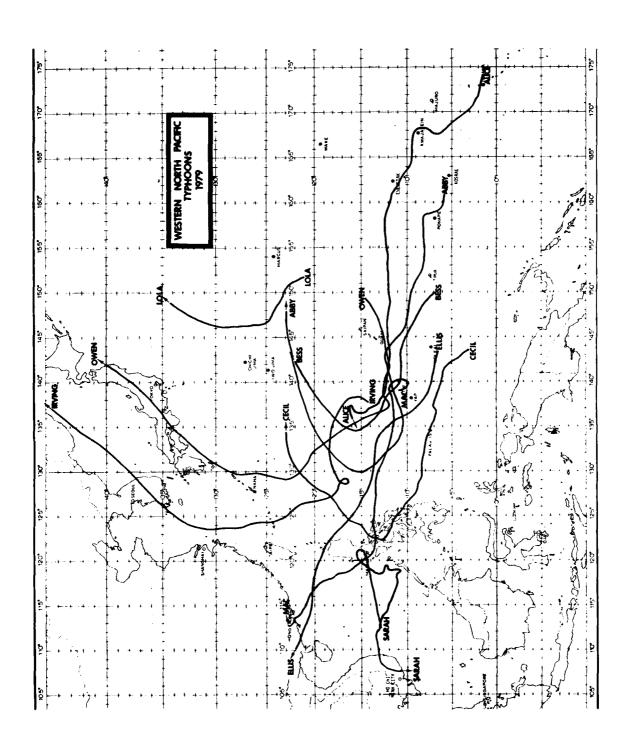
26 VESTERN NORTH PACIFIC TROPICAL DEPRESSIONS 1979 CHICHI PALAU IS

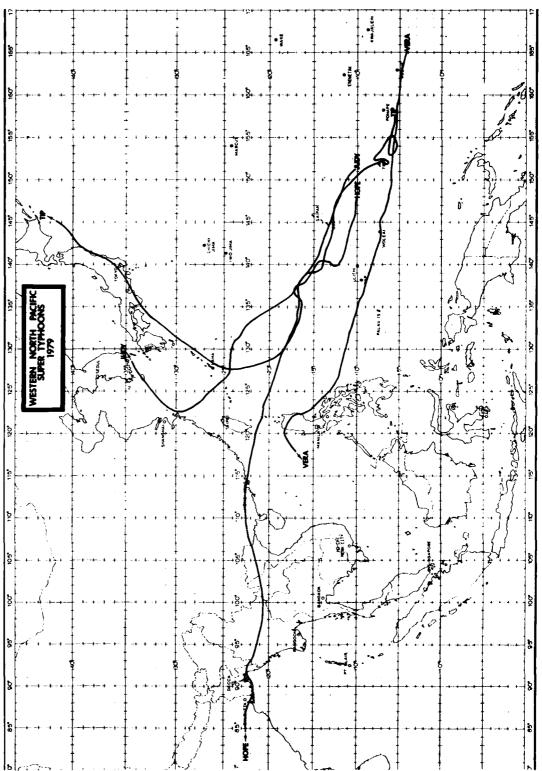


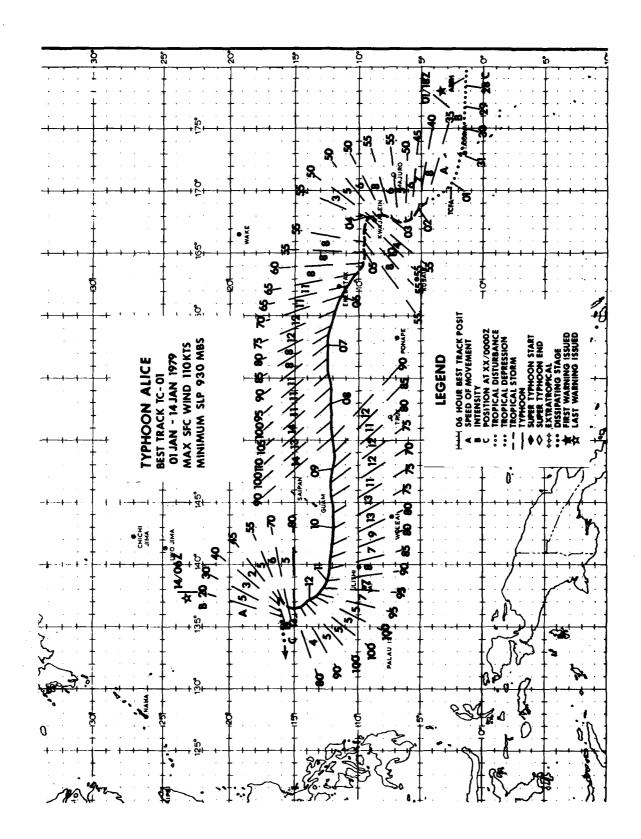
13

後がそこ

され、その対象を対することを持ているというには、対象を表するとなっている。







Typhoon Alice, the first tropical cyclone of the 1979 season, was actually first sighted as a tropical disturbance on the 27th of December 1978. Being over the Gilbert Islands quite close to the equator, the potential for development was considered poor. A tropical cyclone formation alert was issued at 03002 l January 1979 when satellite data showed the disturbance progressively increasing in organization. Soon after, the suspect area accelerated northwest to higher latitudes where development conditions were more favorable, and by 0118002, tropical storm Alice was named. Post-analysis showed that the tropical depression stage began near 0100002 at low latitudes, contrary to the general rule that cyclones do not form close to the equator.

Although a climatologically unfavored period for western North Pacific tropical cyclone development, the fact that Alice did form supports the non-existence of a definitive "typhoon season" for WESTPAC; tropical cyclones are possible anytime of the year. The greatest forecasting difficulties and concomitant large forecast errors occurred during Alice's formative and dissipating stages. Double intensification also contributed to Alice's notoriety.

Early in her lifetime, Alice meandered through the Marshall Islands as if determined to visit each island. One week later, on 12 January 1979, President Carter declared the Marshall Islands a major disaster area.

A satellite reconnaissance fix at 0221332 showed Alice had moved northeastward when forecast to continue northwestward. Being a fix on a poorly defined satellite image (PCN 6), it was not taken verbatim; northwest movement continued to be forecast. An aircraft reconnaissance fix at 0300532 confirmed the earlier satellite fix as did a follow-on 030310Z aircraft fix. Post-analysis revealed that a mid-latitude, shorttrough passed north of Alice during this time period. The trough extended deep enough into the tropics to weaken the midtropospheric ridge. This weakness permitted a southward intrusion of mid-latitude westerlies into Alice's vicinity, temporarily steering her northeastward. As the shortwave trough continued eastward, the subtropical ridge quickly reestablished itself north of Alice producing strong easterly steering flow, temporarily accelerating her from 4 to 10 kt (8 to 19 km/hr) toward the northwest when continued northeast movement was forecast. During this time, decision makers on Enewetak (also within the Marshall Islands), noting the low forecast confidence stated on prognostic reasoning messages, kept a condition of readiness which paid off.

From the 6th to the lltm, Alice traveled due west. On the 8th, Alice attained 110 kt (57m/sec) intensity and simultaneously accelerated to a speed of 14 kt (26 km/hr) (the fastest observed along track), whereupon she began weakening slowly.

During the 9th, Alice began an unexpected northward movement trend and showed further weakening. Post-analysis of low-level synop-

tic data and satellite imagery (Fig. 3-01-1) indicated that an approaching frontal shear-line was the responsible agent. The shear-line began interacting with Alice while she was southeast of Guam. As Alice neared Guam, radar data from Andersen AFB and alrcraft data indicated that Alice's previously well-defined wall cloud became larger and somewhat less organized. Cooler, drier air north of the shear-line was likely responsible for this weakening trend. A weakness in the subtropical ridge vertically above the shear-line apparently allowed for Alice's northward deviation.

The most unusual portion of Alice's track occurred during the final 3 days of Alice's life. Based on interpretation of PE progs, the subtropical ridge was expected to persist and maintain Alice in the easterlies. As a result, the JTWC forecasts (supported by the majority of objective forecast aids) indicated westward movement until 1200002, 18 hours after Alice had actually begun tracking northwestward. The subtropical ridge weakened in response to a long-wave trough deepening over eastern Asia. Easterly steering currents in Alice's vicinity diminished and veered in direction, permitting a more northward track. Alice reached a secondary intensity maximum of 100 kt (51 m/sec) during this period due to her slowing in speed of movement, the increased absolute vorticity of higher latitudes and good outflow aloft.

By the 13th, Alice turned northeastward and began weakening rapidly. The subtropical ridge was now completely severed and upperair westerlies were shearing Alice significantly in the vertical. Close proximity of yet another frontal shear-line contributed to further weakening. The biggest surprise, however, came when Alice's low-level circulation turned almost 180 degrees back toward the west at about 1312002 under the influence of strong, low-level easterlies and weakened rapidly in the strong, vertical-shear environment. As a result of vertical decoupling, Alice as a shallow depression, dissipated during the following 12-hour period.

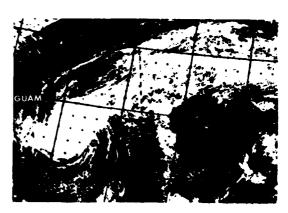
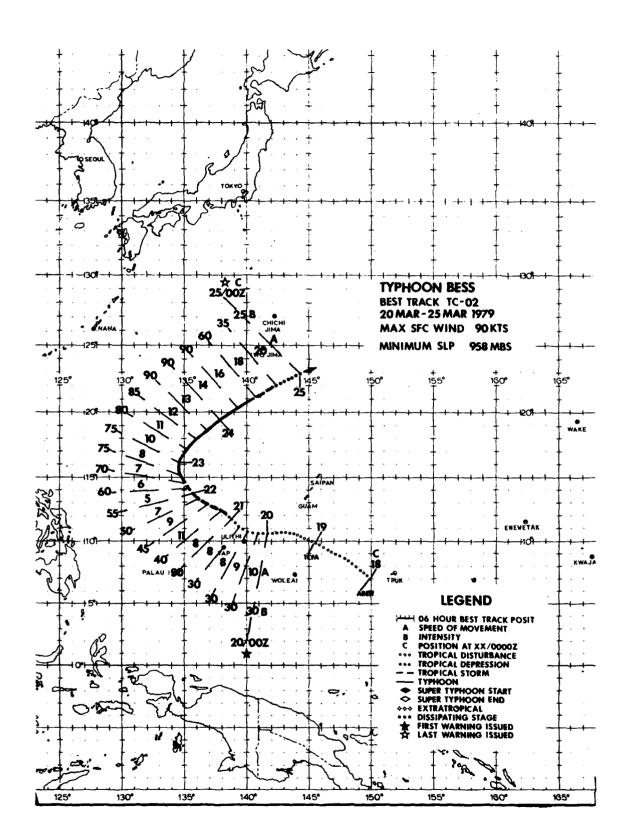


FIGURE 3-01-1. Typhoon Alice merging with the trailing end of a frontal shear-line, 9 January 1979, 00542. (DMSP imagery)



Since 1959, only three typhoons have developed over the Western Pacific in March. Of these three, only Bess developed in the last decade with Typhoon Tess developing in 1961 and Typhoon Sally in 1967. Tropical cyclone development in March is usually inhibited by a southward adjustment in the subtropical ridge axis. Although not recognized in advance, Typhoon Bess' development paralleled Typhoon Tess, which developed in the eastern Caroline Islands and reached tropical depression strength near Woleai Atoll. Continuing northwestward between Guam and Yap, both recurved northward near 135E (Fig. 3-02-1) before dissipating north of 20N under the influence of a strong vertical shear.



FIGURE 3-02-1. Typhoon Bess tracking northwestward between Guam and Yap at 8 kt (15 km/hr), 21 March 1979, 01037. Satellite imagery captured increased organization in the convective banding just prior to Bess reaching tropical storm intensity. (DMSP imagery)

Synoptic data at 160000Z suggested the existence of a weak surface circulation near 3.0N 152.5E at the base of a wave in the easterly flow. Satellite imagery at 160119Z indicated that an ill-defined area of convection existed near the surface circulation. By 161109Z, however, increased upper-level organization suggested development of a weak 200 mb anticyclone (Fig. 3-02-2). Increased curvature in the mid-level convective cloud pattern hinted at the possibility of tropical cyclone formation. As often observed in weak

developing systems, 162207Z satellite imagery showed a significant decrease in the mid- to upper-level convective organization, while the synoptic analysis continued to support a weak circulation southeast of Guam. Continuing to pulsate, the suspect area presented a curious, but intensified upper-level convective pattern on 172151Z and 172333Z satellite imagery. Synoptic analysis at 180000Z indicated that, in addition to the circulation near 3.5N 147.5E, a secondary low had developed on the slow moving wave axis near 7.1N 150.0E and that the earlier ill-defined convection had been associated with these two circulations. As this secondary low tracked northward up the wave axis, increased cyclon-



FIGURE 3-02-2. Infrared imagery of very early development stage of Bess, 16 March 1979, 11092. Streamline pattern indicates an upper-level anticyclone. A surface circulation had not yet developed. [DMSP imagery]

ic shear between strong easterly flow north of the wave and weak equatorial westerlies south of the wave caused the northern circulation to become the dominant center as the initial low weakened. Simultaneously, the upper-level anticyclone intensified, producing an excellent outflow signature on 182315z satellite imagery (Fig. 3-02-3). Although a formation alert was issued based on 182315z satellite imagery, continued rapid development did not occur as expected. Aircraft data at 200259z found strong enhanced easterly flow of 20-30 kt (10-15 m/sec) to the northeast, but only weak cyclonic flow to the south and east. Aircraft reports finally confirmed tropical storm strength early on the 21st (Fig. 3-02-4), five days after Bess was initially observed.



FIGURE 3-02-3. Infrared imagery of Typhoon Bess developing under good upper-level outflow which is visible from the southeast through the northwest, 18 March 1979, 23152. (DMSP imagery)

Sea Surface Temperature (SST) plays a vital role in the development and maintenance of tropical cyclones. A study by Charles P. Guard (1979) indicates that tropical cyclones which move over water cooler than 26C are less likely to intensify due to a reduction in latent heat. The study further states that tropical cyclones which develop prior to June intensify up to 10 kt (5 m/sec) after recurvature. This intensification, if expersenced, will occur within the 12-24 hour period following recurvature. Typhoon Bess followed this recurvature pattern. The axis of recurvature was crossed at 230000Z. Slow intensification occurred over the next 18 hours with Bess reaching her maximum intensity of 90 kt (46 m/sec) at 231800Z. Bess maintained 90 kt (46 m/sec) for 18 hours and then rapidly weakened, dissipating by 250000Z. SST analyses during 24-27 March (Fig. 3-02-5) indicate that the area in which Bess weakened from 90-60 kt (46-31 m/sec) in a six-hour period corresponds closely to the location of water cooler than 26C. The reduction of latent heat input, coupled with increased vertical shear produced by strong westerlies aloft, literally sheared Bess apart during the final 12-18 hours.



FIGURE 3-02-4. Typhoon Bess just prior to reaching her maximum intensity of 90 kt (46 m/sec), 23 March 1979, 02352. Bess displays a large elliptical eye with strong radial cirrus outflow in all directions. (DMSP imagery)

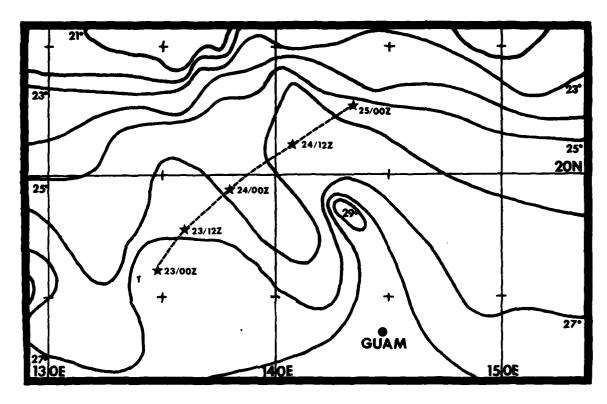
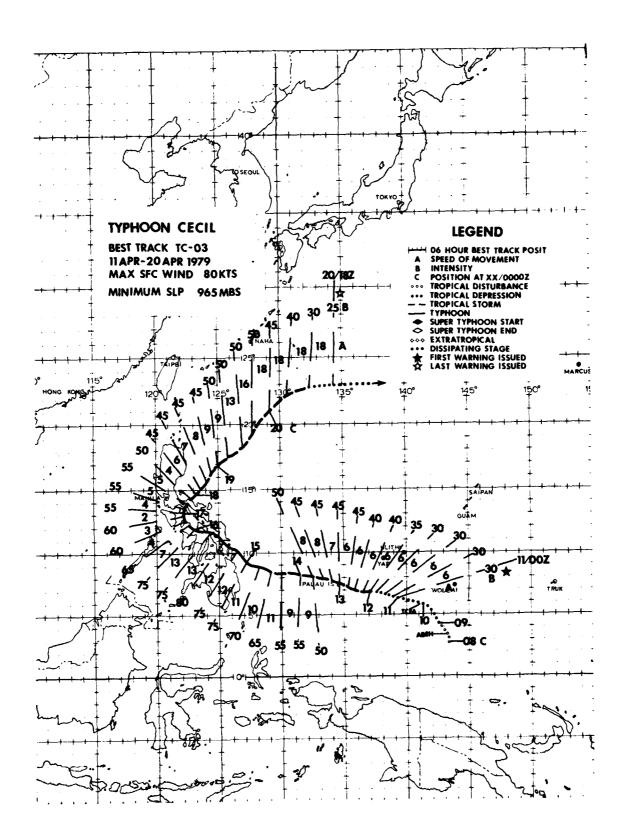


FIGURE 3-02-5. Composite of sea surface temperature analyses from 24-27 March 1979. Northeastward track of Typhoon Bess during dissipation stage is indicated by a dashed line with 12-hour positions.



Typhoon Cecil, the first tropical cyclone of 1979 in the Northwest Pacific given a male name, generated in mid-April from an easterly wave over the Philippine Sea. Cecil was forecast very well while on a climatological west-northwest track toward the central Philippines. Overall, post-analysis statistics showed that mean forecast errors were better than long-term averages. Nevertheless, JTWC warnings failed to forecast the crucial recurvature point in Cecil's track. Was there sufficient evidence to forecast this recurvature 24-48 hours in advance?

Post-analysis showed that recurvature occurred 36 hours after the 151200Z best track position. Satellite imagery (Fig. 3-03-1) located Cecil just south of Samar. At this time, the 500 mb subtropical ridge axis was at 17N with a small high pressure cell located over Northern Luzon. The 500 mb 36-hour PE prog maintained the ridge. Steering techniques based on this synoptic situation indicated westward movement for 72 hours. Analog techniques indicated west-northwestward movement. As a matter of fact, no objective forecast technique indicated recurvature prior to entrance into the South China Sea. The climatological average location of the 500 mb ridge axis is along 15N for April over the Philippines and the climatological recurvature point is 15-17N. Both

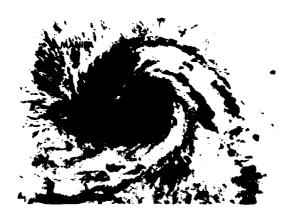
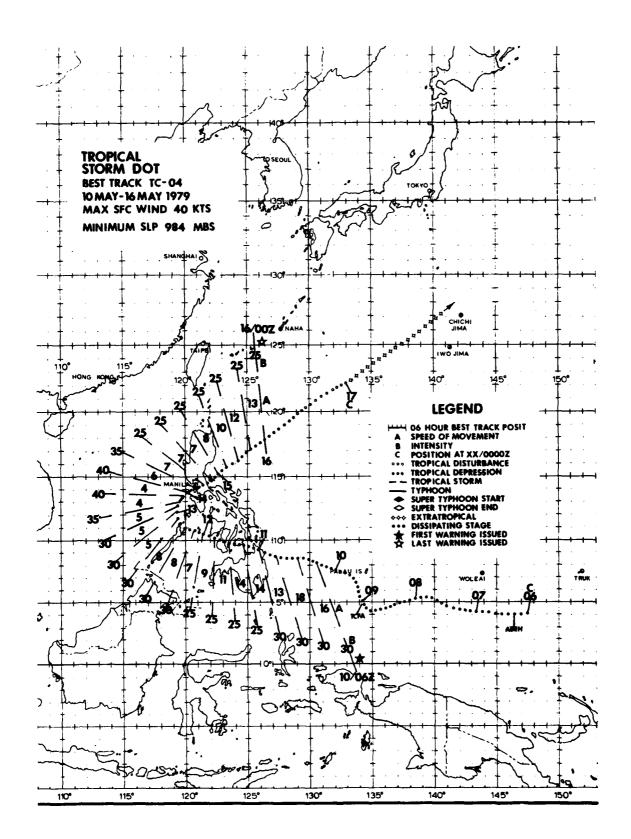


Figure 3-03-1. Infrared imagery of Typhoon Cecil 36 hours prior to recurvature with maximum sustained winds of 80 kt (41 m/sec), 15 April 1979, 1225Z. (DMSP imagery)

synoptic and climatological data indicated a west-northwestward track over the Philippines with recurvature late in the forecast period in the South China Sea as Cecil tracked to the vicinity of 15N. Post-analysis, however, revealed that the ridge axis east of the Philippines abruptly shifted south between 161200Z and 170000Z with westerly winds intruding far to the south over the South China Sea. This pattern shift caused Cecil to recurve much earlier than anticipated. Within 48 hours, Cecil was well east of Luzon (Fig. 3-03-2). The ridge axis shift was the vital piece of information not present in any of the available prognostic tools. Thus, it appears even in post-analysis that forecasting of Cecil's recurvature 36 hours in advance was beyond state-of-the-art capabilities.



FIGURE 3-03-2. Cecil after recurvature with maximum sustained winds of 50 kt (26 m/sec), 19 April 1979, 00142. (DMSP imageru)



#### TROPICAL STORM DOT (04)

Tropical Storm Dot did not reach tropical storm strength prior to landfall on the Philippine Islands (Fig. 3-04-1). Once Dot crossed the islands, tropical storm strength was attained lasting, however, less than 24 hours (Fig. 3-04-2). Dot's development was cut short by the eventual frictional effects of Luzon and increasing vertical wind shear aloft.

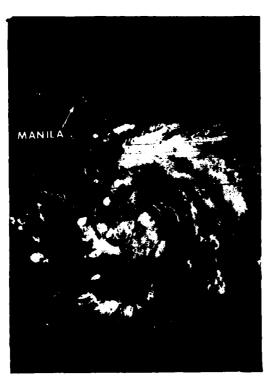
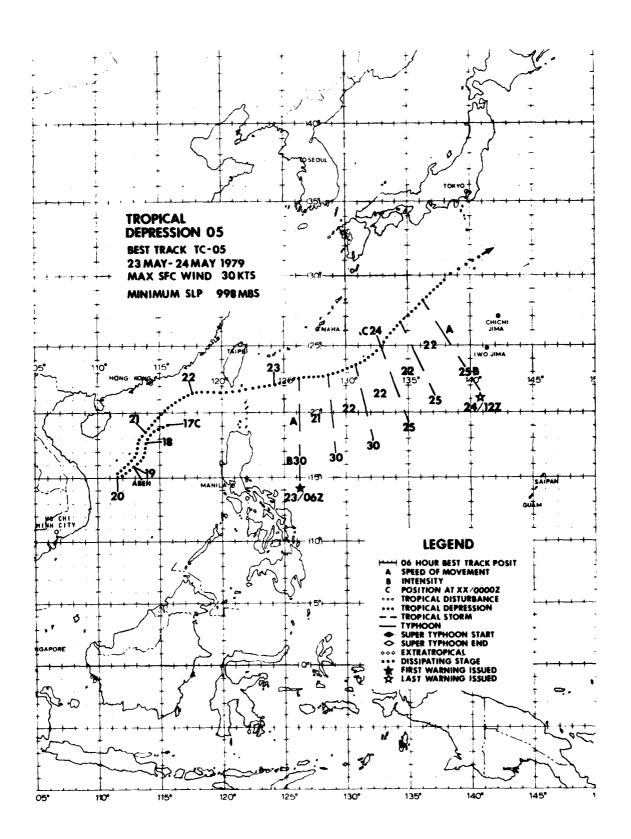


FIGURE 3-04-1. Tropical Storm Dot at 30 kt (15 m/sec) intensity while over northern Mindanao, 11 May 1979, 00292. (DMSP imagery)

TS Dot slowly formed in an area of broad, low-level easterlies, high surface pressures, and strong upper-level shear. The conditions for significant tropical cyclone development were poor while the system existed east of the Philippine Islands. After crossing the Philippines, however, Dot reached tropical storm strength while over the South China Sea.



FIGURE 3-04-2. Tropical Storm Dot while recurving toward Manila, 12 May 1979, 23532. (DMSP imagery)



### MONSOON/TROPICAL DEPRESSION (05)

Early season disturbances in the South China Sea, as discussed by Ramage (1971), may develop as a result of active monsoon troughs which extend eastward across Southeast Asia into the South China Sea (SCS). During late May, increased convergence in the enhanced southwest monsoon flow produced a significant increase in convection across the SCS, and several weak surface circulations were noted along the monsoon trough between Hainan Island and northern Luzon. Surface/gradient level synoptic analysis at 170000Z confirmed the existence of an elongated pressure trough with several 1005 mb centers. The main circulation, located northeast of the Paracel Islands, was actually north of the main convective area which covered most of the SCS south of the trough. Characteristics of SCS monsoon depressions include: strong enhanced southwesterly flow with light winds near the depression center; large areas of convection associated with convergence in the southwesterly flow with little curvature in towards the center; a relatively flat surface pressure regime of large areal extent; and, a mid-tropospheric cyclonic circulation over the area (Ramage, 1971). These conditions were observed in this area.

STATE WAS COMMON ON A SHIP

Initially, TD 05 drifted southwestward east of the Paracel Islands. By 2000002 a slow, eastward-tracking 500 mb short-wave over central China caused TD 05 to accelerate northeastward. As TD 05 accelerated, increased cyclonic shear at the surface southeast of Taiwan caused the system to transition from a monsoon depression to a tropical depression with a small anticyclonic outflow center evident aloft. (Many SCS monsoon depressions never make this transition, usually dissipating after 3-4 days.) Totall divorced from the monsoon trough, TD 05 tracked eastward through the Bashi Channel Totally and then along the remnants of a weak frontal boundary. TD 05 was not forecast to intensi-fy significantly, but it merged with an extratropical frontal boundary near 22.0N 124.8E and produced an improved satellite signature at 230018Z (Fig. 3-05-1) which included a banding-type eye. (Banding-type eyes are usually characteristic of more (Banding-type intense tropical cyclones.) Synoptic analyses during the life of TD 05 never indicated an intensity above 30 kt (15 m/sec). The lowest pressure recorded was 998 mb measured by a ship close to the circulation center. This pressure equates to approximately 32 kt (17 m/sec) (Atkinson and Holliday, 1975).

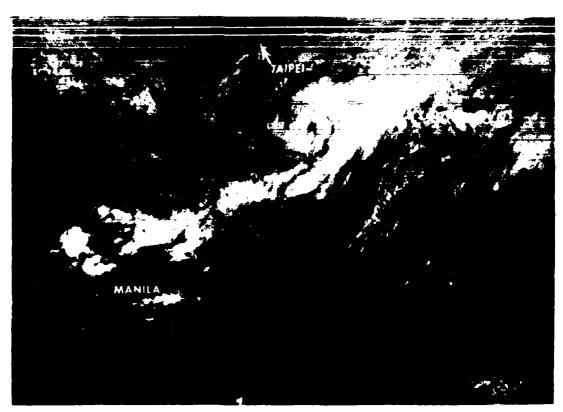
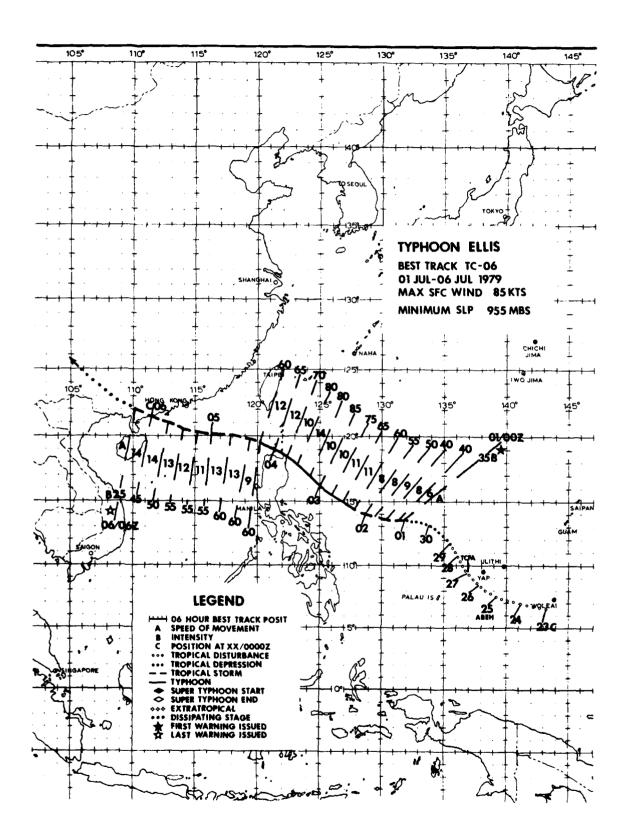


FIGURE 3-05-1. TD 05 at 30 kt (15 m/sec) intensity with banding-type eye moving east-northeastward at 20 kt (37 km/hr), 23 May 1979, 00182. (DMSP imagery)



The tropical disturbance, which later became Typhoon Ellis, was first noted on satellite and synoptic data on 25 June 1979. The surface/gradient-level analysis showed that a broad monsoon trough had developed between Guam and the Philippine Islands. upper-levels, a Tropical Upper Tropospheric Trough (TUTT) was oriented northeastsouthwest between the Volcano Islands and the central Philippine Islands. This TUTT allowed excellent upper-level outflow to the northeast and was expected to induce intensification of the tropical disturbance southeast of the TUTT axis. Therefore, a Tropical Cyclone Formation Alert (TCFA) was issued for the area valid at 2700002. However, significant development did not occur. Reconnaissance aircraft could find only a very broad surface circulation with relatively high surface pressures. The surface circulation drifted under the TUTT and the associated convection was suppressed; development was thereby thwarted. Based on the superposition of the TUTT and the surface circulation and the fact that the overall satellite signature had not improved, the TCFA was cancelled at 282000Z.

The area was closely monitored, and when satellite imagery showed increased convective development and surface data showed decreasing pressures and increasing winds, a second TCFA was issued valid at 300600Z. Subsequent aircraft investigation revealed a minimum sea-level pressure of 1000 mb and surface winds in excess of 35 kt (18 m/sec). Based on this new information, the first warning on TS Ellis was issued at 010000Z July. Ellis was in a favorable position at that time and steady intensification occurred over the next 2 days.

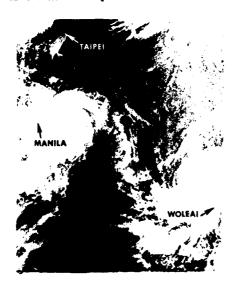


FIGURE 3-06-1. Typhoon Ellis (left) at maximum intensity of 85 kt (44 m/sec), 2 July 1979, 23562. TS Faye (right) is developing north of Woleai. (DMSP imagery)

For his entire lifetime, Ellis followed an uncomplicated, classic west-northwest track at near climatological speeds ranging from 9-14 kt (17-26 km/hr). Post-analysis indicates that Ellis was moving under the influence of the east-southeasterly steering flow on the southern edge of the subtropical mid-tropospheric ridge. Ellis' nearly straight track is due primarily to the fact that this ridge did not change in intensity or orientation during the period.

Ellis reached typhoon strength at 0212002 and a maximum intensity of 85 kt (44 m/sec) at 0300002 (Fig. 3-06-1). Continued intensification was anticipated, but a slow weakening trend was actually observed. As with Tropical Storm Faye, this weakening was associated with a drastic change in the upper-level flow pattern.

During Ellis' developing stage, the TUTT was located to the north-northwest and was providing the necessary outflow channel to the northeast. By 020000Z, however, an upper-level anticyclone over central China began to ridge eastward, forcing the TUTT to the northeast. Strong upper-level northeasterly winds associated with this anticyclone began to exert pressure on Ellis, shearing the convective activity to the southwest. Continuing west-northwest in this shearing environment, Ellis weakened steadily. By the time he was in the South China Sea, Ellis had weakened to tropical storm strength and was a completely exposed low-level circulation (Fig. 3-06-2).

With winds of 54 kt (26 m/sec), Ellis made landfall on the Chinese coast at 060000Z, 164 nm (296 km) southwest of Hong Kong and dissipated rapidly over land thereafter.

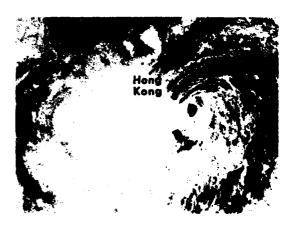
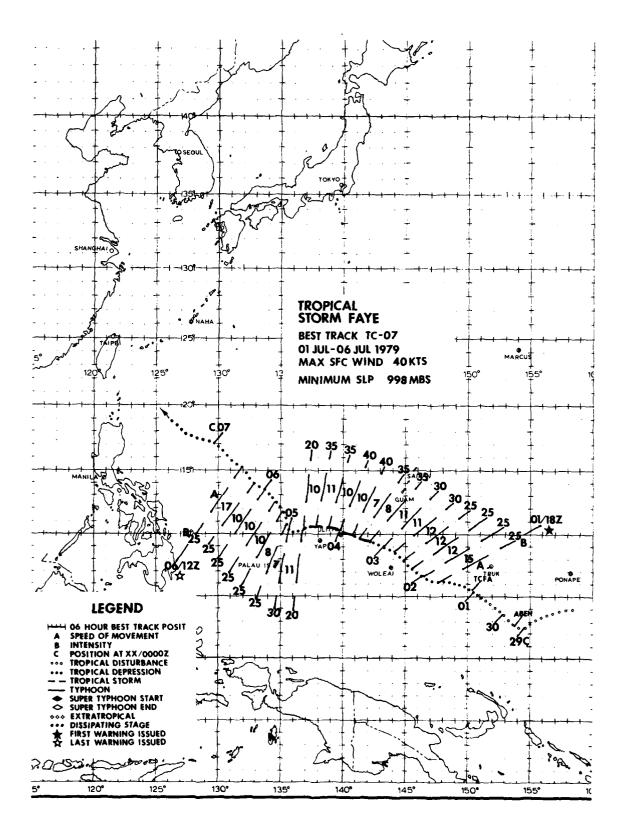


FIGURE 3-06-2. Tropical Storm Ellis as an exposed low-level circulation in the South China Sea, 5 July 1979, 01012. (DMSP imagery from Det 5, 11MU, Clark AB, RP)



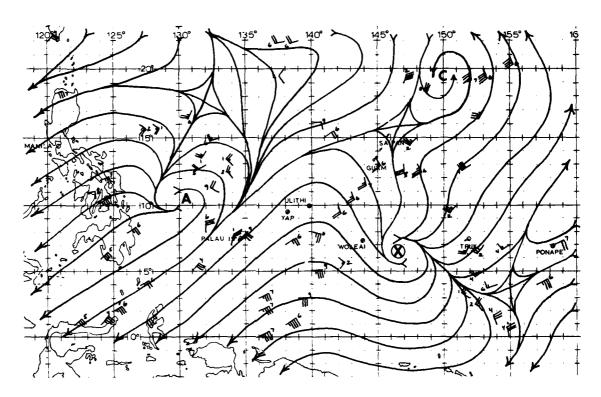


FIGURE 3-07-1. Upper-level streamline analysis ot 0200002 July 1979.

Tropical Storm Faye proved a most interesting case study, not because it developed into an intense tropical cyclone, but because typhoon intensity was not attained as forecast.

TD 07 was first analyzed as a closed surface circulation about 800 nm (1482 km) southeast of Guam on the 28th of June. The associated convective activity remained disorganized until 011200Z July. At that time a TUTT cell developed north of the system; thereby providing an excellent upper-level outflow channel to the northeast (Fig. 3-07-1). The wind data plotted in figures 3-07-1, -3 and -5 are a combination of RAOBS, AIREPS and satellite-derived winds for the 250 mb to 150 mb levels.

Diffluence over TD 07 was extensive and well-defined. The satellite signature also showed improved outflow (Fig. 3-07-2), and further intensification was expected.

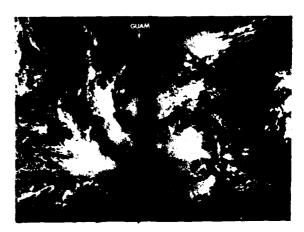


FIGURE 3-07-2. The tropical depression that was to become TS Faye, 02 July 1979, 0022Z. (DMSP imagery)

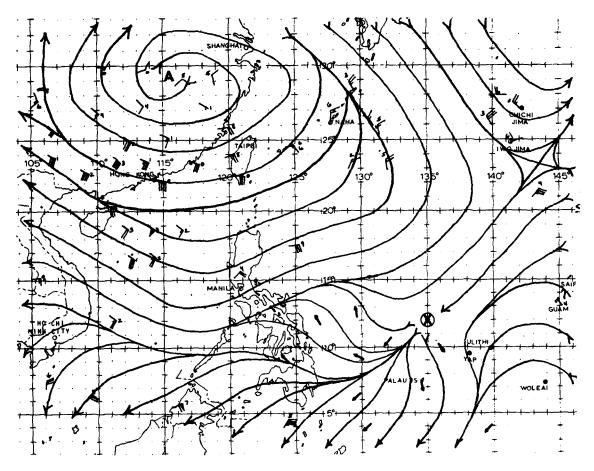
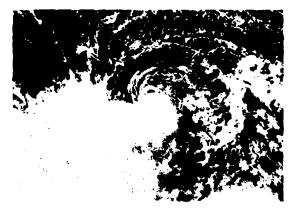


FIGURE 3-07-3. Upper-level streamline analysis at .0512002 July 1979.

The flow pattern over the depression (TD 07) remained favorable for development for the next two days and tropical storm intensity was reached by 031800Z. Continued intensification was still anticipated with typhoon strength forecast within 18 hours.

Instead of intensification, however, Faye weakened. Post-analysis shows that Faye's weakening, and subsequent dissipation, was linked to a radical change in the upper-level flow pattern. Whereas figure 3-07-1 shows a tropical cyclone in excellent position for intensification, figure 3-07-3 shows just the opposite. By 0512002, a large upper-level anticyclone over China was beginning to build southeastward into the western Pacific toward Faye. Faye's outflow channel to the north became restricted and her low-level circulation center became exposed (Fig. 3-07-4). The mid- to upper-level centers and the associated convection were sheared off to the southwest by increased northeasterly winds at the upper-levels.



gas track in the hope by

FIGURE 3-07-4. TD 01 (FAVE), 05 July 1979, 12022. Strong upper-level northeasterlies have begun to shear off the convection to the southwest. [DMSP imagery, Moonlight Visual]

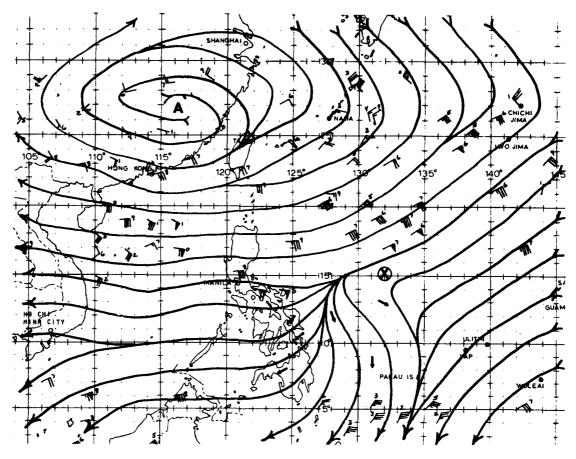


FIGURE 3-07-5. Upper-level streamline analysis at 061200Z July 1979.

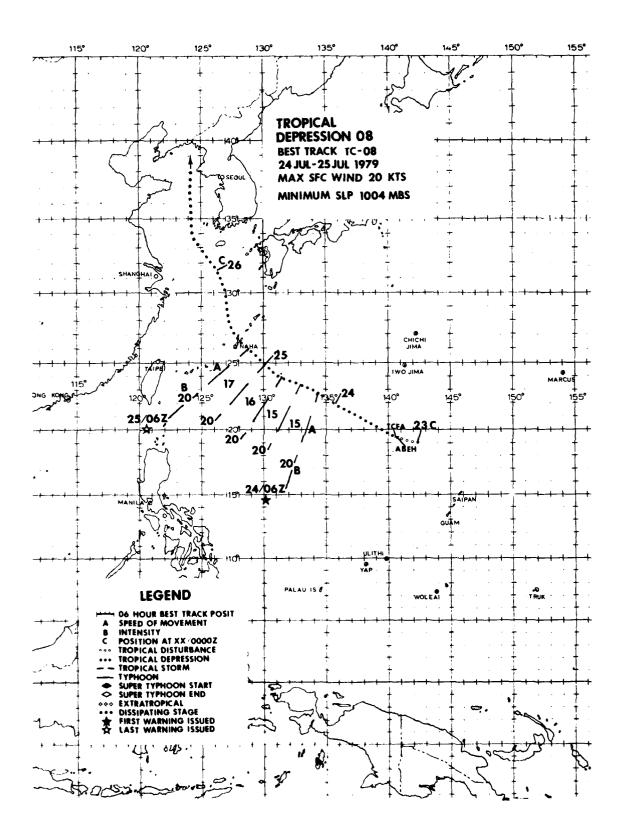
Displacement between surface and upper-level centers was observed often during the 1979 season (e.g., see discussions on Hope, Irving, Ellis). Development is usually arrested in this situation, until the system becomes aligned in the vertical. In the case of TS Faye, the upper-level pattern failed to improve. Figure 3-07-5 shows that by 0612002 the upper-level ridge had intruded as far east as Guam and that northeast winds aloft had increased to 50 kt (26 m/sec). At that time, Faye's low-level circulation was fully exposed (Fig. 3-07-6).

This exposed low-level circulation meandered northwestward for two days and eventually dissipated northeast of Luzon.

The short history of Tropical Storm Faye is an excellent example of premature dissipation induced by strong vertical wind shear.



FIGURE 3-07-6. TD 01 (FAVE) is now a fully exposed low-level circulation, 06 July 1979, 1518Z. (DMSP imagery, Moonlight Visual)



# TROPICAL DEPRESSION 08

For the greater part of its life, TD 08 was an exposed low-level circulation with the major convective activity detached to the north of the surface center (Fig. 3-08-1). Aircraft reconnaissance confirmed an exposed surface circulation approximately 100 nm (185 km) south of the convective center at 241016Z.

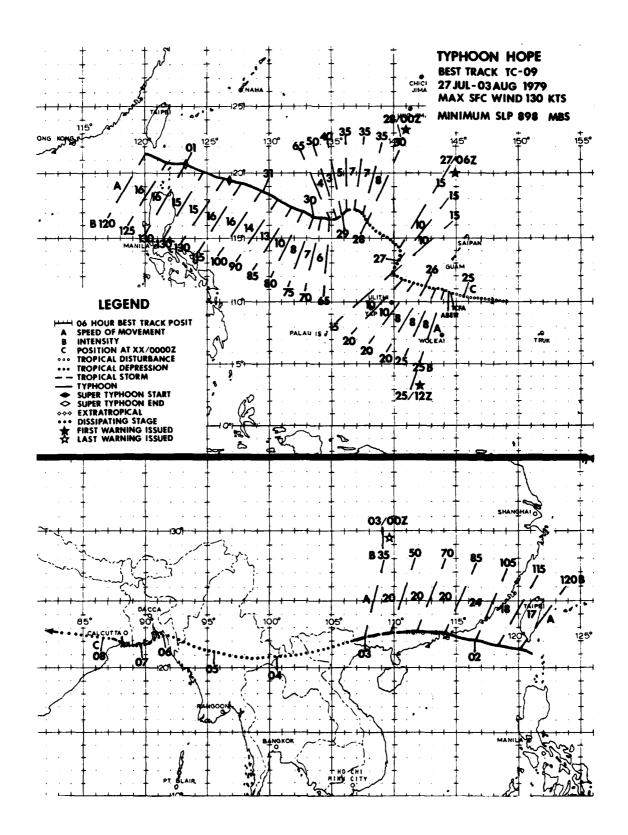
TD 08 was not expected to intensify to

tropical storm strength as a result of strong vertical shear which began on 2312002. However, initial warnings were issued based on the forecast track which indicated passage directly over Okinawa.

Post-analysis indicated that the calmwind center did indeed track over Okinawa with most of the convective activity tracking well north of the island.



FIGURE 3-08-1. Infrared imagery of TD 08 at maximum intensity of 20 kt (37 m/sec), 24 July 1979, 1244Z. TD 08's 2412002 surface center (4) is depicted relative to surface ship reports (4) and 700 mb aircraft reports (4). (DMSP imagery)



#### SUPER TYPHOON HOPE (09)

The disturbance which eventually developed into the first super typhoon of 1979 became evident on satellite imagery at 250000Z July as a focal point of cumulus banding. Future intensification was indicated as the disturbance was situated within an area of strong upper-level diffluence associated with the southern periphery of an east-west oriented TUTT. This outflow mechanism aloft, combined with an improved satellite signature, dictated issuance of a Tropical Cyclone Formation Alert at 2507512; the alert box described an area southwest of Guam. Subsequent aircraft reconnaissance at 2509002 described a cyclonic circulation with wind speeds of 15-25 kt (8-10 m/sec) and a central pressure of 1004 mb centered near 11.1N 144.5E. Based on this aircraft data and the proximity to Guam, the first warning on TD 09 (Hope) was issued at 251200Z.

From the 25th through the 26th of July, while TD 09 (Hope) tracked to the west-northwest, the TUTT axis shifted northward and strong upper-level northeast flow dominated the area. The resultant shear produced by this uni-directional upper-level flow displaced the convective activity to the southwest of the surface circulation, indicating a loss of vertical alignment and subsequent weakening. By 2706002, the center of the convective activity was displaced 120 nm (222 km) southwest of the low-level circulation center. Surface analyses, at this time, indicated the southwest monsoonal flow was being channeled principally into Tropical Storm Gordon located 750 nm (1389 km) to the northwest of TD 09 (Hope). With further weakening of Hope expected, a final warning was issued at 270451Z advising that the area would be closely monitored for possible

regeneration. Post-analysis showed that from 171200Z through 2800002, the TUTT weakened with resultant reduced shear over TD 09 (Hope). Conditions for development being improved, reorganization took place and TD 09 tegan to develop. Unfortunately, the improvement in the surface circulation went unnoticed as it occurred during the night when only infrared satellite imagery, on which low-level clouds are difficult to distinguish, was available. An aircraft investigation on the morning of the 28th reported a surface pressure of 999 mb with 45-50 kt (23-27 m/sec) winds in the heavy convective activity to the southwest of the surface center. A warning was issued at 280221Z indicating the regeneration of TD 09 (Hope).

By 280000Z, Tropical Storm Gordon had moved into the Luzon Straits. Due to the orographic blocking of the Philippine land mass, the majority of the strong southwest monsoonal flow was diverted into Hope. Th. This increased low-level inflow coupled with decreasing upper-level shear resulted in a much improved vertical structure with feederband activity developing in the south; 282052Z aircraft reconnaissance supported this improved organization trend. analysis indicates that TD 09 (Hope) could have been upgraded to tropical storm intensity 12-24 hours prior to the warning upgrade at 290000Z, as 35-45 kt (18-23 m/sec) winds were reported in feederband activity as much as 24 hours earlier (Fig. 3-09-1). By 290920Z, a well-defined eye with a central surface pressure of 972 mb and 65-70 kt (33-36 m/sec) surface winds were reported by aircraft data; the 2912002 warning upgraded Hope to a typhoon.



FIGURE 3-09-1. Hope (right) at tropical storm intensity 570 nm (1056 km) northeast of Quam, 29 July 1979, 02192. Tropical Storm Gordon (left) is 100 nm (185 km) east of Hong Kong. (DMSP imagery)

The 291200Z 200 mb analysis indicated the TUTT had again established itself north of Hope. Due to the east-west orientation of the TUTT, strong westerly flow along its southern periphery enhanced Hope's upperlevel anticyclonic outflow. Aircraft reconnaissance at 292031Z indicated a sharp decrease in surface pressure to 961 mb with the temperature/dewpoint data correlating to an equivalent potential temperature (9e) of 359K. An empirically derived forecast aid that relates pressure and 9e indicates that once the traces intersect, rapid intensification can be expected within 18-30 hours (Fig. 3-09-2). The intensification equates to a possible mean pressure decrease of 44 mb and a mean wind speed increase of 50-60 kt (26-30 m/sec). Typhoon Hope verified this study 36 hours after the intersection occurred; reconnaissance aircraft reported a surface pressure of 898 mb and wind speeds of 100-120 kt (51-62 m/sec). By 311200Z, Hope attained super typhoon intensity of 130 kt (67 m/sec) (Fig. 3-09-3).

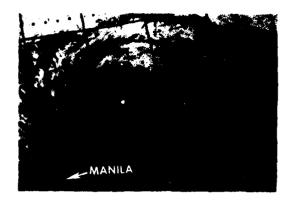


FIGURE 3-09-3. Infrared imagery of Hope just after attaining super typhoon intensity of 130 kt (67 m/sec), 31 July 1979, 1244Z. (DMSP imagery)

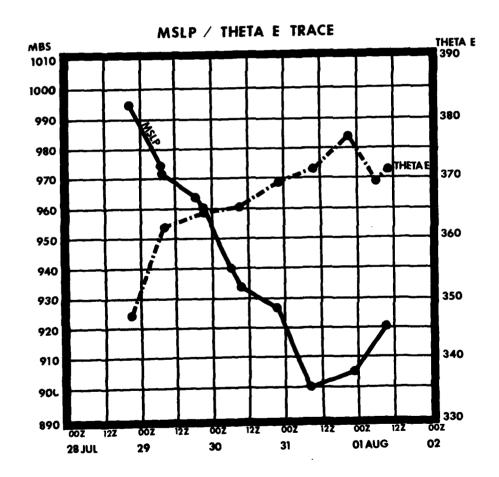


FIGURE 3-09-2. Time cross-section of Hope's minimum sea-level pressure versus equivalent potential temperature (THETA E  $\{\theta_e\}$ ) derived from aircraft reconnaissance.

Hope entered the Luzon Straits approximately 4 days after Tropical Storm Gordon. Hope's compact wind structure and a slight weakening trend were noted as Heng Chun (WMO 46752) on the southern tip of Taiwan reported sustained winds of 40 kt (21 m/sec) with gusts to 86 kt (44 m/sec) at 011000Z as Hope passed 45 nm (83 km) south of the station. Two persons on the Batanes Islands and one person on Taiwan were killed as a result of the torrential rainfall experienced as Hope tracked through the Luzon Straits.

Typhoon Hope made landfall less than 10 nm (19 km) north of Hong Kong at 0205302 (Fig. 3-09-4) with maximum sustained winds of 70 kt (36 m/sec) and gusts to 110 kt (57 m/sec) reported. Figure 3-09-5 is a time sequence of the surface observations received from the Royal Observatory of Hong Kong during Hope's passage. Extensive wind and rain damage, 3 deaths and over 258 injuries were reported. Damage to shipping within Hong Kong harbor was heavy as 17 ships broke their moorings and 8 ships collided.

Subsequent to passage over Hong Kong, Hope moved into southern China and weakened. The final warning was issued at 0301112 downgrading Hope to tropical storm intensity. Hope's uncomplicated northwest track after development into a typhoon resulted in minimal right-angle track errors with her unexpected acceleration accounting for the majority of the discrepancy.

Although weakening considerably during passage over southeast Asia, Hope did maintain a satellite signature and exited into the northern Bay of Bengal 110 nm (204 km) southeast of Dacca, Pakistan at 060500Z.

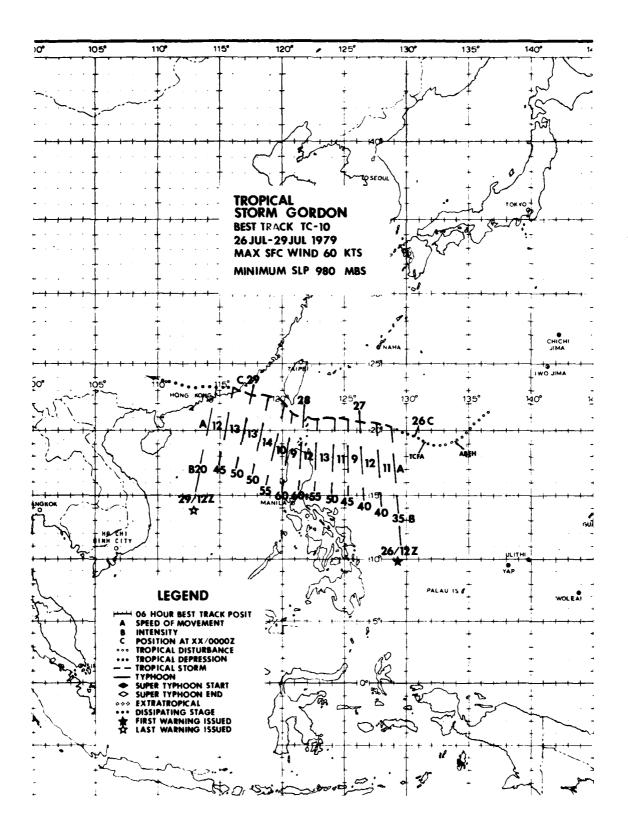


FIGURE 3-09-4. Typhoon Hope at 100 kt [5] m/sec] intensity, 3 hours prior to closest point of approach to Hong Kong, 2 August 1979, 02472. (DMSP imagery)

Strengthened once again by pre-existing strong southwest monsoonal flow, Hope reintensified from 0700002 through 0718002 with maximum sustained winds of 35 kt (18 m/sec) reported on 0712002 surface analysis. A tropical cyclone warning was not issued due to Hope's proximity to land and her expected movement into northeastern India within 12 hours. Hope, however, was discussed at length in the Significant Tropical Weather Advisory (ABEH PGTW).

45005 - HONG KONG OBSERVATORY				ST HOPE		DATE:02 JULY 1979 / TIMES:01-10Z			
02/012	02/02z	02/03z	02/04z	02/052	02/06z	02/07z	02/08z	02/09z	02/10 <sup>2</sup>
G37: 10 991	·//_989	984 G47] 984	978 G56.: • 978	965 GA-965	960 G83		: 3 983	∴ 988 G54	÷ \$ 992

FIGURE 3-09-5. Hourly surface synoptic observations from the Royal Observatory of Hong Kong (ROHK) during passage of Typhoon Hope.



Gordon, the 10th significant tropical cyclone of 1979, developed in late July in the monsoon trough near 20N-135E and eventually made landfall east-northeast of Hong Kong. A stronger sister, Hope (TD 09), followed Gordon several days later on a similar track into Hong Kong. Note that TD 09 (Hope) and TD 10 (Gordon) are alphabetically out of sequence because TD 10 was upgraded to tropical storm stage before TD 09.

Post-analysis revealed that Gordon reached tropical storm intensity at the time of the first warning. CINCPACINST 3140.1N, section 2.5.1., paragraph b states that warnings will be issued when "maximum sustained wind speeds are forecast to increase to 34 or more knots within 48 hours." In this case, there was no lead time between the first warning and tropical storm stage. Figures 3-10-1 and 3-10-2 illustrate why this occurred. TD 10 developed rapidly within the 22-hour time period between these figures. Synoptic data indicated increasing southwest monsoon flow into the area during this period; yet no definitive surface circulation could be located. The most significant finding of the post-analysis was that Gordon could not be traced back 48 hours prior to the first warning from available synoptic and satellite data, and, therefore, falls into the category of a rapid developing system.

Gordon's track took an unexpected jog northwestward while passing south of Taiwan (Fig. 3-10-3). (Typhoon Hope took a similar, but less pronounced, jog.) This northward adjustment is historically evident from tropical cyclones that pass south of Taiwan. The influence of Taiwan's high mountain range is thought to be responsible. As tropical cyclones pass south of Taiwan, they induce lee-side troughing west of the mountains over the Formosa Strait and track northwestward in response.



FIGURE 3-10-1. Tropical Storm Gordon in its infancy 4 hours prior to being discussed on the Significant Tropical Weather Advisory (ABEH PGTW), 25 July 1979, 01512. (DMSP imagery)

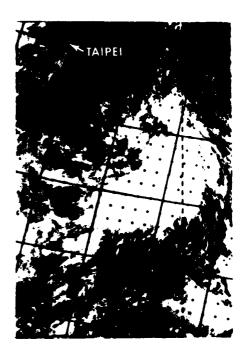
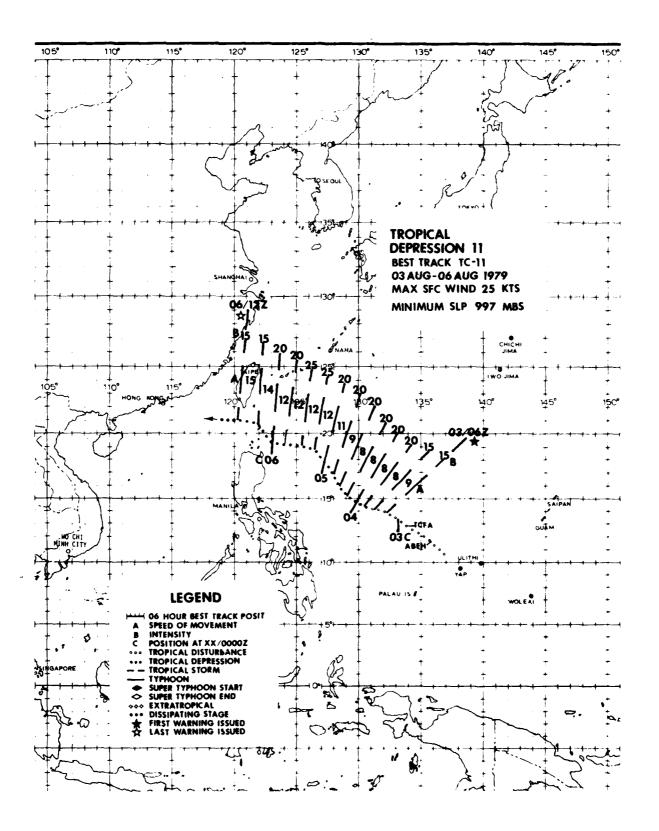


FIGURE 3-10-2. Tropical Storm Gordon 22 hours after Figure 3-10-1 showing increased development, 25 July 1979, 23502. A Tropical Cyclone Formation Alent was issued 6 hours prior to this time. (DMSP imagery)



FIGURE 3-10-3. Kaohsiung radar presentation of Gordon at 2821037 after passing south of Taiwan. (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan.)



# TROPICAL DEPRESSION 11

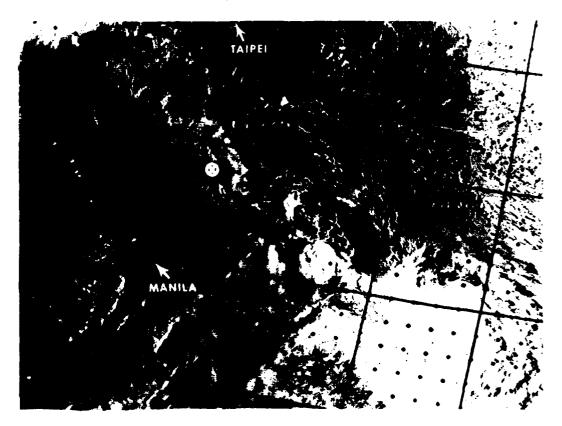
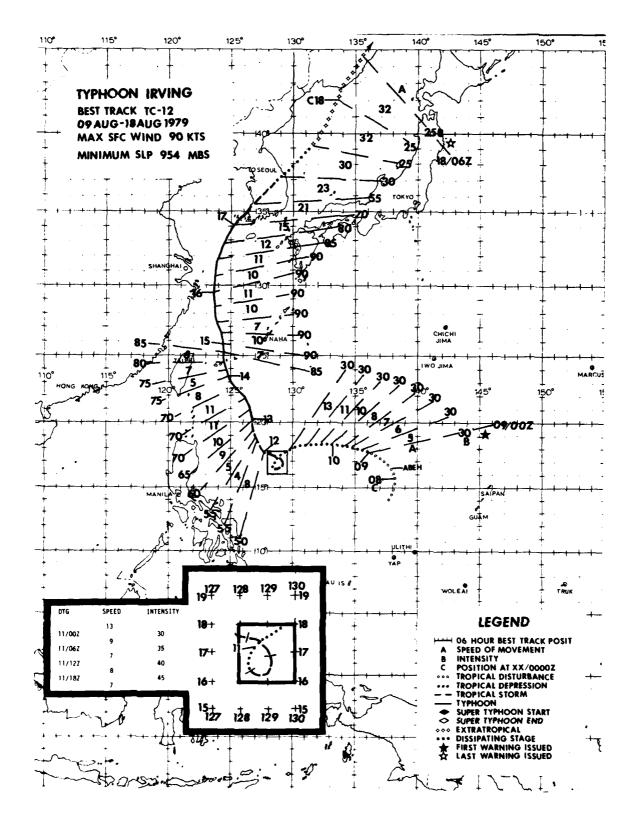


FIGURE 3-11-1. Tropical Depression 11 at 20 kt (10 m/sec) intensity, 5 August 1979, 21532. The TD symbol () is superimposed at location of surface circulation center as determined by aircraft reconnaissance at 0522222. Considerable vertical shear existed over the system and was the reason that it did not develop into tropical storm strength. (DMSP imagery)



Surges in the southwest monsoon frequent the western North Pacific during the early tropical cyclone season and produce widespread convection from the Malay Peninsula to as far east as Guam. During the same period, the 500 mb monsoon trough fluctuates eastward across the South China Sea (SCS) and occasionally into the Philippine Sea. By late July 1979, an eastward extension of the midlevel monsoon trough was the main synoptic feature west of Guam. The 500 mb trough axis extended along 15N from northern Vietnam through the central SCS and then eastward into a quasi-stationary low pressure center over the Philippine Sea.

On 7 August at 1200Z, a developing surface circulation was observed at the eastern end of the monsoon trough near 14.1N 137.7E. This weak circulation tracked cyclonically around the eastern periphery of the broad 500 mb low pressure center in the Philippine Sea. Taking on the characteristics of a monsoon depression (Ramage, 1971), Irving was described in aircraft reconnaissance data received from 9-11 August as a weak depression with poor vertical alignment and maximum surface winds located 150 to 180 nm (278 to 333 km) west of the surface center. At this stage, Irving displayed an

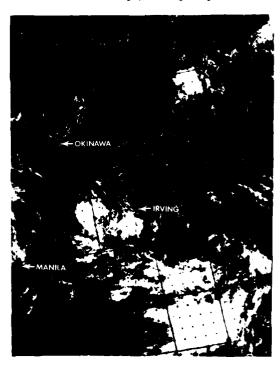


FIGURE 3-12-1. Typhoon Irving as a weak tropical depression with an exposed low-level circulation, 10 August 1979, 01262. Prior to intensification, aircraft reconnaissance consistently observed the maximum convection to the west of the surface center. IDMSP imagery!

exposed low-level circulation in satellite imagery with maximum convection located to the west of the surface center (Fig. 3-12-1). Ship synoptic data during the same period indicated that 25-35 kt (13-18 m/sec) winds extended outward 120 nm (222 km) south of the surface center.

By the 11th, the monsoon surge had weakened and receded westward, leaving a cut-off 500 mb low over the Philippine Sea in the vicinity of Irving's surface circulation. Irving executed a small, tight cyclonic loop on the 11th. During the loop, vertical alignment between the surface and the 500 mb center improved, and Irving intensified to tropical storm intensity. Simultaneously, a break developed in the 500 mb subtropical ridge to the north, and Irving tracked north-northwestward towards the Ryukyu Islands while intensifying further to typhoon strength. Although originally forecast to recurve south of Japan, strengthening of the 500 mb ridge southeast of Japan caused Typhoon Irving to track over the western East China Sea and accelerate north-northeastward across Korea before merging with an extratropical frontal boundary north of Japan.

Although not a spectacular typhoon, Irving's apparent sinusoidal motion, unusually large wind radii, failure to rapidly deepen and damage to southern Korea are noteworthy. Sinusoidal motion of tropical cyclones has been observed for many years, especially when short-term movements are observed by accurate fix platforms such as land radar (Fig. 3-12-2) and reconnaissance aircraft. Sinusoidal motion was observed from 1316002 to 1518002 as Irving tracked north-northwestward through the East China Sea. Radar reports from the Ryukyu Islands

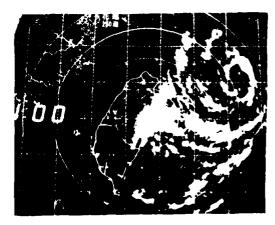
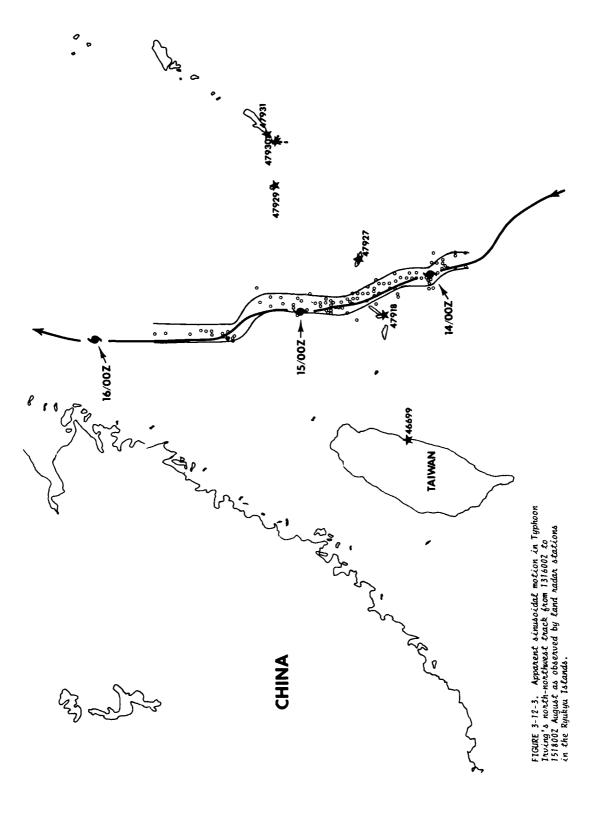


FIGURE 3-12-2. Typhoon Inving as seen by the radar at Haulien, Taiwan. Inving tracked north-northwest-ward across the southern Ryukyu Islands and was accurately tracked by eight radar sites, 14 August 1979, 17002. (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan)



clearly indicate that Irving oscillated about an overall north-northwest track (Fig. 3-12-3).

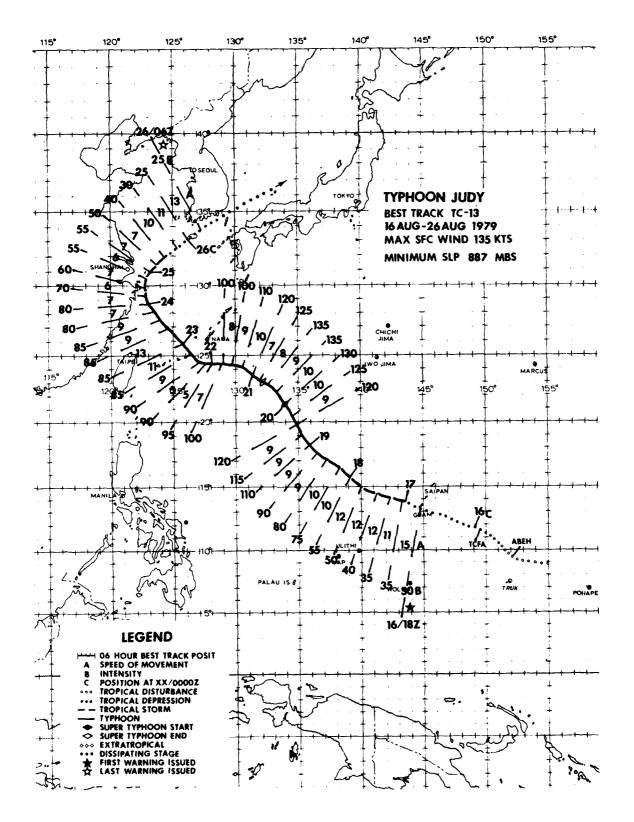
The relationship between Irving's surface and 500 mb centers during the earlier stages of development produced unusually large surface wind radii. Synoptic and aircraft data between 092002 and 1200002 indicate that Irving's maximum wind band actually existed 150-200 nm (278-370 km) west of the large, calm-wind surface center. Although the maximum wind hands did eventually migrate towards the surface center, the wind radii remained large for the duration of Irving. The large wind radii may be related to Irving's developmental interaction with the 500 mb monsoon low and its large areal extent. Irving never became a tight, wel' developed tropical cyclone. Aircraft reconnaissance during the period of eyewall development indicated that Irving had a large 30 nm (56 km) diameter eye with the radius of over 30 kt (15 m/sec) winds extending outward 400 nm (741 km) in the eastern semi-circle.

Unlike Super Typhoon Hope, Typhoon Irving (Fig. 3-12-4) did not follow the intensification pattern suggested by JTWC's Equivalent Potential Temperature ( $\theta_{\rm e}$ )/Minimum Sea-level Pressure Study. This study indicates that sea-level pressure should fall about 44 mb and maximum surface winds should intensify an average of 55 kt from the point where the  $\theta_{\rm e}$  and pressure curves intersect (see Super Typhoon Hope, Figure 3-09-2). The reason why Irving failed to intensify further is not known.

Typhoon Irving was the first tropical cyclone to strike Korea in 1979. Rapidly weakening as he made landfall, Irving spared southern Korea from the destructive typhoon force winds he had maintained through most of the East China Sea. Korea did, however, receive torrential rains which produced wide-spread flooding. The hardest hit area was the island of Cheju Do where 4.3 inches (109.7mm) of rain were reported at Cheju. Official estimates reported 150 dead or missing, 1000-2000 homeless and approximately 10-20 million US dollars damage to food and agriculture.



FIGURE 3-12-4. Although Typhoon Irving did not develop according to intensification studies, Irving did possess good feederband activity and cirrus outflow, 14 August 1979, 02282. [DMSP imagery]



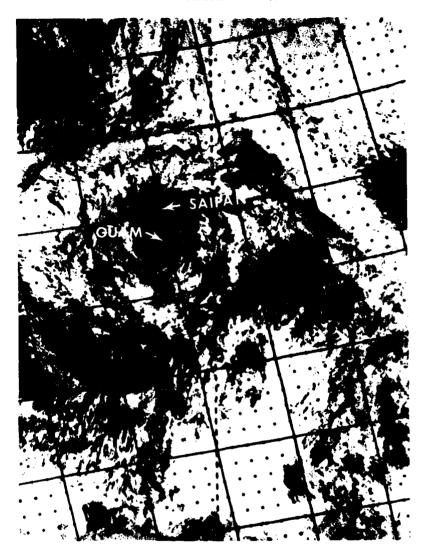


FIGURE 3-13-1. Infrared imagery of tropical disturbance (Judy) while southeast of Guam, 16 August 1979, 11202. The star denotes the approximate location of a weak surface center discovered by a reconnaissance aircraft about 4 hours earlier. (DMSP imagery)

Of all the typhoons of 1979, Judy's significance was only surpassed by Super Typhoon Tip. Judy eventually developed into the year's second super typhoon, but more importantly, she served as a reminder of how rapidly a minor tropical disturbance can develop into a dangerous tropical cyclone.

Surface synoptic data from the beginning to the middle of August showed that the area south and east of Guam was fairly inactive. Good cross-equatorial flow was

present, but only a few flare-ups of convective activity were noted. Surface circulations were broad, ill-defined and transient. By 15 August, however, synoptic and satellite data revealed a tropical disturbance, about 120 nm (222 km) east-northeast of Truk, which was to eventually become Typhoon Judy.

This area was closely monitored by JTWC, and when the satellite signature began to improve, a Tropical Cyclone Formation Alert was issued at 1521002.

No significant pressure falls were observed over the area as the disturbance drifted slowly west-northwestward. A reconnaissance aircraft at 1607002 was able to define only a weak surface circulation with a MSLP of approximately 1006 mb and observed surface winds in the south semicircle of 10 kt (5 m/sec) or less (Fig. 3-13-1).

Rapid intensification was not expected at that time, but at 161635Z, less than 10 hours after the aircraft investigation, weather radar at Andersen Air Force Base, Guam, located a well-defined circulation center moving west-northwest toward Guam at 15 kt (28 km/hr). Gradient-level wind reports from Guam, Truk, Palau and Ulithi at 161200Z also showed that the low-level inflow pattern associated with the disturbance had increased in areal extent. The disturbance continued tracking toward Guam and at 161800Z the center passed over the Naval Oceanography Command Center (NAVOCEANCOMCEN), Guam building on Nimitz Hill (Fig. 3-13-2). NAVOCEANCOMCEN reported a MSLP of 1001.0 mb and a wind gust to 51 kt (26 m/sec) at that time. Based on this "first-hand" information, JTWC issued the first warning on Tropical Storm Judy at 161900Z. Post-analysis revealed, however, that Judy did not reach tropical storm strength until 170000Z.

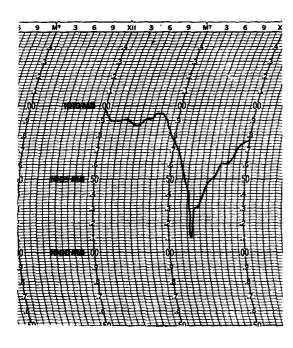


FIGURE 3-13-2. Microbarograph trace recorded at NAVOCEANCOMCEN, Guam during the passage of TD 13 (Judy) at about 1618002, August 1979.

Judy intensified steadily while following a nearly climatological west-northwest track at 10-12 kt (19-22 km/hr) for the next 24 hours. She reached typhoon strength at approximately 1803007. After that, a long-wave trough in the mid-level westerlies, moving over Japan toward the Pacific, fractured the subtropical mid-tropospheric ridge north of Judy, allowing her to track more to the northwest.

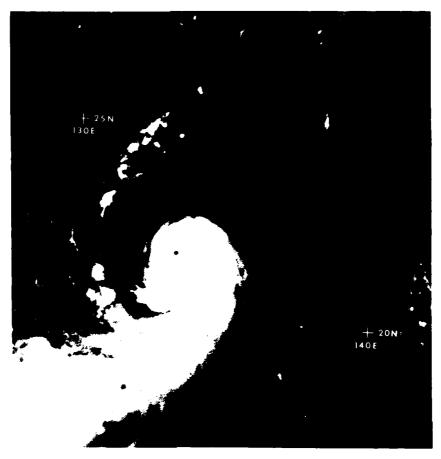
During the next 36-hour period, after reaching typhoon strength, Judy's central pressure dropped 69 mb and she attained super typhoon strength at 200000Z. Her lowest central pressure, 887 mb, was measured by a reconnaissance aircraft at 192145Z. Three distinct, concentric wall clouds were also noted at that time (Fig. 3-13-3). Super typhoon intensity was maintained until 201500Z, with gradual weakening thereafter.

Forecast aids indicated that Judy would pass to the south of Okinawa, but based on her persistence track and the deep trough that existed over Japan at 500 mb, Judy was forecast to recurve east of Okinawa. The steering aids were reacting to the mid-level PE Forecast series which built the ridge back between Japan and Judy. The numerical forecasts had not been verifying well up to that point, and, thus, the well-entrenched trough was forecast to persist. The numerical forecasts proved to be correct, however, and Judy did pass south of Okinawa before beginning to recurve into the East China Sea.

The rapidly intensifying ridge was expected to drive Judy into the Asian mainland south of Shanghai. The 500 mb analysis at 241200Z provided the first indication that Judy was not going to make landfall. At that time, she was just off the Chinese coast, but north of the mid-level ridge axis. Three-hourly synoptic reports from Sheng-Szu were watched closely and when the winds backed from east at 40 kt (21 m/sec) to north at 35 kt (18 m/sec), there was little doubt that Judy had, in fact, recurved to the northeast.

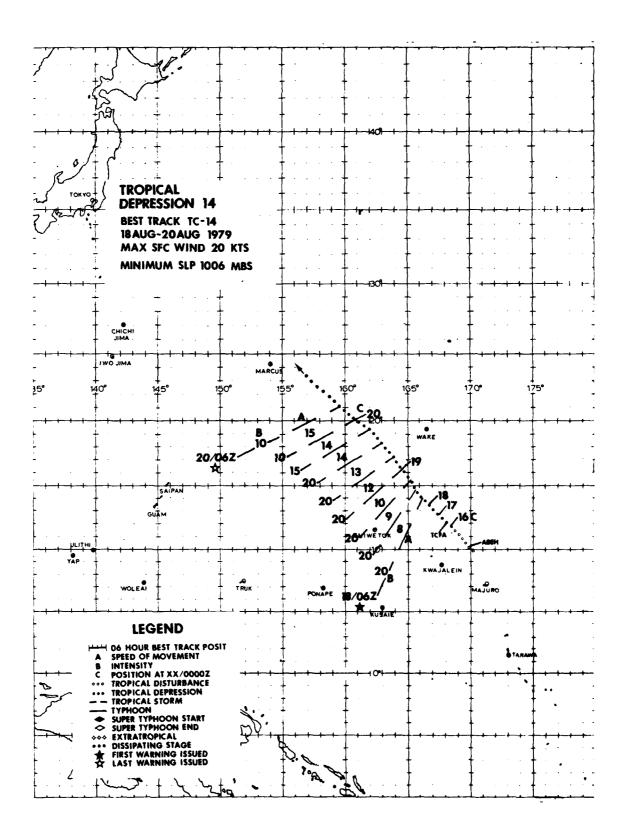
As Judy recurved, she was downgraded to tropical storm strength based on land synoptic data. Transition to an extratropical system occurred at 2612002 while Judy passed through the Korea Strait.

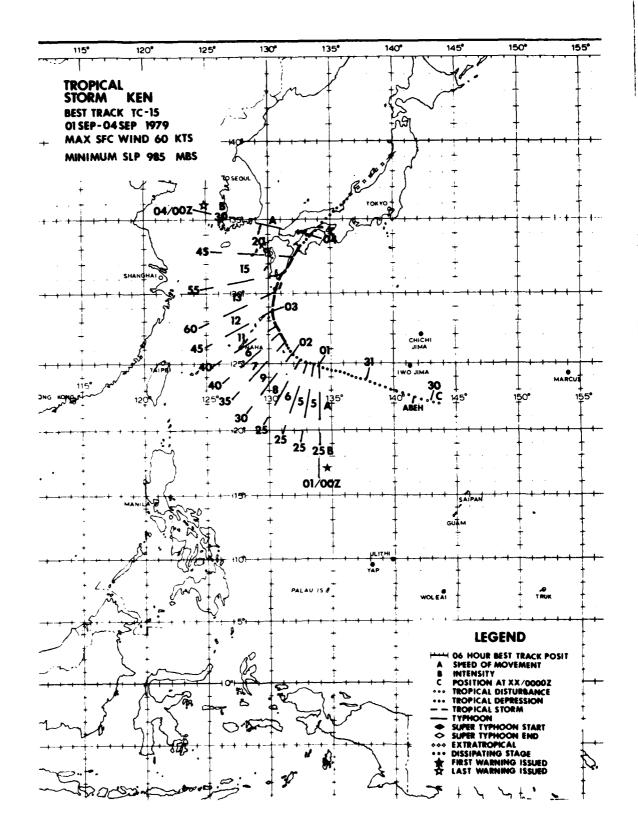
Due to being still relatively weak while passing over Guam, damage there was insignificant. Damage to Okinawa was also minimal, even though sustained winds of 40 kt (21 m/sec) were experienced for a 28-hour period. Southern Korea did not fare as well, however. One hundred eleven people were killed, over 8,000 houses were inundated, 57 vessels were destroyed and many thousands of acres of crops were ruined by Judy's torrential rains and strong winds.

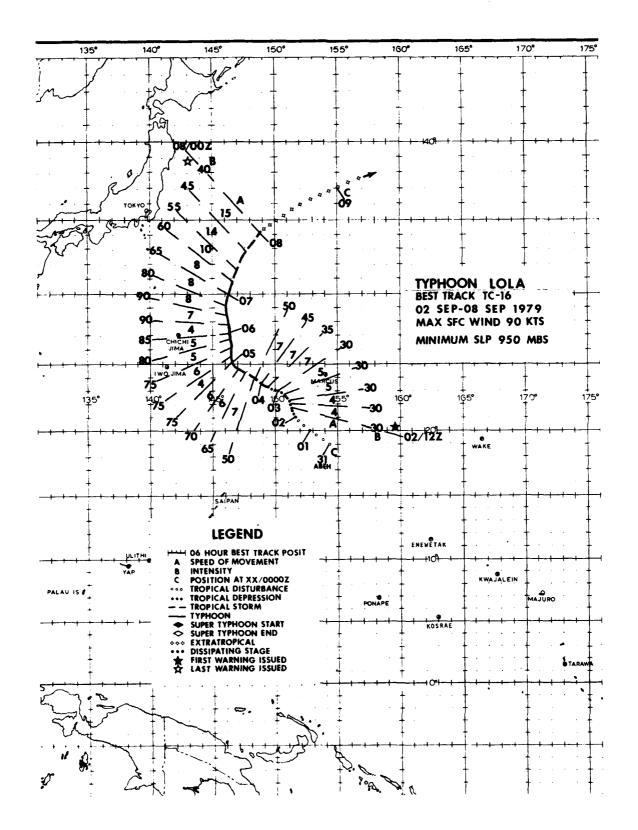


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FIGURE 3-13-3. Judy as a super typhocn, 20 August 1979, 0219Z. (DMSP imagery)







## TROPICAL STORM KEN (15) AND TYPHOON LOLA (16)

Ken and Lola developed almost concurrently along the periphery of an upper-level TUTT. Satellite imagery on 1 September 1979 (Fig. 3-16-1) shows a number of disturbances organized into a line of convection ringing the TUTT in question from north of Kadena to south of Marcus. Ken developed from the disturbance just east of Kadena. At this same time, the disturbance which developed into Lola is south of Marcus and appears quite weak. The largest and most menacing middle disturbance northwest of Guam (Fig. 3-16-1) did not develop.

During the next 48 hours, the TUTT

deepened southwestward over the middle disturbance and suppressed its convection. At the same time, it divided the convective line into the two distinct systems, Ken and Lola (Fig. 3-16-2).

After forming, Ken and Lola began to move in similar recurvature tracks. Ken tracked northward into the Sea of Japan reaching a maximum intensity of 60 kt (31 m/sec). Lola intensified into a typhoon and eventually transitioned into an extratropical system over the cooler waters east of Japan.

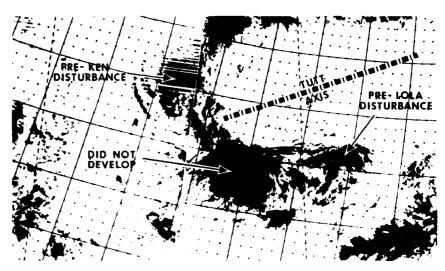
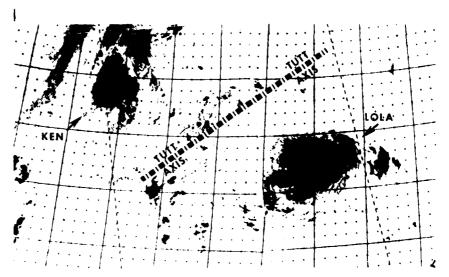
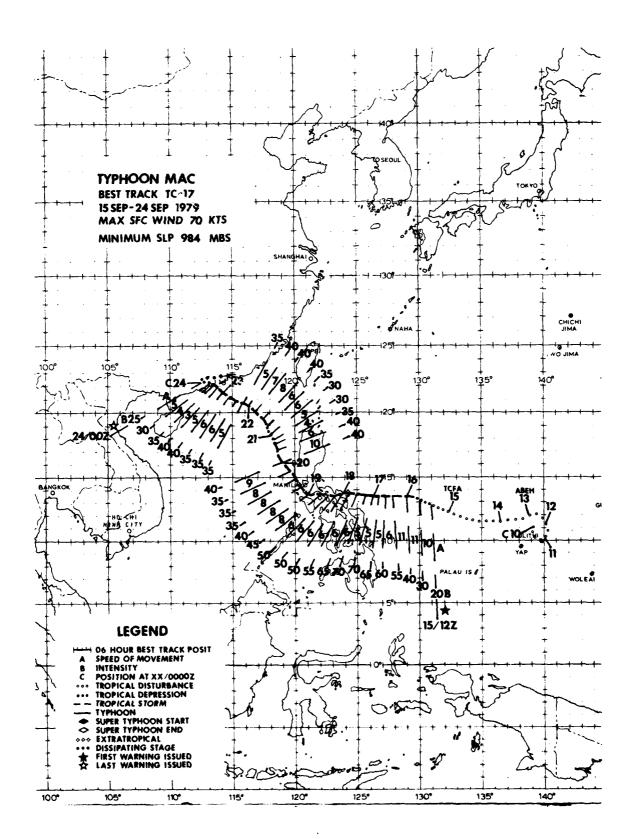


FIGURE 3-16-1. Line of tropical disturbances from which TS Ken and TY Lola eventually developed, 3122572 Aug - 0100392 Sep 1979. (DMSP imagery)



TIGURE 3-16-2. Ken at 45 kt (23 m/sec) intensity and Lola at 36 kt (15 m/sec) intensity, 0222212 - 0300032 Sep 1979. (DMSP imagery)



### TYPHOON MAC (17) AND TROPICAL STORM NANCY (18)

Typhoon Mac developed from a weak surface circulation northeast of Yap in September 1979. This circulation tracked westward, reaching tropical storm intensity by 160000Z. Mac followed the climatological intensification rate for tropical cyclones approaching the Philippines and reached typhoon intensity prior to making landfall. Frictional effects caused Mac to weaken slowly as he tracked across southern Luzon towards the South China Sea. The unexpected development of Tropical Storm Nancy east of Hai-nan Island influenced Mac's track in the South China Sea.

JTWC's real-time forecasts do not always reflect the actual intensity of a tropical cyclone. Rapid intensification or weakening, peripheral data unavailable due to geographical restrictions, and tight maximum wind bands, which are not initially detected, all reduce the accuracy of intensity estimates provided in tropical cyclone warnings. These intensity discrepancies often go unrecognized until discovered during post-analysis, as in the case of Typh-on Mac.

Reanalysis of aircraft reconnaissance data from 16-18 September indicates that Mac most probably intensified to typhoon intensity by 161800Z. During the period 16-18 September, aircraft reconnaissance at 160503Z reported 68 kt (35 m/sec) at 1500 ft (457 m) and 60 kt (31 m/sec) on the surface prior to encountering moderate turbulence which forced the aircraft to climb through the overcast stratocumulus cloud layer above. Subsequent reconnaissance data at 170810Z confirmed typhoon intensity by locating 80-90 kt (41-46 m/sec) surface winds in a 10-nm (19 km) wide band tucked under the strong eastern feederband. Mac made landfall prior to the next scheduled aircraft fix with geographical constraints severely reducing peripheral data collection.

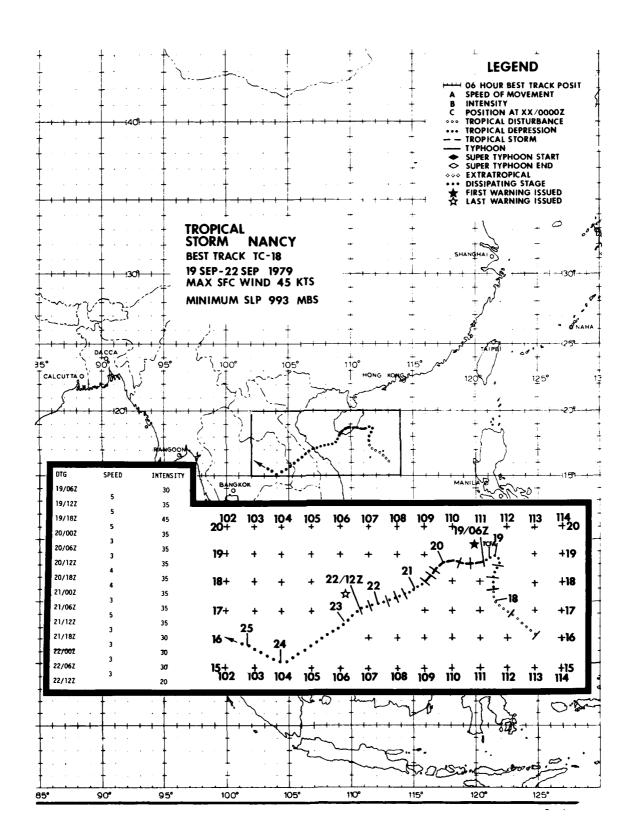
Although real-time data were available which indicated Mac had possibly reached typhoon intensity, the isolated reports of strong winds were dismissed as gusts associated with lower velocity sustained winds. (Aircraft data are occasionally not used verbatum when they fall outside reasonable limits after being analyzed with available surface reports, satellite data intensity estimates and the JTWC Maximum-Wind Minimum-Pressure Relationship (Atkinson and Holliday, 1977).) During post-analysis, the reconnaissance data were re-examined using an intensity study of tropical cyclones crossing the Philippines (Sikora, 1976). For typhoons with maximum sustained winds of less than 80 kt (41 m/smc), the study shows that an average intensification of 30 kt (15 m/sec) can be expected for tropical cyclones which follow a track similar to Mac's. Reanalysis of the period between 1518002 and 1800002 shows, in fact, that Mac intensified to typhoon intensity before weakening from frictional effects over Catanduanes Island on 18 September (Fig.

The unexpected development of a second tropical cyclone in the South China Sea (SCS) produced a series of track and intensity modifications in Typhoon Mac. Upon exiting the Philippines, Mac, which was originally forecast to track west-northwest into the SCS, began a Fujiwhara interaction (Fig. 3-18-2) with the rapidly developing Tropical Storm Nancy located near Hai-nan Island. Instead of tracking west-northwest, Mac tracked north-northwest, skirting Cubi Point Naval Air Station, Philippines, on his new track toward Hong Kong. Strong anticyclonic outflow from Nancy sheared Mac's convection towards the southwest with aircraft reconnaissance reporting an exposed low-level circulation of 30-35 kt (15-18 m/sec) intensity on the 20th.

Weak steering currents allowed Nancy to take a cyclonic track across southern Hai-nan Island before heading southwestward into Vietnam. Nancy's southwestward track towards landfall forced Mac further north than originally forecast. Mac eventually passed just south of Hong Kong. Ironically, Nancy's development, which caused Mac to track towards Hong Kong, also helped to spare Hong Kong from potential typhoon force winds. Nancy's upper-level outflow, which dominated the SCS from 19-23 September, produced strong vertical shear over Mac and slowed his rate of reintensification. Typhoon Mac only reached minimal tropical storm intensity prior to making landfall west of Hong Kong.



FIGURE 3-17-1. Typhoon Mac after crossing Catanduanes Island, Philippines, 18 September 1979, 00382. (DMSP imagery)



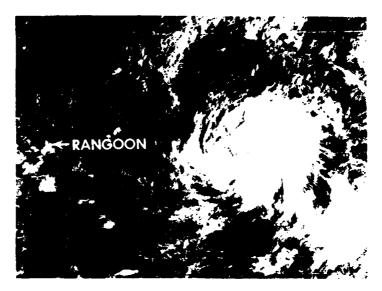
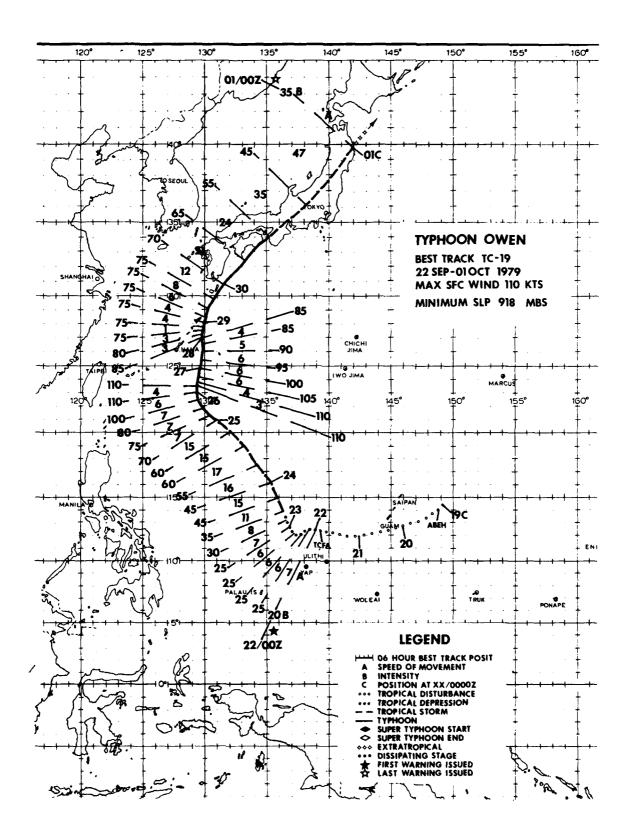


FIGURE 3-18-1. Tropical Storm Nancy at 35 kt [18 m/sec] intensity just after landfall on the southern end of Hai-nan Island, 20 September 1979, 01432. (DMSP imagery from Det 8, 1WW, Kadena AB, Okinawa)



FIGURE 3-18-2. Typhoon Mac and Tropical Storm Mancy undergoing Fujiwhara interaction over the South China Sea, 22 September 1979, 03022. The 48-hour tracks before and after picture time are superimposed (Dots bracket 24-hour intervals). (DMSP imagery from Det 5, 1WW, Clark AB, RP)



### TYPHOON OWEN (19)

Typhoon Owen developed from a disturbance which tracked south of Guam during 20 September 1979. Two days later, satellite imagery (Fig. 3-19-1) showed that the system was organizing at the same time that aircraft reconnaissance data indicated a definite surface circulation with a 1000 mb central pressure. This prompted JTWC to issue a tropical depression warning or the system at 2200002.

During the 2 days prior to and 1 day after 22 September, the system moved on a generally westward track at 5 to 8 kt (9 to 15 km/hr). This speed and direction was in good agreement with climatological tracks. Also, the 500 mb analysis showed a strong subtropical ridge which indicated westward steering. Based on this information, JTWC forecast westward movement for the first 8 warnings. However, Owen unexpectedly turned sharply to the north and began moving at speeds of 15 kt (28 km/hr).

Post-analysis revealed a possible reason for this movement. Figure 3-19-2 shows

the 2212002 analyses at 500 mb and 200 mb superimposed. An upper-level trough is evident on the 200 mb analysis just west of the cyclone. Southerly winds of 50 kt (26 m/sec) were observed on the eastern periphery of the trough. Considerable vertical shear existed in the layer from 500 mb to 200 mb. It appears that the steering and depth of this upper-level trough rather than 500 mb steering was the dominant feature in Owen's movement. Under its influence, Owen tracked generally northward throughout his lifetime, although undergoing major changes in speed. He slowed to a barely perceptible 1-kt (2 km/hr) movement just northeast of Okinawa (at the latitude of the subtropical ridge axis) and then dramatically accelerated to 24 kt (44 km/hr) 36 hours later under vertically consistent westerly steering. At this time, Owen made landfall near Osaka, Japan and began weakening in intensity while still accelerating to 47 kt (87 km/hr). Eventually, he transitioned into an extratropical system but not before reaching a maximum intensity of 110 kt (57 m/sec) (Fig. 3-19-3) on 26 September.

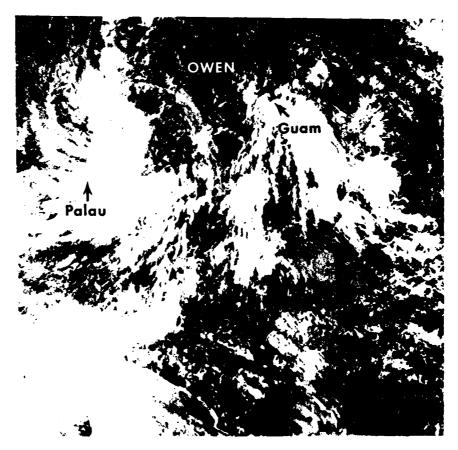


FIGURE 3-19-1. Typhoon Owen as a tropical disturbance, 21 September 1979, 23262. [DMSP imagery]

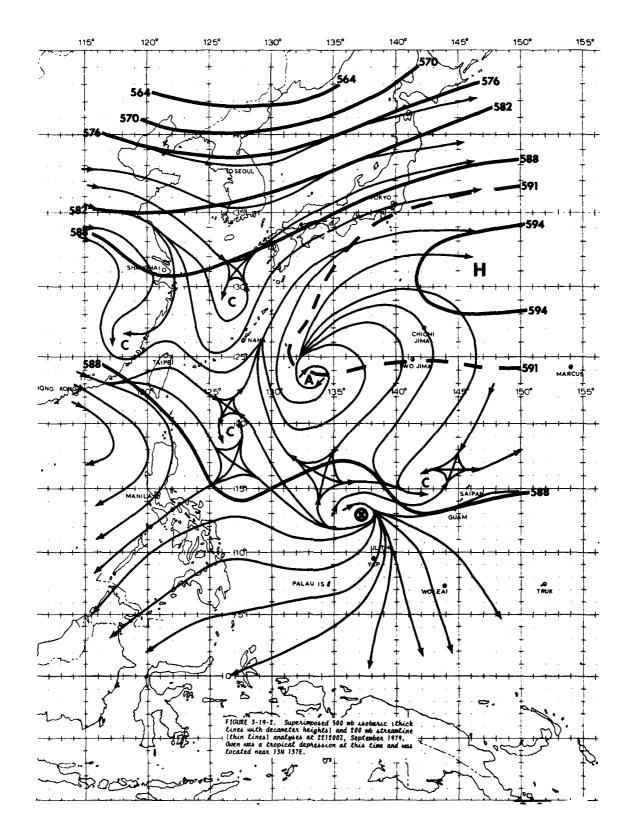
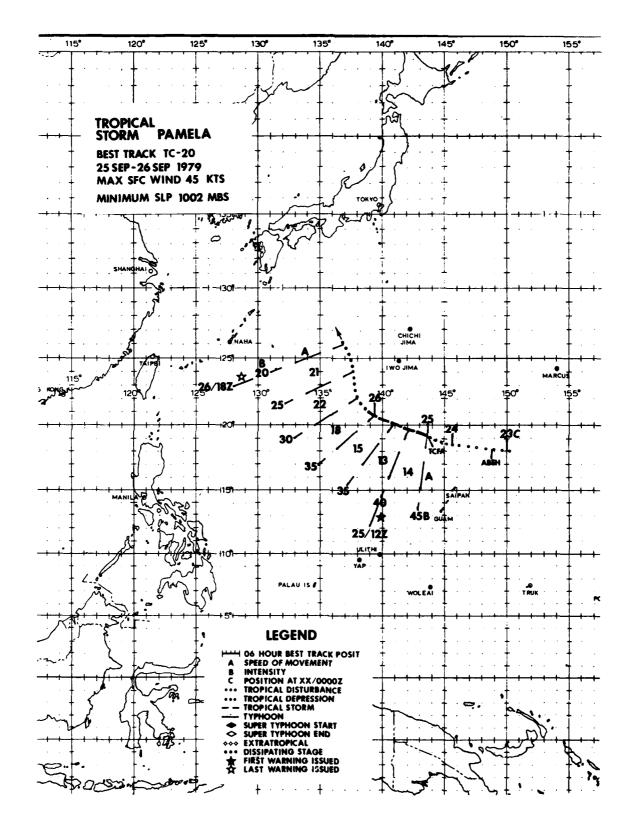




FIGURE 3-19-3. Typhoon Owen at maximum intensity of 110 kt (57 m/sec), 26 September 1979, 01452. (DMSP imagery)



## TROPICAL STORM PAMELA (20)

Developing at the apex of a wave in the easterly flow in late September 1979, Tropical Storm Pamela tracked westward, north of the Mariana Islands, and dissipated in Typhoon Owen's eastern feeder band under strong vertical shear (Fig. 3-20-1).

A JTWC pressure-wind relationship study (Atkinson and Holliday, 1977) suggested TS Pamela's maximum intensity should have ranged between 25-30 kt (13-15 m/sec) for the concomitant 1002-1003 mb minimum sealevel pressure reported. Instead, aircraft data at 250827Z reported a very narrow,

transient wind band of 60 kt (31 m/sec) north and east of the surface center. The ARWO on this mission indicated that surface winds may have been even higher than the reported 60 kt (31 m/sec). Subsequent aircraft investigations were not able to locate winds greater than 25 kt (13 m/sec). The occurrence of maximum winds which exceed the range of the JTWC tropical cyclone pressure-wind relationship is encountered several times each season. Although several explanations have been offered for these anomalies, none have been substantiated.

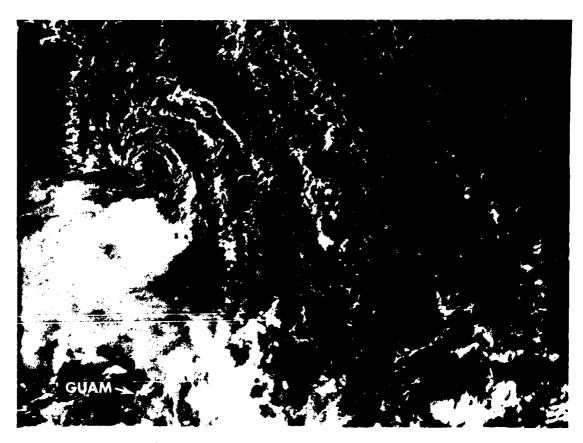
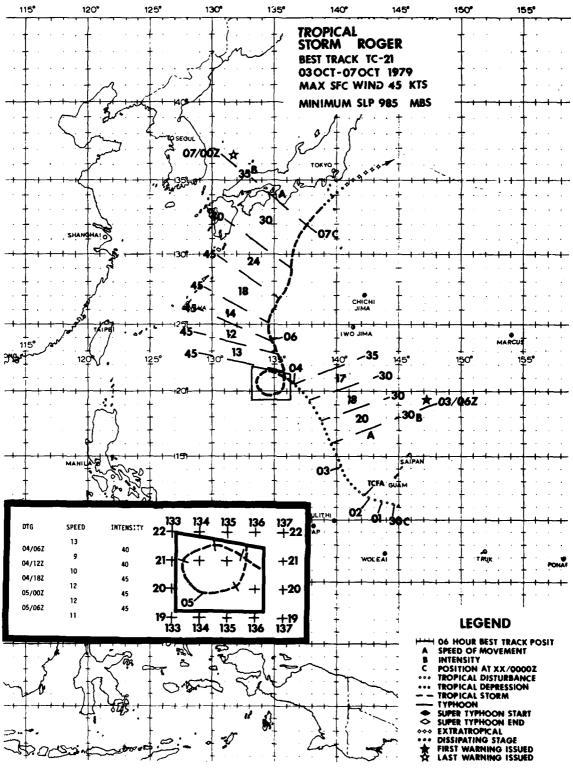


FIGURE 3-20-1. Tropical Storm Pamela with maximum sustained winds of 45 kt [23 m/sec], 24 September 1979, 22327. The exposed low-level circulation was a result of strong vertical shear produced by Typhoon Owen. (DMSP imagery)



## TROPICAL STORM ROGER (21)

As Typhoon Owen began recurving toward Japan, activity increased in the monsoon trough that extended over the Caroline Islands. The increased activity was noted in the Significant Tropical Weather Advisory (ABEH PGTW) on 28 September. For the next 5 days, 2 weak surface circulations and associated cloud clusters within the broad trough, one southwest of Guam and the other southeast of Guam, were closely monitored. As Owen began weakening over Japan, the southwest monsoon flow into the trough oriented NW-SE increased on 30 September, and a line of strong convective activity developed from the southern Philippines to a position south of Guam.

Post-analysis indicated the existence of a weak circulation southwest of Guam which was to become Tropical Storm Roger. During the entire time preceding the issuance of the first warning on Roger, JTWC's attention was focused on another area of major convective activity 50 west of the circulation center which was associated with strong low-level convergence and cyclonic shear. Gradient-level winds at Yap of 56 kt (29 m/sec), Palau 52 kt (27 m/sec) and Guam 28 kt (14 m/sec) are indicative of the strong low-level winds around the periphery of the trough. Thus, the initial and the reissued formation alerts (0206002 Oct and 0222002 Oct) covered the area of heavy convective activity rather than the actual surface circulation center.

Numbered warnings began at 06002 on 3 October when a reconnaissance aircraft at

0302202 reported a surface pressure of 998 mb and estimated surface winds of 40 kt (21 m/sec) in a band of strong southwesterly flow 60 nm (111 km) south of the surface center. The aircraft also observed a calm wind center at the surface of 30 nm (56 km) in diameter with clear skies over the area.

Synoptic and satellite data at 031200Z indicated that TD 21 was beginning to separate from the broad trough as convective activity was becoming more directly associated with the circulation center (Fig. 3-21-1). TD 21 was upgraded to a tropical storm at 0600Z on 4 October based on 35 kt (18 m/sec) surface winds and a 982 mb sealevel pressure reported by aircraft reconnaissance at 040308Z. Post-analysis indicates tropical storm intensity was attained 6 hours earlier.

A break in the mid-tropospheric subtropical ridge north of Roger existed as Owen recurved over Japan. The strong mid-level southeasterly steering current along the southwestern periphery of the ridge was responsible for Roger's 15 to 20 kt (8 to 10 m/sec) northwestward movement. The ridge retreated eastward between 0000Z and 1200Z on 4 October as a mid-level trough deepened over Korea. The loss of definitive steering flow permitted Roger to execute a cyclonic After emerging from the loop, Roger loop. continued on a northwestward track until north of the ridge axis, after which he accelerated north-northeastward. Extratropical transition was complete by 0706002 as Roger merged with a cold front south of Japan.

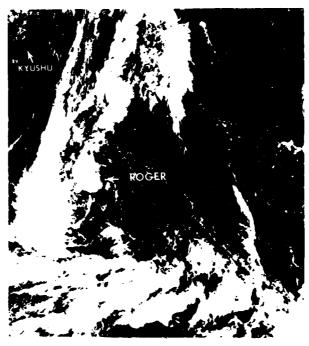
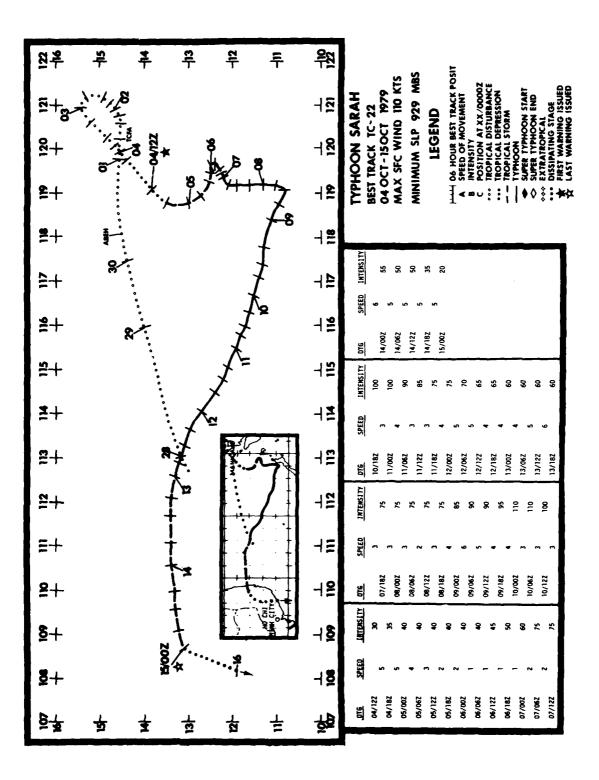


FIGURE 3-21-1. Tropical Storm Roger at 35 kt (18 m/sec) intensity 04 October 1979, 00542. (DMSP imagery)



Typhoon Sarah spawned in the monsoonal trough during late September 1979. trough extended from the southwestern portion of the South China Sea toward Luzon. A northeast monsoon surge existed north of the trough, while the southwest monsoon dominated the area south of the trough. circulation was steered initially by the southwest monsoon and then later by the first northeast surge of the fall from the Asian mainland. During the last few days of September, the circulation meandered slowly toward Luzon under the influence of the southwest monsoon, and then looped over Luzon during the first three days of October as a mid-tropospheric short-wave trough moved eastward north of Luzon. Once the short-wave trough had moved east of the circulation, the northeast surge intensified and became more of an influence as the circulation finished its loop and began its south-southwest track.

On 5 and 6 October, Sarah, now a tropical storm, apparently was again influenced by another mid-tropospheric short-wave trough which moved across Sarah's longitudinal position and induced the brief eastward movement in her track. At this time, the southwest monsoon also increased in intensity and may have been another factor in steering Sarah eastward. For almost the entire period that Sarah was tracking southward there was a weakness in the mid-tropospheric ridge between the Philippines and the Asian mainland, enabling Sarah's track to be influenced by short-wave troughs. This weakness in the ridge resulted in mid-tropospheric flow that was too weak to significantly affect the steering of Sarah. This weakness allowed the surface winds to dictate Sarah's direction of motion through the first 8 days of October. Figures 3-22-1 and 3-22-2 illustrate the surface and midlevel flow patterns which influenced Sarah during this phase of her track.

During Sarah's depression stage, strong easterlies in the upper-troposphere restricted Sarah's outflow to the northeast, thus inhibiting development into a tropical storm. As Sarah proceeded southward, the easterlies decreased in strength, outflow increased, and Sarah intensified to tropical storm and then typhoon strength. It is very interesting to note that Sarah intensified to typhoon strength while tracking southward which is quite unusual for a tropical cyclone. Several aircraft reconnaissance flights reported that Sarah had attained typhoon strength even though her cloud structure was not well organized.

During the first several days of October when Sarah was slowly developing to typhoon strength and moving south, Palawan Island and the central Philippines were battered by high winds and rain. These areas were inundated by flooding and landslides which caused massive crop damage and death. Many villages were cut off from any

source of food, fresh water, and other necessities for survival. Four deaths were attributed to Sarah. On 8 October, Sarah finally began to track westward and the weather finally cleared over Palawan Island and the central Philippines. Sarah's change in track was due to the strengthening of the mid-tropospheric ridge north of Sarah from Luzon across the South China Sea into Asia. Aircraft reconnaissance early on the 9th reported that Sarah's structure had become better organized. Earlier aircraft reported that Sarah was not vertically aligned; but on the 9th, the mid-level center had become vertically aligned with the surface center. With vertical alignment and improved upperlevel outflow, Sarah's intensity increased to 110 kt (57 m/sec) as she became a most impressive storm. This is in contrast to her unusual origin.

After Sarah reached peak intensity early on 10 October, she began to slowly weaken as

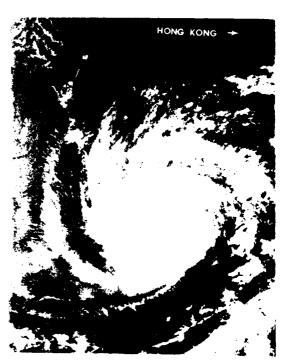
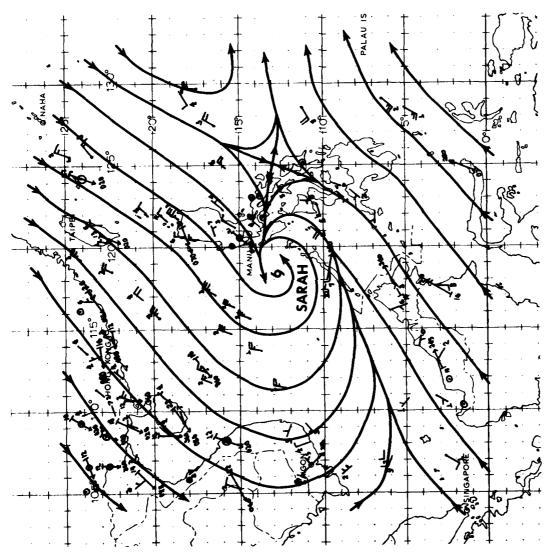


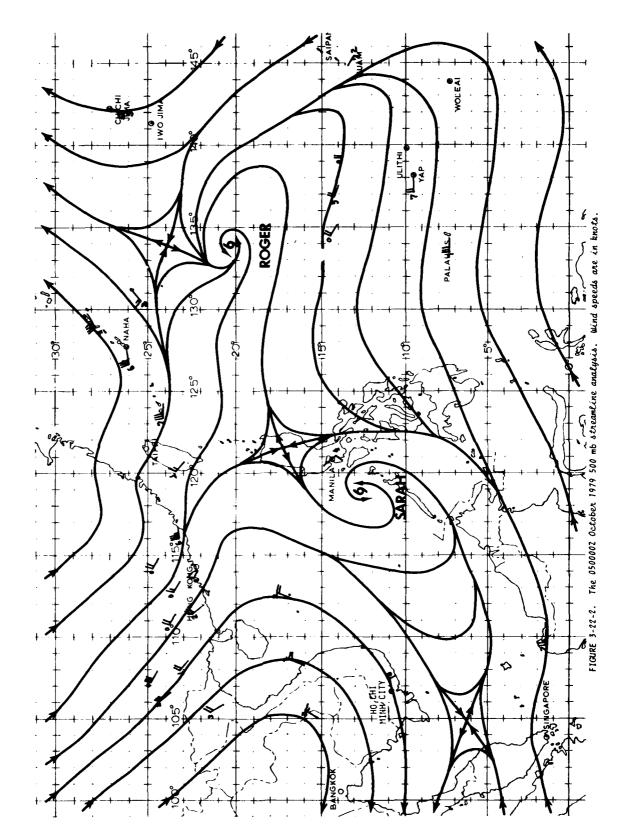
FIGURE 3-22-3. Sarah with 60 kt (31 m/sec) intensity one day prior to landfall over Vietnam, 13 October 1979, 01362. (DMSP imagery)

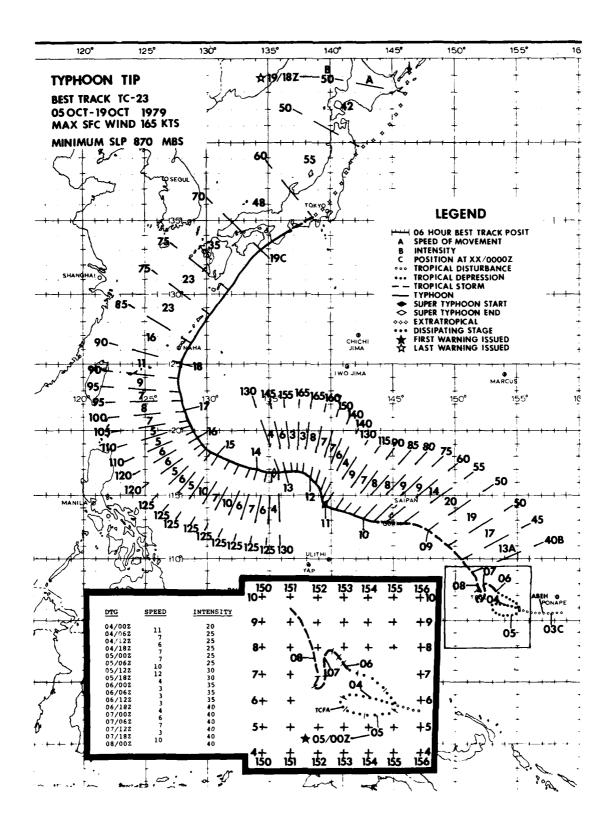
she tracked west-northwestward (Fig. 3-22-3). Sarah continued on a west-northwest track until dissipation over Vietnam on 17 October. After 20 days, she dissipated within 300 nm (556 km) of her origin as a monsoon depression on 28 September.

FIGURES 3-22-1 and 3-22-2 are on following pages.



[]/gradient-level (ddd ——{66) wind data and streamline





Super Typhoon Tip was the most significant typhoon of the 1979 season, and possibly the most significant tropical cyclone this century. Forty aircraft reconnaissance missions were flown on Tip, which produced 60 fixes, and thus made it one of the most closely watched cyclones in recent memory. Aircraft and synoptic data showed that Tip achieved the lowest sea-level pressure ever observed in a tropical cyclone (870 mb) and also had the largest circulation pattern on record (nearly 1200 nm (2222 km) in diameter).

Satellite and synoptic data during the early part of October revealed an active monsoon trough that extended from the Marshall Islands through the Caroline Islands to Luzon. Three distinct circulations developed in this trough: One near Manila, which would become Typhoon Sarah; another southwest of Guam, which would become Tropical Storm Roger; and the last between Truk and Ponape, which was destined to become Super Typhoon Tip.

It is not possible to discuss the development of Tip without, at the same time, examining the development of TS Roger. The surface analysis for 030000Z showed the three circulations in the monsoon trough with strong cross-equatorial flow, most of which was feeding into TS Roger. This situation was enhanced, in part, by an extratropical trough north of Roger over Southern Japan. The split in the surface flow pattern hear Guam tended to keep Tip from developing rapidly while southeast of Guam. The upperlevel analysis at the same time showed a large anticyclone north of Guam in close association with TS Roger and a developing TUTT cell about 300 nm (556 km) east of Marcus Island. The TUTT cell was moving slowly westward. Only strong upper-level northeasterlies existed over Truk and Ponape.

The satellite signature of the tropical disturbance near Truk continued to show improvement despite the initially unfavorable upper-air pattern. A Tropical Cyclone Formation Alert was issued at 040900Z, when a reconnaissance aircraft found a closed surface circulation about 120 nm (222 km) southeast of Truk with a MSLP of 1003.9 mb and a maximum observed surface wind of 25 kt (13 m/sec).

A reconnaissance aircraft fixed the disturbance the following day about 100 nm (185 km) southeast of the previous position. Based on indications of continual development, the first warning on TD 23 was issued at 050000Z. Although the surface pressure did not drop significantly, the observed surface winds did increase, and as a result, TD 23 was upgraded to Tropical Storm Tip at 060000Z.

During the period from 0500002 to 0718002, TS Tip gave the JTWC forecasters a striking example of what the term "erratic movement" really means. TS Tip first executed a cyclonic loop southeast of Truk, then accelerated to the northwest, only to stall and meander to a position south of Truk. It was difficult to keep track of

TS Tip's surface position during this period. The best track is based almost entirely on aircraft surface positions, because the satellite fixes were based on upper-level outflow centers, and even the 700 mb center, as observed by aircraft reconnaissance, was considerably displaced from the surface center. Changes in the surface wind direction reported by Truk assisted JTWC in monitoring TS Tip during this period of erratic behavior.

Post-analysis shows that Tip's slow development and early erratic behavior are related to the weak, yet extensive circulation patterns that were associated with TS Roger. While near Truk, TS Tip was still competing with TS Roger for strong southerly surface inflow and, until the 8th, was coming out second best. During the period of erratic movement, JTWC continued to forecast a northwestward track with p.ssage south of Guam. These forecasts were based primarily on the mid-level steering winds observed at Guam and obtained by the reconnaissance aircraft. These fairly strong winds were from the southeast and were expected to steer Tip toward Guam. However, at this stage of development, Tip was evidently too far south of this wind band and the steering in the immediate vicinity of Tip remained weak.

On 8 October, the expected northwest movement began. Roger was far to the north becoming extratropical, and the southerly winds that had been flowing north began to veer toward Tip. The TUTT cell earlier near Marcus Island migrated to a position northwest of Guam, affording Tip an excellent outflow channel to the north. Synoptic and subsequent aircraft data revealed that the southeasterly mid-level winds finally began to influence TS Tip, and the 080208Z aircraft fix confirmed that Tip was heading toward Guam at approximately 13 kt (24 km/hr). The minimum sea level pressure dropped to 995 mb and surface winds were 40 kt (21 m/sec).

Tropical Storm Tip continued to intensify and accelerate, eventually to 20 kt (37 km/hr) as he headed toward Guam. Until 6 hours before reaching Guam, Tip's persistence track and JTWC's forecasts indicated that he would pass directly over the center of the island. Six hours before expected landfall, however, reconnaissance aircraft and radar positions from Andersen AFB showed that TS Tip had turned to the west. Tip actually passed south of Guam, reaching CPA at about 25 nm (46 km) south of the southern end of the island at 091015Z. Maximum winds of 48 kt (25 m/sec) with gusts to 64 kt (33 m/sec) were recorded at the Naval Oceanography Command Center on Nimitz Hill. Andersen AFB recorded 6.5 inches of rain between 081800Z and 091800Z, and an additional 2.61 inches between 091800Z and 091900Z.

Shortly after passing Guam, Tip reached typhoon strength and continued on a basic west-northwest track. The analyses over the next few days showed that Typhoon Tip was moving into an area of strong upper-level divergence which appeared to cover most of

the western Pacific. Kypid intensification was forecast based upon the favorable upper-level pattern and the continued drop in surface pressure as observed by the reconnaissance aircraft. Intensification was much more rapid than expected, however, as the pressure between the 9th and the 11th dropped 98 mb to 898 mb. Tip reached super typhoon strength at that time with maximum winds of 130 kt (67 m/sec) reported by aircraft reconnaissance. The surface analyses revealed that the circulation pattern associated with Typhoon Tip had increased to a diameter of 1200 nm (2222 km) which broke the previous record of 720 nm (1333 km) set by Typhoon Marge in August 1951.

Super Typhoon Tip intensified still further, and at 120353Z, a reconnaissance aircraft recorded the lowest sea-level pressure ever observed in a tropical cyclone: 870 mb. This was 6 mb lower than the previous record set by Super Typhoon June in November 1975. The 700 mb height was 1944 meters and the 700 mb temperature within the eye was an exceptionally high 30° C (Fig. 3-23-1). The Aerial Reconnaissance Weather Officer (ARWO) on that particular mission remarked that "...one unusual feature was the spiral striations on the wall cloud. It looked like a double helix spiraling from the base of the wall cloud to the top, making about two revolutions in

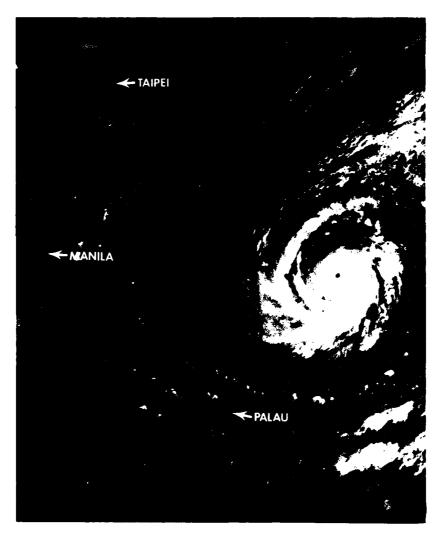


FIGURE 3-23-1. Super Typhoen Tip shortly before the record MSLP of 870 mb was observed by reconnaissance aircraft, 12 October 1979, 00122. (DMSP imagery).

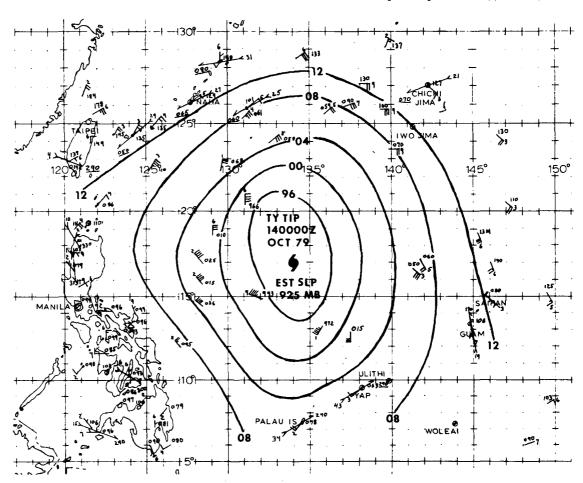
climbing." 1 Tip maintained super typhoon strength for the next 54 hours while moving to the northwest at between 3 and 7 kt (6 and 13 km/hr). Estimated maximum wind intensity of 165 kt (85 m/sec) was reached at 120600z.

The immense circulation pattern associated with Typhoon Tip extended from the surface through 500 mb (and probably higher) and essentially split the subtropical midtropospheric ridge south of Japan. This would have allowed an average typhoon to recurve sharply to the north, but Tip was an atypical system and the northwestward movement persisted for the next three days.

Steering forecast aids were useless during this period because they merely steered Tip in his own large storm-induced flow. Persistence and climatology became the primary forecast aids during this stage in Tip's life.

SALES TO MAKE AREA SALES

From the 13th to the 17th, the radius of surface and gradient-level 30 kt (15 m/sec) or greater winds extended over 600 nm (1111 km) from Typhoon Tip's center. The radius of over 50 kt (26 m/sec) winds was over 150 nm (278 km) (Fig. 3-23-2). The aircraft reconnaissance data likewise showed that 700 mb winds of 105 kt (54 m/sec) existed more than 120 nm (222 km) from Tip's center during this period (Fig. 3-23-3).



1PATRICK W. GIESE, Capt, USAF: Mission ARWO.

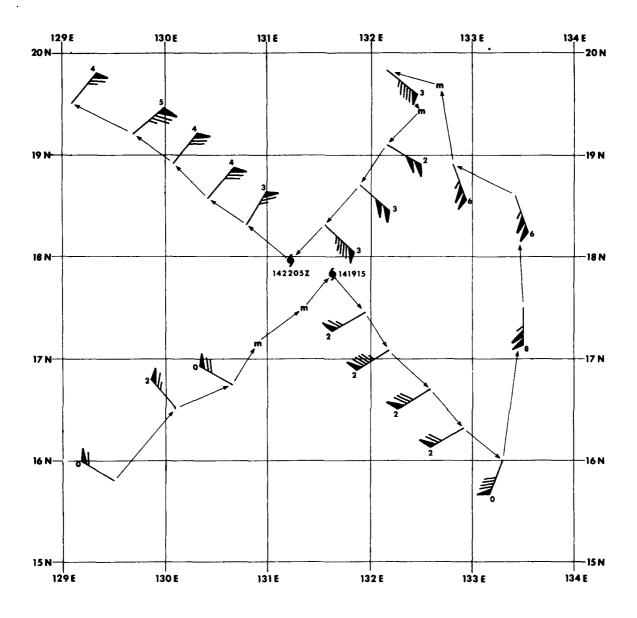


FIGURE 3-23-3. Plot of aircraft reconnaissance data from the 26th mission into Super Typhoon Tip on 15 October 1979. Tip's positions were fixed at 1419157 and 1422052. Wind barbs are the measured 700 mb winds. The tens digit of the wind direction is also plotted with the wind barbs. An "m" indicates no 700 mb wind data available.

After the 17th, Tip began to weaken as the large circulation pattern began to shrink. This, together with the effects of a mid-level trough moving toward Japan from China, caused Tip to begin tracking northward. By the 18th, he was accelerating to the northeast under the influence of the increased mid-level southwesterlies.

Ouring recurvature, Tip passed within 35 nm (65 km) of Kadena AB on Okinawa, which reported maximum sustained winds of 38 kt (20 m/sec) with gusts to 61 kt (31 m/sec).

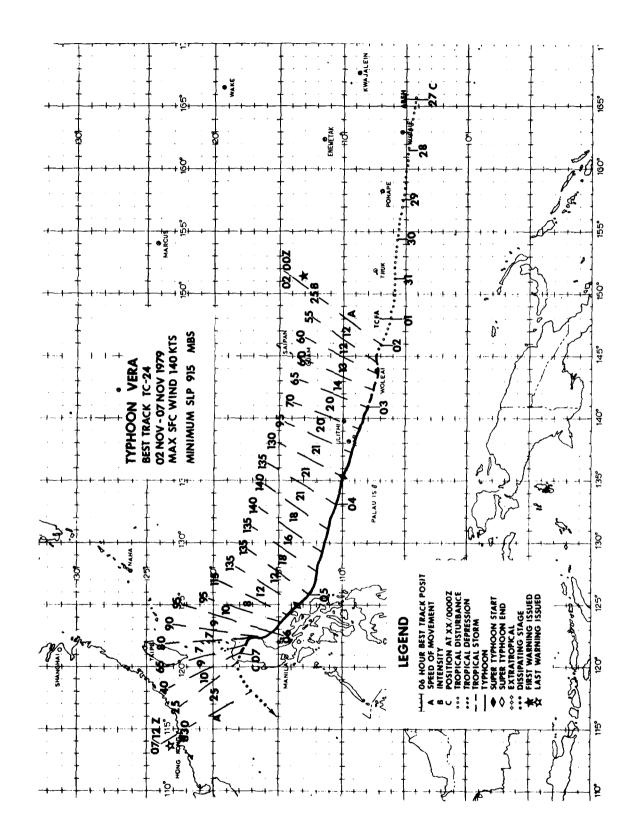
At approximately 190100Z, after reaching a forward speed of between 35 and 45 kt (65 and 83 km/hr), Typhoon Tip, with maximum winds of 70 kt (36 m/sec), made landfall on the Japanese island of Honshu, about 60 nm (111 km) south of Osaka. Synoptic and radar data from stations on the island showed that Tip maintained a speed in excess of 45 kt (83 km/hr) as he passed to the north of Tokyo and eastward into the Pacific Ocean. According to satellite imagery, Tip completed extratropical transition over Honshu.

The extratropical low pressure center (the remnants of Tip) maintained winds of storm force, 48 kt (25 m/sec), until the 21st when it moved to a position east of Kamchatka and finally began to fill rapidly.

The majority of the severe damage occurred in Japan where the agricultural and fishing industries sustained losses into the millions of dollars. Flooding from Tip's rains also breached a fuel retaining wall at Camp Fuji, west-northwest of Yokosuka. The fuel caught fire causing 68 casualties, including 11 deaths, among the U.S. Marines stationed there.

Considering the size and strength of Super Typhoon Tip, the Western Pacific faired well. Luckily, the maximum intensity was reached while the system was still far from any inhabited areas. The potential for mass destruction was always there, but from a strictly meteorological standpoint, Tip was also a thing of great beauty. One of the Aerial Reconnaissance Weather Officers stated, shortly after she returned from a mission, that "...the second penetration was beyond description. This is unquestionably the most awe-inspiring storm I have ever observed. In the 2½ hours that transpired between the first and second fixes, the moon had risen sufficiently to shine into the eye through an 8 nm clear area at the top of the eyewall. To say it was spectacular is totally inadequate...'awesome' is a little closer."

1CAROL L. BELT, 1LT, USAF: Mission ARWO.



Vera, the fourth and final super typhoon of 1979, originated in an active near-equatorial trough (NET) which extended through the Caroline and Marshall Islands. Vera was first analyzed as a weak surface circulation 100 nm (185 km) southeast of Ponape on 27 October and was included on JTWC's Significant Tropical Weather Advisory (ABEH PGTW) for the next 4 days as it remained in the NET. Low-level inflow during this period was split between several weak eddies.

By 3000002, synoptic data indicated that the low-level inflow was now concentrated into the developing cyclone. Meanwhile, the convective activity increased rapidly over a 24-hour period from 3100002 to 0100002. A Tropical Cyclone Formation Alert was issued at 0100002 November based on increased upper-level outflow and a continued decrease in surface pressure.

Aircraft reconnaissance at 012100Z found an ill-defined circulation center with a central pressure of 1004 mb and estimated surface winds of 15 kt (8 m/sec). Numbered warnings began at 020000Z based on an improved satellite signature. Rapid intensification occurred, and TD 24 was upgraded to Tropical Storm Vera 6 hours later. Vera continued to intensify, reaching typhoon strength by 0000Z on 3 November while 190 nm (352 km) south-southeast of Yap. At this time, the 200 mb analysis revealed that a large upper-level anticyclone, previously located northwest of Vera at 010000Z, was weakening and was no longer restricting Vera's outflow to the north. By 020000Z, the anticyclone situated over Vera had become the dominant upper-level synoptic feature over the western Pacific.

From the time of the first warning until her approach to the Philippines northeast of Samar, Vera moved on a virtually straight west-northwest track. The major influence on her movement was the unusually strong mid-tropospheric subtropical ridge over the western Pacific. The strength of the easterly current south of the ridge steered Vera at forward speeds of 20 to 22 kt (37 to 41 km/hr)--almost twice the climatological average--as she passed 35 nm (65 km) south of Yap. As a result, although JTWC's forecast tracks were consistent and accurate, forecast forward speeds lagged behind Vera's actual speeds. The underestimates were considerable during the early stages of acceleration.

Vera continued to intensify during her west-northwestward acceleration and reached super typhoon intensity only 18 hours after being upgraded to a typhoon. Reconnaissance aircraft reports indicated Vera maintained super typhoon strength for over 24 hours before weakening as she approached Catanduanes Island. The peak wind reported on Catanduanes Island was 50 kt (26 m/sec) at 0512002 as Vera passed just off the coast.

The island chain began restricting low-level inflow as Vera continued northwestward toward northern Luzon. Vera made landfall north of Tarigtig Point packing winds of 90 kt (46 m/sec).

After landfall, the onset of enhanced low-level northeasterly flow over the Taiwan Straits coupled with strong upper-level southwesterlies over the Philippines resulted in vertical disorganization and rapid weakening of Vera. Radar and aircraft reports indicated the low-level circulation continued to track northwestward over the Cagayan River valley and exit into the South China Sea near Culili Point south of Laoag. The upper-level circulation sheared off near Tuguegarao and was tracked using satellite imagery northward over Aparri then east-northeastward into the Philippine Sea. Surface synoptic and ship reports at 0700002 indicated that a secondary surface center existed near Baguio. At the same time, the primary center was crossing the Cordillera Central Mountain range 95 nm (176 km) to the north (Fig. 3-24-1).

After exiting into the South China Sea, the strong northeast monsoon flow accelerated Vera southwestward, and the final warning was issued at 1200Z on the 7th downgrading Vera to a tropical depression.

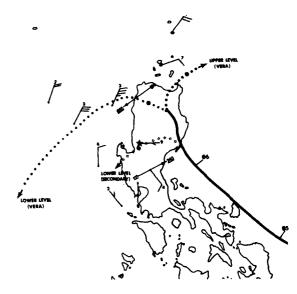
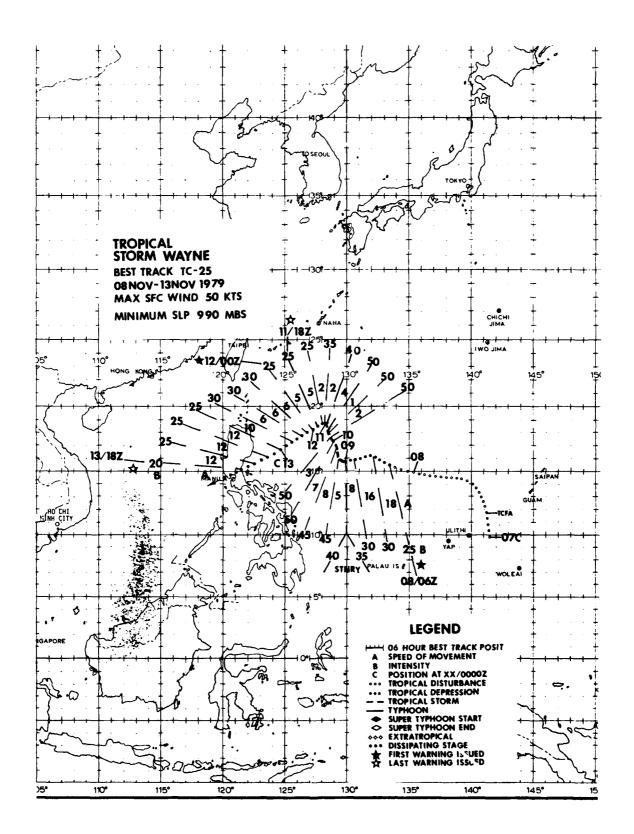


FIGURE 3-24-1. Tracks of low-level and upper-level centers after the upper-level sheared off over northern luzon. Synoptic and ship reports at 0700002 November indicate secondary low-level center near Baguic (WMO 98328) (indicated by a star). The 0700002 center positions are indicated by solid dots. Wind speeds are in knots.



## TROPICAL STORM WAYNE

Tropical Strom Wayne was first detected as a mid-level circulation on satellite imagery in early November. Figure 3-25-1 shows the broad cloud structure associated with the system. Aircraft reconnaissance around this period showed that the disturbance was most developed at mid-levels. Wayne moved northward initially and began developing a more definitive surface circulation which became evident in synoptic data on 7 November. Wayne lasted only a relatively short time, but he still proved to be one of the more difficult storms to forecas: for 1979.

JTWC's first forecasts called for recurvature. They were based on the 080000Z November 500 mb synoptic situation which showed a weakness in the subtropical ridge with westerlies extending south to 23<sup>ON</sup> latitude. Steering flow at all levels, however, was not consistent and strong low-level easterlies prevented Wayne from recurving toward the east. On 9 November, an extratropical system with accompanying surface frontogenesis developed north of Wayne. This caused a break in the otherwise persistent easterly flow and Wayne began to track northward. JTWC forecasts again reflected recurvature and called for early dissipation due to the strong shear from low-level easterlies and upper-level westerlies. The extratropical system moved rapidly eastward bypassing Wayne. By 11 November, strong northeasterlies had once again been established, and Wayne turned back to the west, ultimately, tracking west-southwest toward the central

Thilippines. At the same time, strong shear did weaken Wayne as it tracked toward the Philippines (Figure 3-25-2) and dissipation occurred as he made landfall over Luzon.

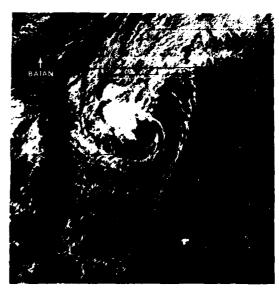


FIGURE 3-25-2. Tropical Storm Wayne weakening due to strong shear as it approached the Philippines, 12 November 1979, C1002. (DMSP imagery)

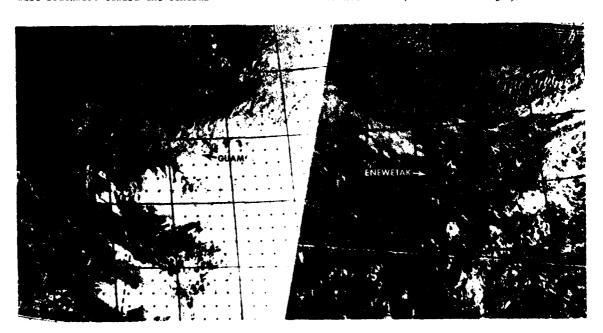
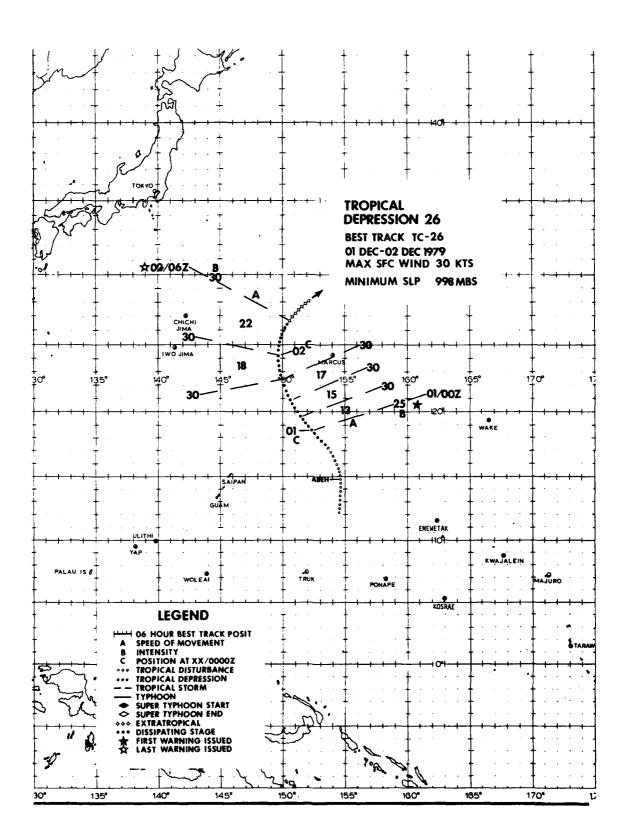


FIGURE 3-25-1. Disturbance stage of Tropical Storm Wayne when the system was mainly a mid-level circulation, 6 November 1979, 12082. (DMSP imagery)



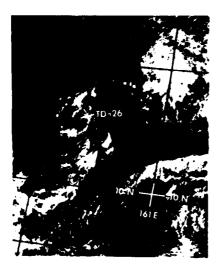


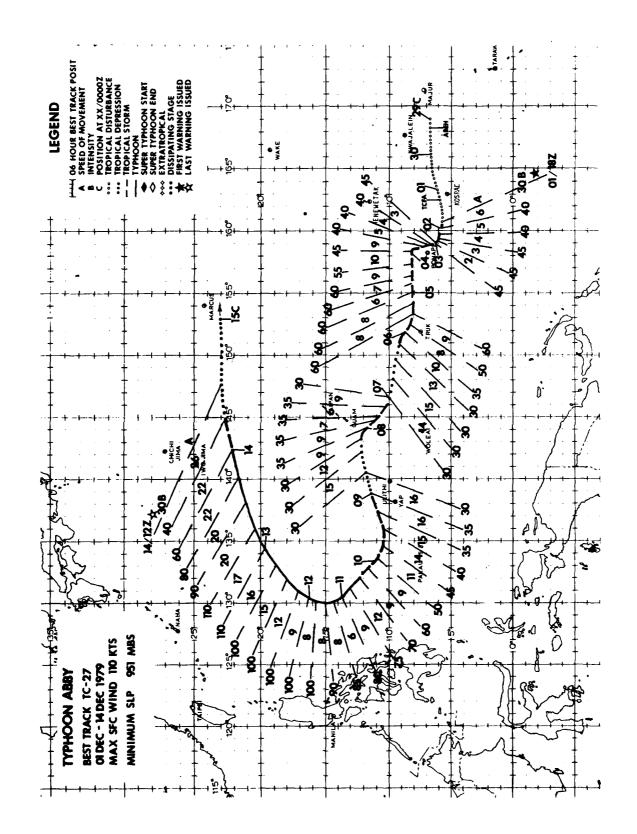
FIGURE 3-26-1. Tropical Depression 26 developed north-northeast of the Truk Islands and appeared to be the surface reflection of a mid-level circulation. Surface data suggest the existence of a weak circulation 400 nm (741 km) northeast of Tropical Depression 26 and a broad circulation (Typhoon Abby) to the southeast, 29 November 1979, 22552. (DMSP imagery)



FIGURE 3-26-3. Tropical Depression 26 passed west of Marcus Island and merged with an extratropical frontal boundary. Tropical Depression 26 sheared in the vertical with the low-level exposed surface circulation remaining on the western edge of the convection, 2 December 1979, 00362. (DMSP imagery)



FIGURE 3-26-2. Tropical Depression 26 developed an identifiable surface circulation and intensified as it tracked north-northwestward. A ship, transiting the area, passed through the storm center and reported 35 kt (18 m/sec) winds in heavy showers. Based on synoptic data, the first warning was issued on Tropical Depression 26, but 35 kt-or-greater winds were never reported again. This photo shows Tropical Pepression 26 at its maximum convective intensity, 30 November 1979, 22372. (DMSP imagery)



Abby, the last typhoon of the 1979 season, developed over the Marshall Islands during early December. Abby proved to be an unusual cyclone in several ways. Throughout much of Typhoon Abby's existence, Abby was not vertically aligned. Aircraft reconnaissance located the mid-level circulation center displaced as much as 55 nm (102 km) from the surface center. At one point, two centers were identified; a point to be discussed later. In addition, Abby fluctuated between tropical depression and tropical storm strength several times before reaching typhoon strength 10 days after formation.

Within 24 hours of the first warning, aircraft reconnaissance observed surface winds of 45 kt (23 m/sec) and a sea-level pressure of 996 mb. The surface and 700-mb centers were displaced by 12 nm (22 km). Abby continued to intensify to 60 kt (31 m/sec) on 4 October while increasing the displacement between the surface and 700-mb centers.

Abby deviated from a westward track to a north-northwestward track on 3 December with a reduced forward speed of movement. The temporary northward movement was associated with a deepening mid-tropospheric trough which moved rapidly northeastward away from Japan on 1 December. Abby resumed a westward track with increased forward speed after the trough axis passed east of Abby late on the 3rd.

All available information (climatology, analog aids, analyses and numerical foreindicated continued intensification as Abby tracked towards Guam. This expected intensification was reflected in JTWC warnings during this period. However, the opposite occurred. As Abby moved west of Truk, she weakened to less than tropical storm strength. An upper tropospheric anti-cyclone north of Abby restricted Abby's outflow and resulted in the observed we ing (Fig. 3-27-1). By 7 December, Abby reintensified to minimum tropical storm strength as she moved westward and away from the influence of the restricting anticyclone. Abby then tracked west-northwestward under the influence of a mid-tropospheric long-wave trough oriented along 142E. As the trough moved east of Abby, the subtropical midtropospheric ridge again built eastward, providing a mechanism which steered Abby towards the west-southwest. During the 8th, Abby once again weakened to less than tropical storm strength and increased her forward speed of movement.

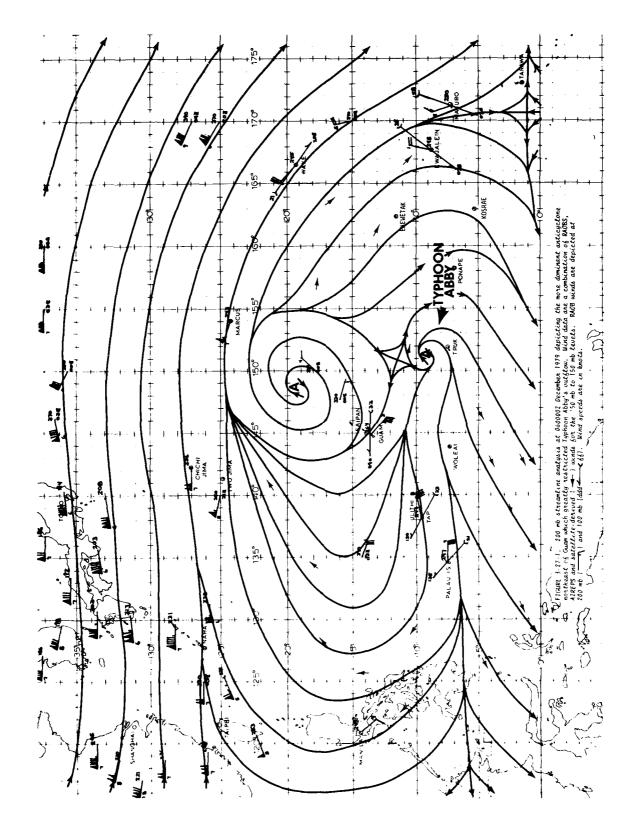
Abby was not vertically aligned from the issuance of the first warning through the 9th. On the 9th, aircraft reconnaissance making a supplemental fix at 0617Z observed that Abby possessed multiple 700 mb centers. By the time of entry into Abby for a levied 0830Z fix, only one well organized, intensifying center was found. The following is a storm mission summary by the Aerial Reconnaissance Weather Officer (ARWO), who made the double penetration into Abby: "This mission started out as a normal fix but ended

FIGURE 3-27-1 is on following page.

up being unusual. On our way inbound for the supplemental fix, there was no problem reading winds at flight level or on the surface. Winds were 20-25 kt the entire way. An area of thunderstorm activity became visible ahead of us. As we neared it, the doppler indicated that the 700 mb center was in the middle of the thunderstorm Not eager to go find this out, we went have to find the surface center. Enroute, we saw surface winds in excess of 35 kt which .ed us to a fairly disorganized surface certer just east of the main thunderstorm. 200 was a fairly small light and variable with center. Radar showed little curvature ... the shower pattern, but the surface was is did indicate a weak circulation existed of this first position. No weather existed to the east of our first fix, and this posit was right on the JTWC forecast track. the second fix, things had changed. As we came in the second time, we encountered considerable precipitation. Doppler and search radar indicated a center with a possible wall cloud forming considerably west of our first fix. Winds were stronger at flight level and we penetrated a wall cloud of about 80% coverage. When we broke through, we encountered our strongest winds at flight level. The surface center was under the eastern wall cloud with a small light and variable wind center at 700 mb centered in the eye. Lightning started in the eastern wall cloud and spread around the



FIGURE 3-27-2. Typhoon Abby's two outflow centers are indicated by arrows, 9 December 1979, 01442. (DMSP imagery) Figure 3-27-1 is on next page.



eye. Our drop was made as close to the surface center as was possible and indicated a good 988 mb sea-level pressure. The 700 mb height was down 72 meters from the first fix. The positions were 85 miles apart causing me to believe that two centers existed for a short time with the latter becoming the predominate one. The pressure profile seems to indicate this theory...."1 Satellite imagery at 090144Z also indicated the possible existence of multiple outflow centers (Fig. 3-27-2). While Abby was reorganizing into a single center, she began to reintensify to tropical storm strength. By the 10th, Abby had attained typhoon strength which made her the last typhoon of the decade.

A mid-tropospheric short-wave trough moved from mainland China into the Sea of Japan and deepened on the 10th. In response to the short-wave trough, the subtropical mid-tropospheric ridge again receded eastward north of Abby. The interaction of these two synoptic features allowed Abby to again track northwest. On the 11th, Typhoon Abby recurved in response to another mid-tropospheric short-wave trough, which extended further south than the trough on the 10th. This last trough in the series moved into the northern part of the South China Sea and deepened, causing Abby to finally follow a recurvature track.

Typically, recurving typhoons have their maximum intensities either less than 12 hours after recurvature or prior to recurvature (Riehl, 1971). Abby, however, did not reach maximum intensity until 36 hours after recurvature. By 13 December, Typhoon Abby reached maximum intensity of 110 kt (57 m/sec) with a minimum sea-level pressure of 951 mb (Fig. 3-27-3). As Abby continued toward the east-northeast, she approached a regime of very strong westerlies in the middle-and upper-troposphere. The strong westerlies induced Abby's acceleration

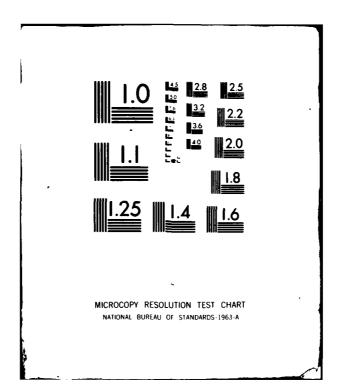
and rapid weakening. Abby dissipated on the 14th due to strong vertical shear between the surface and middle levels.

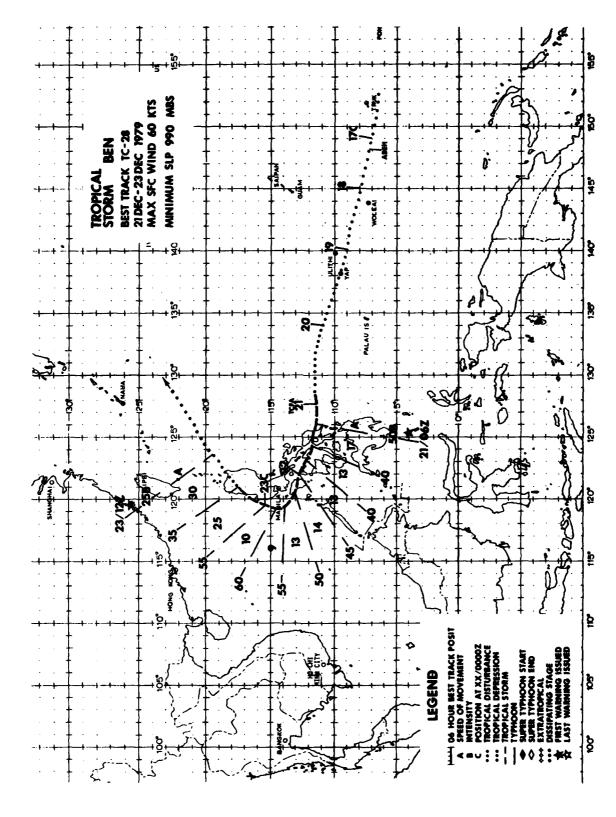


FIGURE 3-27-3. Typhoen Abry just after recurvature, 12 December 1979, 00:12. (DMSP imagery)

 $<sup>^{\</sup>dagger}$  CHARLES B. STANFIELD, Capt. USAF: Midsion ARWO.

NAVAL OCEANOGRAPHY COMMAND CENTER/JOINT TYPHOON WARNI--ETC F/6 %/2 ANNUAL TYPHOON REPORT 1979.(U) 1979 J W DIERCKS, J K LAVIN, J H BELL AD-A082 071 UNCLASSIFIED NL ≟⊹:3 5 0





esc. p.



FIGURE 3-28-1. Tropical Storm Ben at 40 kt {21 m/sec} intensity, 21 October 1979, 00592.
Ben was the last tropical cyclone in the western North Pacific during 1979. (DMSF imagery)

## 2. NORTH INDIAN OCEAN TROPICAL CYCLONES

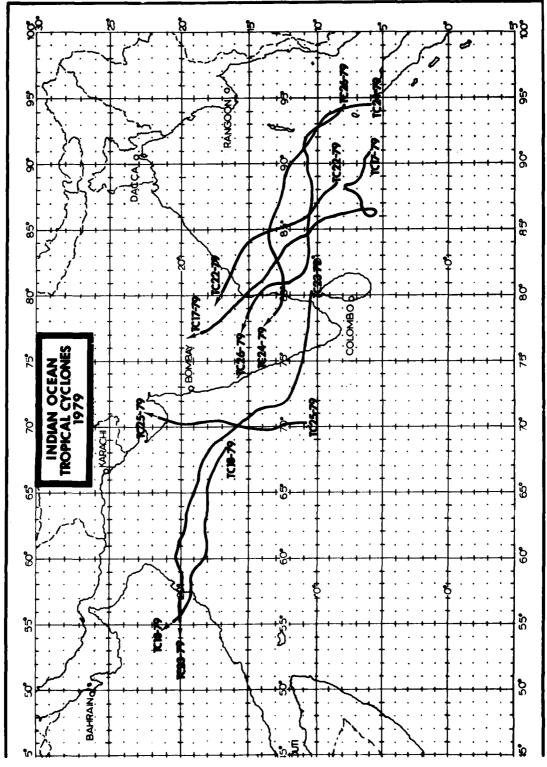
During 1979, 7 significant tropical cyclones occurred in the North Indian Ocean area (Table 3-3). As usual, the transition

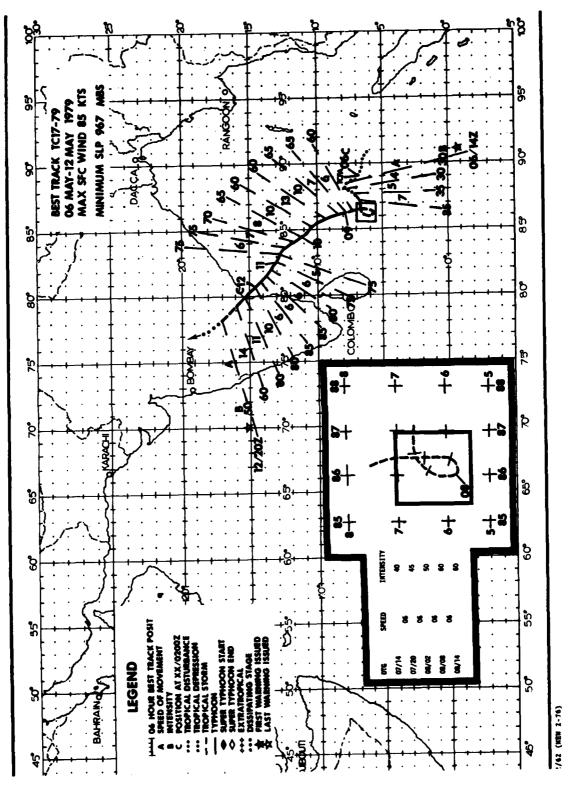
seasons between the northeast and southwest monsoon periods were the favored "cyclone seasons" (Table 3-4). This was an above normal season with most activity occurring during the fall transition period.

TABLE 3-3		NORTH INDIAN OCEAN									
1979 SIGNIFICANT TROPICAL CYCLONES											
CYCLONE	PERIOD OF MARNING	CALENDAR DAYS OF MARNING	MAX SFC WIND	EST MIN <u>SLP</u>	NUMBER OF MARNINGS	DISTANCE TRAVELLED					
TC 17-79	O6 MAY-12 MAY	7	85	967	26	1267					
TC 18-79	18 JUN-20 JUN	3	50	985	12	581					
TC 22-79	21 SEP-23 SEP	3	25	1000	10	694					
TC 23-79	21 SEP-25 SEP	5	55	980	14	1108					
TC 24-79	29 OCT-01 NOV	4	35	995	13	720					
TC 25-79	16 NOV-17 NOV	2	40	994	.8	547					
TC 26-79	23 NOV-25 NOV	3	30	995	10	1071					
	1979 TOTALS	24*			93						

TABLE 3-4.													
			1979 5	IGNIFIC	ANT TRO	PICAL C	YCLONE	STATIST	103				
NORTH INDIAN OCEAN	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	ост	NOV	DEC	TOTAL
ALL CYCLONES	0	0	0	0	1	1	0	0	2	1	2	0	7
(1971-78) AVERAGE*	0.1	0	0	0.3	0.5	0.3	0	0	0.4	0.8	1.4	0.3	4
FORMATION ALERTS	7 of	the 8	(87%) F	Formation	n Alert	Events	develo	ped int	o numbe	red cyc	lones.		
MARMINGS			_	days:					,		_		
Number of warning days with 2 cyclones: 3  Number of warning days with 3 or more cyclones: 0													
*From 1971 through 1974, only Bay of Bengal cyclones were considered; the JTMC area of responsibility was													

extended in 1975 to include Arabian Sea cyclones.





TC 17-79 was the only significant tropical cyclone in the Bay of Bengal during the 1979 spring transition season. Attaining typhoon intensity, TC 17-79 was the most destructive cyclone in India since TC 22-77 (Nov 1977) which, coincidentally, followed a similar track.

A Tropical Cyclone Formation Alert and the first warning were precipitated by synoptic reports received from ships participating in the First GARP Global Experiment (FGGE). At 1200Z on 6 May, these ships' observations defined a cyclonic circulation near 07M-088E with reported surface pressures near 1003 mb and wind speeds of 20-25 kt (10-12 m/sec). The first warning on TC 17-79 was issued at 061507Z.

From 0600002 through 0612002, a strong mid-tropospheric ridge extended westward along 15N with southeast steering flow dominating TC 17-79's movement. During the same time period, a short-wave trough, evident at both middle and upper levels, was deepening over India. Interaction between this ridging and troughing resulted in a loss of definitive steering flow in the vicinity of TC 17-79, producing an erratic north and then south track. Also during this time, TC 16-79 located in the southern Indian Ocean about 750-800 nm (1389-1481 km) to the southwest,

COLOMBO

FIGURE 3-29. TC 17-79 with well-defined satellite signature during the erratic cyclonic loop, 8 May 1979, 05282. (DMSP imagery from AFGMC, Offutt AFB, Nebraska)

began tracking slowly to the southeast possibly initiating a Fujiwhara type interaction.

By 080000Z, a mid-level anticyclone had formed in the northern Bay of Bengal with east-northeasterly steering flow over TC 17-79 resulting in a west-southwest forecast track. Prom 080000Z through 090000Z, while TC 17-79 intensified (Fig. 3-29), the dominant steering flow shifted to the south then southeast as the mid-level ridge was replaced by a trough and the upper-level trough dug southward over India. As a result of this shift in steering flow, TC 17-79 executed a tight cyclonic loop from 080000Z to 081800Z. From 7 through 9 May, though satellite fix position accuracies improved due to the formation of a well-defined eye, forecast errors increased appreciably due to the erratic movement.

By 0912002, southeast steering flow became dominant with TC 17-79 oscillating about a northwest track until making landfall over India (Fig. 3-30). TC 17-79 struck the east central coast of India at 1208002, 45 nm (83 km) north of Nellore with maximum sustained winds of 80 kt (41 m/sec). Twenty-one deaths occurred and over 800,000 persons were left homeless as a result of TC 17-79's passage over the Nellore district.

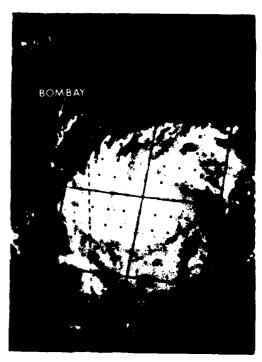
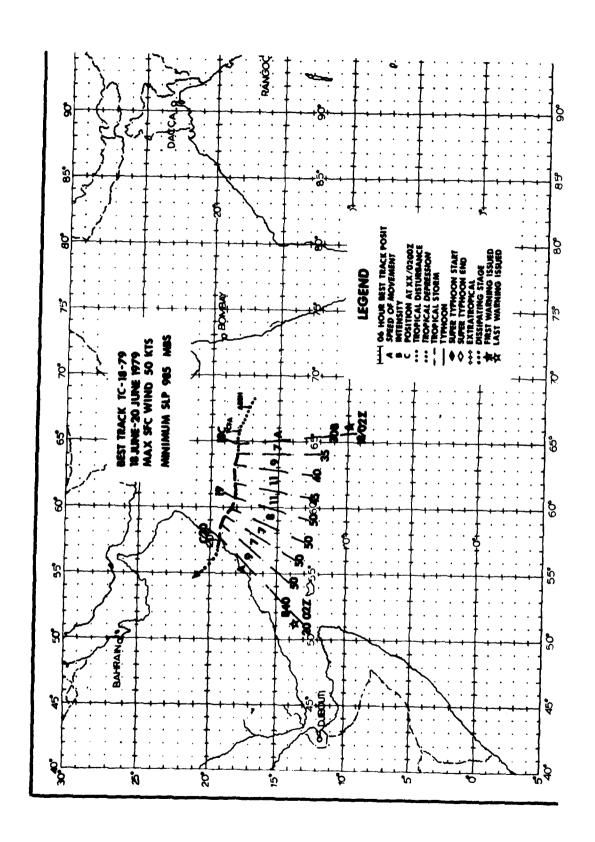


FIGURE 3-50. TC 17-19 just prior to making landfall over east central India with 80 kt (41 m/sec) intensity, 12 May 1979, 05562. (SMSP imagery from AFGMC, Offutt AFB, Nebrasha)



TC 18-79 began 1714002 June 1979 as a monsoon depression in the Arabian Sea and tracked virtually westward throughout its life, finally dissipating over the Oman coast (Fig. 3-31). Although TC 18-79's movement was confined to a narrow 2-degree latitudinal band, the extent of the meteorological hazard from gale force winds encompassed roughly half of the Arabian Sea. These gale force winds were produced by the interaction of TC 18-79 with the normal southwest monsoonal flow over the Arabian Sea.

During this season, a climatological low-level wind maximum develops off the coast of Somali. Normal wind speeds can reach 35-40 kt (18-21 m/sec), but the gale area is generally localized near the coast. However, beginning 2 days prior to TC 18-79's forma-

tion, a surge in the monsoonal flow occurred and a low-level jet could be traced from the Somali coast extending eastward across the entire Arabian Sea. The strength and persistence of this feature aided the formation of TC 18-79 in the cyclonic shear side of the wind maximum. As TC 18-79 intensified and moved westward, the southwesterly flow strengthened to a point where 65 kt (33 m/sec) surface winds were observed 600 nm (1111 km) away from TC 18-79's center. Examination of the visual data of Figure 3-31 shows cloud streets indicative of this strong low-level flow from 05N to 12N between 55E to 62E. The gale area persisted during gradually with time. Interestingly, post-analysis reveals the maximum winds in the gale area exceeded the maximum sustained winds estimated in TC 18-79's center.

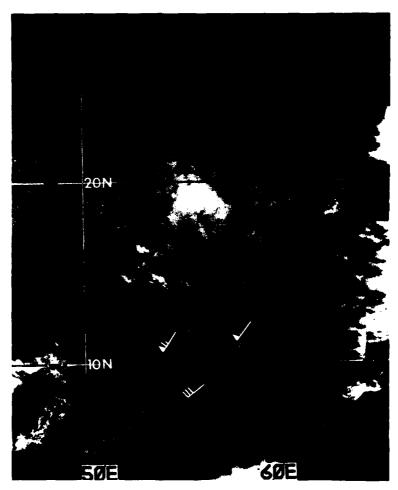
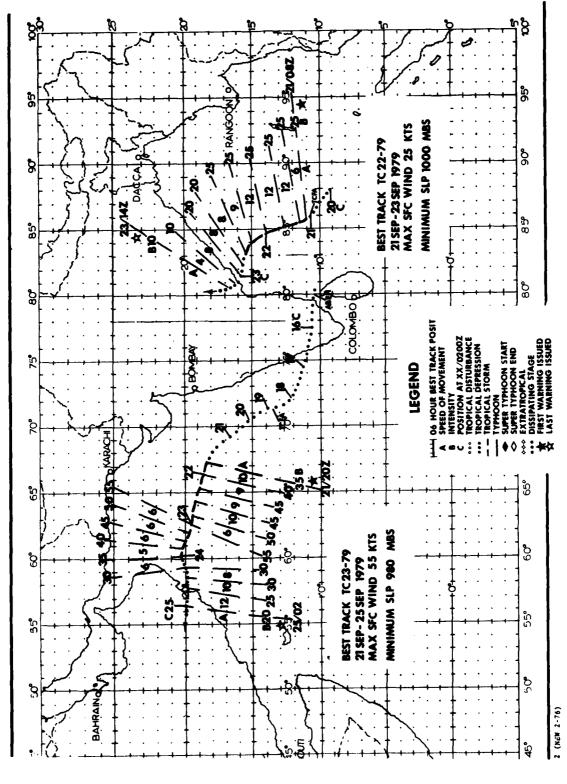
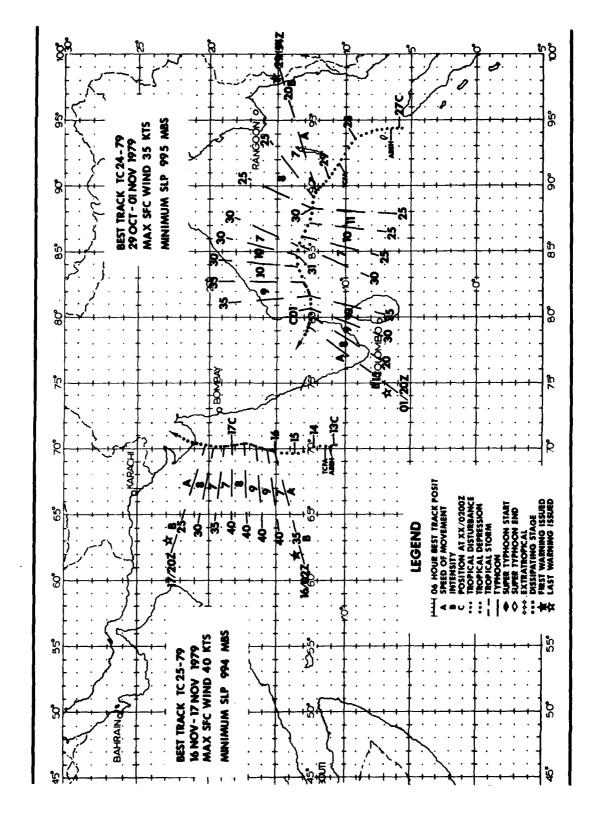
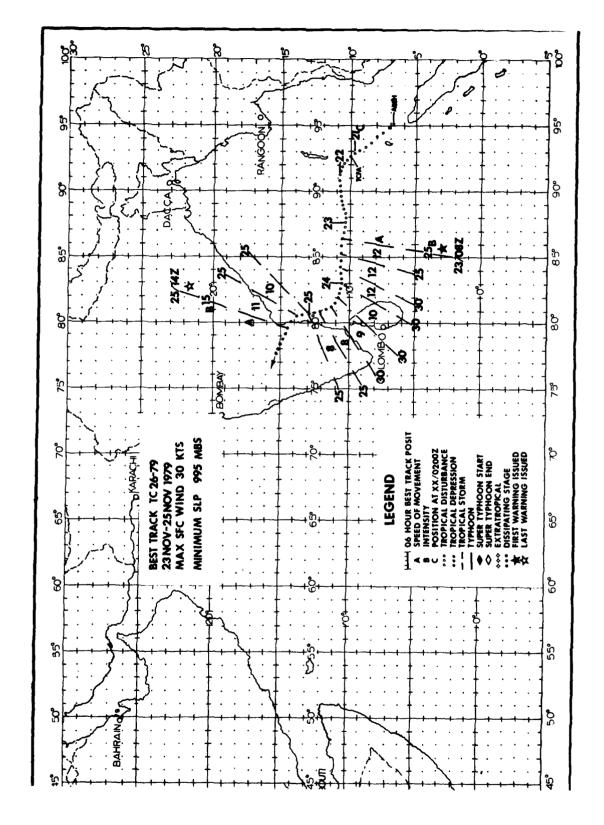


FIGURE 3-31. TC 18-79 located just off the Oman coast with gale force winds to the south, 20 June 1979, 07312. Superimposed are ship observations at 2006002. (DMSP imagery from AFGWC, Offutt AFB, Nebrask4)







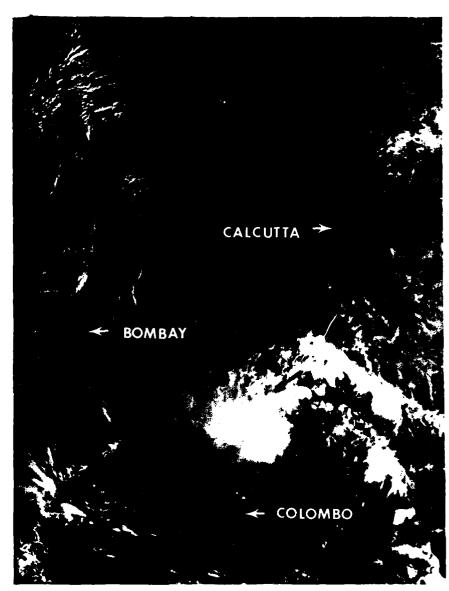


FIGURE 3-32. TC 26-79 as an exposed low-level circulation, 24 November 1979, 04552. (DMSP imagery from AFGWC, Offutt AFB, Nebraska)

# CHAPTER IV SUMMARY OF FORECAST VERIFICATION

# 1. ANNUAL FORECAST VERIFICATION

#### a. Western North Pacific Area

Forecast positions at warning times and 24-, 48-, and 72-hour valid times were verified against corresponding best tracks. Vector errors and right angle errors for individual tropical cyclones were calculated

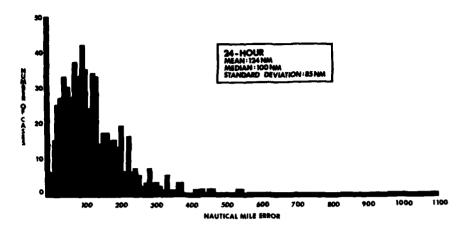
and are displayed in Table 4-1. Annual mean errors for all tropical cyclones are listed in Table 4-2 for comparison. Frequency distributions of the vector errors for 24-, 48-, and 72-hour forecasts on all 1979 tropical cyclones are shown in Figure 4-1. Annual mean vector errors are graphed in Figure 4-2.

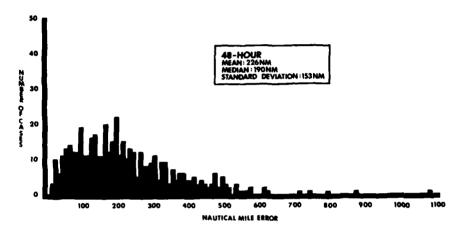
TABLE 4-1. FORECAST ERROR SUMMARY FOR THE 1979 WESTERN NORTH PACIFIC SIGNIFICANT TROPICAL CYCLONES.

			ED 5015114			24 110115			48 .HOUR			72	
l		POSIT	WARNING RT ANGLE		POSIT	24 HOUR RT ANGLE		POSIT	RT ANGLE		POSIT	72 HR RT ANGLE	
c	YCLONE	ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS	ERROR	BRROR	WRNGS	ERROR	ERROR	WRNGS
1.	TY ALICE	18	11	51	105	83	47	222	175	43	338	271	39
2.	TY BESS	19	15	21	114	73	17	265	164	13	348	240	9
3.	TY CECIL	15	11	40	87	62	37	191	131	33	320	215	29
4.	TS DOT	23	16	24	130	79	23	244	171	20	315	257	16
5.	TD-05	12	12	6	158	150	3						
6.	TY ELLIS	25	21	22	71	57	18	145	103	14	185	113	10
7.	TS FAYE	35	21	20	138	86	17	167	93	14	180	99	10
8.	TD-08	43	20	5	195	70	4	396	396	1			
9.	TS GORDON	23	12	13	129	90	9	173	121	5	449	278	1
10.	TS HOPE	23	16	33	134	75	29	266	140	23	376	188	21
11.	TD-11	47	30	14	144	94	3.0	138	89	6	171	129	2
12.	TY IRVING	26	17	38	163	98	34	286	209	30	441	344	26
13.	ST JUDY	18	12	39	105	81	36	173	138	27	277	213	23
14.	TD-14	33	19	9	157	43	5	296	118	1			
15.	TS KEN	29	13	13	116	60	10	278	111	7	415	195	3
16.	TY LOLA	16	10	23	88	64	21	172	148	19	287	236	14
17.	TY MAC	23	16	35	93	66	27	196	152	19	279	227	19
18.	TS NANCY	28	19	14	116	86	9	216	186	4	227	219	1
19.	TY OWEN	25	15	37	146	78	33	250	158	29	327	256	25
20.	TS PAMELA	28	22	6	254	15	2						
21.	TS ROGER	32	19	16	195	93	13	251	108	9	303	178	4
22.	TY SARAH	26	16	43	61	40	39	110	86	34	143	107	27
23.	ST TIP	24	15	60	135	69	56	259	142	52	345	214	48
24.	ST VERA	43	20	23	148	69	19	249	111	15	385	247	11
25.	TS WAYNE	27	14	22	170	115	16	362	295	12	443	413	4
26.	TY ABBY	31	17	52	164	108	48	286	198	39	338	215	26
27.	TD-26	21	16	6	55	28	3		<del>-</del>	_	-		
28.	TS BEN	34	18	10	81	89	6	287	16	2			
ALL	FORECASTS	25	16	695	124	77	591	226	151	471	316	223	368

TABLE 4-2. ANNUAL MEAN FORECAST ERRORS FOR THE WESTERN NORTH PACIFIC.

		24-HR		48-HR		72-HR
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971	111	64	212	118	317	177
1972	117	72	245	146	381	210
1973	108	74	197	134	253	162
1974	120	78	226	157	348	245
1975	138	84	288	181	450	290
1976	117	71	230	132	338	202
1977	148	83	283	157	407	228
1978	127	75	271	179	410	297
1979	124	77	226	151	316	223





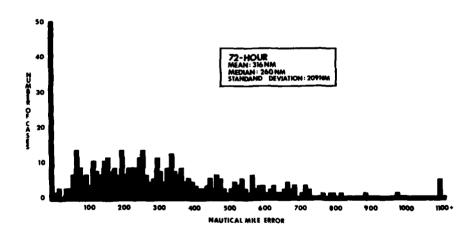


FIGURE 4-1. Frequency distribution of 1979 24-, 48-, and 72-hour forecast vector errors for all significant tropical cyclones in the western North Pacific.

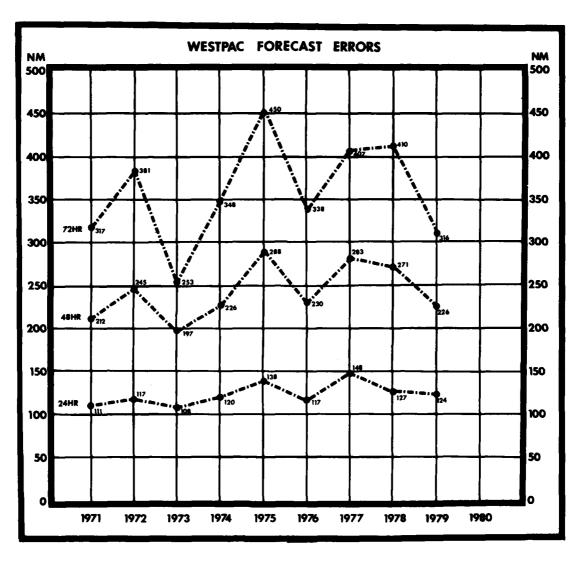


FIGURE 4-2. Annual vector errors (nm) for all cyclones in the western North Pacific.

Intensity verification statistics for all significant tropical cyclones in the western North Pacific area are depicted in Figures 4-3 and 4-4. The average absolute magnitude of the intensity error as well as the intensity bias (algebraic average) are graphically depicted. An analysis of the errors indicates that JTWC intensity forecasts often lag true intensity. In intensi-

fying situations, JTWC underforecasts, while in weakening situations JTWC overforecasts. This causes a large average magnitude error, but a small average bias. Verification of intensity forecasts by objective aids is also depicted in Figures 4-3 and 4-4. (An explanation of the objective forecasting aids is found in this chapter, Section 2-Comparison of Objective Techniques.)

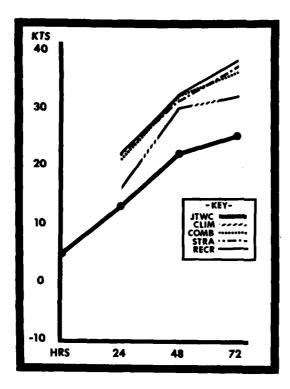


FIGURE 4-3. Comparison of average intensity errors (magnitude) for all cyclones in the western North Pacific.

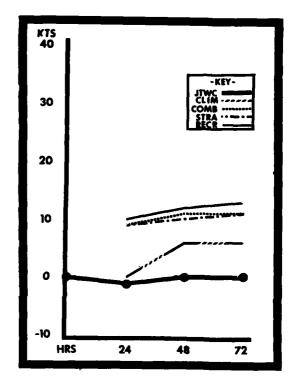


FIGURE 4-4. Comparison of average intensity errors (biases) for all cyclones in the western North Pacific.

#### b. North Indian Ocean Area

Forecast positions at Marning times and 24-, 48-, and 72-hour valid times were verified by the same methods used for the western Morth Pacific area. Table 4-3 is the forecast error summary for the significant tropical cyclones in the North Indian

Ocean area. Table 4-4 contains the annual average of forecast errors back through 1971. Vector errors are plotted in Figure 4-5. Seventy-two hour forecast errors were evaluated for the first time in 1979.

Porecast intensities were not verified.

ZABLE 4-3. PORBCAST ERROR SUMMARY FOR THE 1979 HORTH INDIAN OCEAN SIGNIFICANT TROPICAL CYCLOMES.

WARNING 24 HOUR 48 HOUR 72 HOUR 72 HOUR FOSTS RT ANGLE 9 FOST

CYCLOHE	ERROR	RT AMGLE	WINGS	ERBOR	ERROR	WROIGS	POSIT	ERROR	MRMGS	ERROR	ERROR ERROR	<b>Impos</b>
TC 17-79 TC 18-79 TC 22-79 TC 23-79	36 48 54 48	17 24 34 21	26 12 10 14	139 137 122 160	95 78 90 97	22 7 7	233 363 170 253	192 284 122 184	18 4 3	346 773	296 629	14
TC 24-79 TC 25-79 TC 26-79	48 50 52	26 26 31	13 8 10	190 189 148	142 103 83	9 4 5	482 121 163	332 73 21	5 1 2	1036	902	í
ALL PORECAST	8 46	24	93	151	99	63	270	202	38	437	371	17

TABLE 4-4. ANNUAL MEAN FORECAST ERRORS FOR THE NORTH INDIAN OCEAN (the Arabian Sea was not included prior to 1975).

		24-HR		48-HR		72-HR
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971	232	-	410	-	-	-
1972	224	101	292	112	-	•
1973	182	99	299	160	-	-
1974	137	81	238	146	-	-
1975	145	99	228	144	-	-
1976	138	108	204	159	-	-
1977	122	94	292	214	-	-
1978	133	86	202	128	-	•
1979	151	99	270	202	437	371

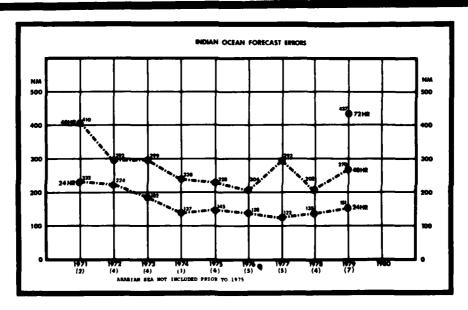


FIGURE 4-5. Annual mean vector errors (nm) for all cyclones in the North Indian Ocean.

#### 2. COMPARISON OF OBJECTIVE TECHNIQUES

#### a. General

3

Objective techniques used by JTWC are divided into four main categories:
(1) climatological and analog techniques;
(2) extrapolation; (3) steering techniques;
and (4) a dynamic model. The analog technique provides three movement forecasts:
one for straight moving cyclones, one for recurving cyclones and one which combines the tracks of straight, recurving and cyclones that do not meet the criteria of straight or recurving analogs. All techniques were executed using the operational data available at warning time.

#### b. Description of Objective Techniques

- (1) TYFN75 Analog program which scans history tapes for cyclones similar (within a specified acceptance envelope) to the current cyclone. Three 24-, 48-, and 72-hour position and intensity forecasts are provided (straight, recurve and combined).
- (2) MOHATT 700/500 Steering program which advects a point vortex on a preselected analysis and smoothed prognostic field at designated levels in 6-hour time steps through 72 hours. Utilizing the previous 12-hour history position, MOHATT computes the 12-hour forecast error and applies a bias correction to the forecast position.
- (3) TCM The Tropical Cyclone Forecast model is a coarse mesh (220 km) PE Model, with the digitized storm warning position bogused in the 850 mb wind and temperature fields of the FLENUMOCEANCEN Global Band Analysis. Hemispheric forecast data are used on the boundaries.
- (4) CLIM A climatological aid in the form of 24-, 48-, and 72-hour tropical

cyclone forecast positions and intensity changes for initial latitude/longitude positions. The data are arranged by months and are based on historical data which includes 1945 to 1973. This detailed climatology replaced the previous JTMC climatology on 1 September 1980.

- (5) 12-HR EXTRAPOLATION A track through the current warning position and the 12-hour old preliminary best track position is linearly extrapolated to 24 and 48 hours.
- (6) HPAC The 24- and 48-hour forecast positions are derived by averaging the 24- and 48-hour positions from the 12-hour EXTRAPOLATION track and the CLIM track.
- (7) INJAH74 Analog program for the North Indian Ocean similar to TYPM75, except tracks are not segregated.
- (8) TYAN An updated analog program which combines TYFN75 and INJAH74.
- (9) CYCLOPS An updated version of the MOHATT program which has the capability to select steering forecasts at the 1000, 850, 700, 500, 400, 300 and 200 mb levels.

#### c. Testing and Results

A comparison of selected techniques is included in Table 4-5 for all western North Pacific cyclones and in Table 4-6 for Indian Ocean cyclones. In Tables 4-5 and 4-6, "X-AXIS" refers to techniques listed horizontally across the top, while "Y-AXIS" refers to techniques listed vertically. The example in Table 4-5 compares COMB to MH70. In the 425 cases available for comparison, the average 24-hour vector error was 134 nm for COMB and 160 nm for MH70. The difference of 26 nm is shown in the lower right. (Differences are not always exact due to computational round off.)

TABLE 4-5.

STATE	STICS	FOR	YEAR		24 H	A FCS	TS													
	<u>J1</u>	Æ	<u>51</u>	RA.	95	CR	였		1	172	挽	60	10	<del>110</del>	Ġ	<u>IM</u>	<u>X1</u>	RP.	HP.	AC
JTMC	591 124	124								Γ				-AXIS	7					
STRA	525 153	122 31	533 153	153 0						_		4		MOR.	4					
RECR	516 139	127 12	489 136	153 -16	524 139	139			/	120	Y-AXIS CHANGU MAKKR		DIF	PERCE Y-X	×					
COMB	543 135	124 10	514 133	153 -19	509 135	139 -3	551 135	135 0	/	<u> </u>		i								
<b>10</b> 170	435 159	123 36	407 158	150 8	399 163	136 26	425 160		445 158	158 0										
19150	425 158	124 35	396 157	152 5	389 160	136 25	413 159	135 24	430 157	159 -1	434 157	157 0								
TCMD	121 132	122 10	111 134	152 -16	104 146	128 18	115 141	127 14	96 143	148 -4	96 142	138 4	124 136	136 0						
CL IM	305 150	129 20	282 142	165 -22	265 150	152 -1	291 149	145 3	245 149	170 -20	245 150	162 -11	93 153	144 9	315 150	150 0				
XTRP	572 150	124 26	521 146	152 -5	511 153	138 15	538 150	133 17	439 145	159 -13	431 145	158 -12	124 142	136 6	309 168	150 18	584 149	149 0		
HPAC	559 134	124 10	514 129	152 -23	501 135	137 -2	527 134	133	434 133	158 -24	426 132	158 -25	124 129	136 -6	309 138	150 -11	571 134	150 -15	571 134	134 0

	JT	WC.	ST	RA	RE	CR	ÇQ	19	194	70	100	60	19	<b>70</b>	<u>cr</u>	<u>IM</u>	XT	RP	HP:	AC.
												·		-						
JTMC	471 226	0											TPA -	OFFICE STRAIG	H7 (T	<b>(FN 7</b>	5)			
STRA	437 309	224 85	462 306	306 0								o	<b>90 -</b>	PECURA COMBUS MUSICAT	ED (T	<b>(71)</b> 7	5)			
RECR	415 247	232 15	422 248	306 -57	440 252	252 0						7	OID -	TOPIC	AL CY			(0)	<b>10</b> (Y)	
COMB	440 244	225 20	449 243	306 -62	430 243	251 -7	466 244	244 0				×	77 <b>8</b> -	12-HOU Historica	R EXT			TOLOGY		
<b>PH</b> 70	330 313	222 91	340 308	307 1	323 318	249 69	347 310	243 67	359 308	308 0										
<b>PH</b> 50	330 299	220 79	339 296	305 -8	320 297	247 50	345 297	242 55	345 292	310 -17	358 295	295 0								
TCM0	98 249	232 18	97 255	314 -57	86 273	246 27	96 264	25 <b>4</b> 10	76 264	357 -92	76 263	283 -20	102 257	257 0						
CLIM	244 246	235 11	249 243	330 -86	222 251	276 -25	247 252	265 -12	205 242	337 -94	206 242	294 -51	75 260	272 -11	263 250	250 0				
XTRP	457 291	224 67	450 290	304 -13	430 298	249 49	454 292	241 51	351 2 <b>9</b> 5	309 -13	353 291	296 4	101 311	255 56	260 325	249 76	485 291	291 0		
HPAC	445	223	442	305	418	246	442	242	345	308	346	295	101	255	260	249	471	291	471	23

STATE	STICS	FOR 1	YEAR		72 H	R FCS	rs									
	JT	MC	<b>S</b> 1	RA	RE	CR	CO	MB	H	170	H	N50	TO	240	α	.IM
JTWC	368 316	316 0														
STRA	338 443	315 129	361 453	453 0												
RECR	319 327	331 -3	345 348	456 -107	360 349	349 0										
COMB	343 328	316 12		452 -109	352 336	349 -12	385 340	340 0								
<b>M</b> 170	230 471	325 147	260 474	464 10	236 488	362 126	259 475	352 122	267 473	473 0						
M450	227 482	329 153	258 481	467 14	234 486	364 124	257 482	355 127	259 479	<b>469</b> 10	265 486	486 0				
TCM0	73 347	314 33	78 376	445 -68	69 393	351 41	78 380	359 22	61 401		62 3 <b>9</b> 6	484 -87	84 372	372 0		
CLIM	184 315	308 7	208 333	494 -160	179 338	357 -18	204 334	366 -31		506 -176	164 331	483 -151	64 353	389 -34	216 332	332 0

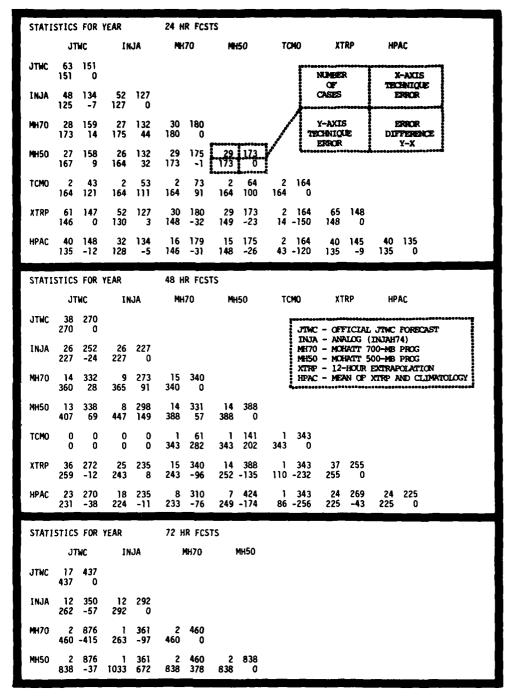


TABLE 4-6.

# CHAPTER X APPLIED TROPICAL CYCLONE RESEARCH SUMMARY

#### 1. JTWC RESEARCH

Part of the mission of the Joint Typhoon Warning Center is to conduct applied tropical cyclone research as time and resources permit. The purpose of this research is to improve the timeliness and accuracy of operational forecasts. During 1979, there was continued effort to convert and update operational programs and to streamline operational procedures for compatibility with the Naval Environmental Display Station. The following abstracts summarize the year's applied research projects which were completed or are still in progress.

ESTABLISHMENT OF THE JTWC TROPICAL CYCLONE DATA BASE

(Curry, W. T. and Matsumoto, C. R., NAVOCEANCOMCEN/JTWC)

A data base of 6-hour best track positions (intensities, direction and speed of movement) and 24-, 48-, and 72-hour objective technique and official JTWC forecasts for each tropical cyclone in the western North Pacific, Arabian Sea and Bay of Bengal from 1966 through 1978 has been established on FLENUMOCEANCEN computer mass storage systems. Tropical cyclone fix data (position, intensities, platform, etc.) for each tropical cyclone from 1966 through 1977 remain to be added. This climatological data base will be maintained on disk and tape files at FLENUMOCEANCEN Monterey, California and updated annually.

#### NEDS/COMPUTER APPLICATIONS

(Staff, NAVOCEANCOMCEN/JTWC)

JTWC's objective techniques have been converted by contractors to execute on FLENUMOCEANCEN computers. A NEDS graphic capability is being developed to depict forecast tracks from objective techniques. Evaluation and monitoring of program conversion will continue in 1980.

TROPICAL CYCLONE MINIMUM SEA-LEVEL PRESSURE - MAXIMUM SUSTAINED WIND RELATIONSHIP

(Lubeck, O. M. and Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

The pressure-wind relationship developed by Atkinson and Holliday (1977), Tropical Cyclone Minimum Sea Level Pressure - Maximum Sustained Wind Relationship for Western North Pacific, is a primary tool used to determine tropical cyclone intensities for JTWC operations. This relationship was re-evaluated and tested with an independent data set. The study produced no significant differences or changes. Therefore, the current Atkinson and Holliday relationship will continue to be used at JTWC. Other regression equations using case-dependent latitude and environmental pressure (versus 1010 mb) as predictors were also tested. These predictors did not improve the maximum sustained windminimum sea-level pressure relationship.

OBJECTIVE TROFICAL CYCLONE INITIAL POSITIONING WITH A WEIGHTED LEAST SQUARES ALGORITHM

(Lubeck, O. M. and Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

Recent studies indicate tropical cyclone forecast errors through 72 hours can be reduced by more accurate initial warning positions. This study developed an objective and standardized method of determining initial position based on all available fix information. A least squares algorithm was used on available fix data with a weighting scheme which is inversely proportional to the stated fix accuracies. The results of this objective method showed no significant improvement over the current subjective method. Therefore, this method was not incorporated into operational procedures. This method, however, produces an improved tropical cyclone "best track" and was incorporated into JTWC's post-analysis procedures.

EQUIVALENT POTENTIAL TEMPERATURE/MINIMUM SEA-LEVEL PRESSURE RELATIONHIPS FOR FORE-CASTING TROPICAL CYCLONE INTENSIFICATION

(Dunnavan, G. M., NAVOCEANCOMCEN/JTWC)

The relationship between equivalent potential temperature at 700 mb in the center of developing tropical cyclones and associated intensity changes was explored by Sikora (ATR 1975), Milwer (ATR 1976), and Hassebrock (ATR 1977). The Sikora and Milwer studies produced conflicting results, but the Hassebrock study showed some skill in forecasting explosive and rapid deepening when 1977 and 1978 tropical cyclones were evaluated. Evaluation of 1979 tropical cyclones again showed that the Hassebrock technique has some skill. Unfortunately, dewpoint data from aircraft reconnaissance missions from earlier years are not readily available at JTWC, so it has been difficult to increase the data base. The Hassebrock study will be applied to 1980 tropical cyclones and any cyclones prior to 1976 for which data are available. The data base may then be large enough to draw some definite conclusions.

A related study of equivalent potential temperature was also started. A comparison was made of past 12- and 24-hour changes in equivalent potential temperature in the eye of a tropical cyclone with the subsequent 12- and 24-hour changes in 700 mb height. These correlations proved inconclusive, again due to the small initial data base. An attempt will be made to obtain more data for this study also.

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BASIC STREAMLINE ANALYSIS AND TROPICAL CYCLONE FORECASTING TECHNIQUE GUIDE

(Guay, G. A., NAVOCEANCOMCEN/JTWC)

A case study, based on an active tropical cyclone period, is being developed. The study will be worked into a training guide for new forecasters and will include basic streamline analysis procedures as well as tropical cyclone forecasting techniques. The case study will also be integrated into STORMEX training (training scenario for DET 4 HQ AWS, 54 WRS, DET 1 lWW, JTWC, and AJTWC personnel).

IMPROVEMENT AND EXTENSION OF THE JTWC CLIMATOLOGY

(Shewchuk, J. D., NAVOCEANCOMCEN/JTWC)

Climatology is an important objective forecast aid for JTWC. A new climatology was developed for the western North Pacific which provides position and intensity forecast information for 24-, 48- and 72-hour intervals. Pertinent statistical information is produced by month for each latitude/longitude of available historical data, which includes 1945 to 1973.

Similar climatological information is being developed for the North and South Indian Oceans and the western South Pacific. The periods of available historical data are 1900-1970, 1900-1969 and 1900-1971, respectively.

#### 2. NEPRF RESEARCH

TROPICAL CYCLONE RESEARCH AT OR UNDER CONTRACT TO THE NAVAL ENVIRONMENTAL PREDICTION RESEARCH FACILITY (NEPRF), MONTEREY, CALIFORNIA

TROPICAL CYCLONE MODELING

(Hodur, R.M., NEPRF and Madala, R., NRL)

A one-way interactive Tropical Cyclone Model (TCM) is being evaluated operationally. This model differs from the original channeled TCM, that has been used for the past three years, in two ways. First, hemispheric forecast data are used on the boundaries as opposed to the channel boundaries used in the original TCM. Second, a new bogus is used to represent the storm based on the observed maximum wind. This latter change has cut the average initial position error by 59% to 15 nm. The one-way interactive TCM average forecast errors at 4%, 60 and 72 hr are 8%, 14% and 21% less than the channel model, respectively, for Pacific cyclones through August 1979. Both TCMs have about the same average forecast errors at 12, 24 and 36 hr.

A more sophisticated TCM is being developed jointly by NEPRF and NRL and is expected to become operational in 1981. This TCM includes the effects of surface friction, cumulus clouds and latent and sensible heat transfer from the ocean. Preliminary tests indicate that these improvements may reduce forecast track errors by 15% to 20% when compared to the one-way interactive TCM.

#### TROPICAL CYCLONE WIND DISTRIBUTION

(Tsui, T., Brody, L.R., and Brand, S., NEPRF)

The wind distribution around tropical cyclones for the warnings issued by the JTWC from 1966 through 1977 have been compiled and edited into a unique data set. An analysis of the wind radii shows the asymmetrical nature of the radii of 30 kt and 50 kt winds around tropical cyclones as a function of the characteristics of the storm. A statistical forecast model to predict the asymmetric wind distribution has been developed.

#### TROPICAL CYCLONE STRIKE PROBABILITIES

(Brand, S., NEPRF and Jarrell, J.D., Science Applications Inc.)

Tropical cyclone strike probability is a method for determining probabilities up through 72 hours that a tropical cyclone will come within specified distances around geographic points of interest to the user. This program can be used as an aid for operational decisions associated with tropical cyclone evasion, evacuation and base preparedness. Strike probability output is presently being evaluated by a number of Navy and Air Force meteorologists and operational customers in WESTPAC. Other applications of strike probability that are presently being developed include geographic depictions, wind probabilities and strike probabilities for EASTPAC.

A STATISTICALLY DERIVED PREDICTION PROCEDURE FOR TROPICAL CYCLONE GENESIS

(Perrone, T., Lowe, P., Rabe, K., and Brand, S., NEPRF)

A statistical experiment using stepwise discriminant analysis was conducted to determine algorithms to be applied to daily, operationally-available meteorological analyses. Parameters identified as potential predictors of tropical cyclone formation were statistically examined to determine their tropical cyclone genesis prediction capability and were found to possess substantial promise to predict tropical storm formation 24, 48 and 72 hours prior to occurrence.

#### EXTREME SEA STATES WITHIN A TYPHOON

(Rabe, K., and Brand, S., NEPRF)

Extremely high sea states are known to occur to the right of the direction of movement in typhoons. A well-documented case of such extreme sea heights in the western North Pacific was examined and compared with results from a numerical spectral ocean wave model. The wind and sea state field of the numerical model compared favorably with the observed data. An examination was also made to determine how extreme sea states relate to tropical cyclone intensity, forward speed of movement, and circulation size or wind distribution. The results indicated that all three are important with the intensity being the primary factor, speed of movement being of secondary importance and circulation size or wind distribution being the least important factor.

TROPICAL CYCLONE ORIGIN, MOVEMENT AND INTENSITY CHARACTERISTICS BASED ON DATA COMPOSITING TECHNIQUES

(Gray, W.M., Colorado State University)

Observational studies using large amounts of composited rawinsonde, satellite and aircraft flight data have been performed to analyze global aspects of tropical cyclone occurrences. The data were used to study the physical processes of tropical cyclone genesis, tropical cyclone intensity changes, environmental factors influencing tropical cyclone turning motion 24-36 hours before the turn takes place, tropical cyclone intensity determination from upper-tropospheric reconnaissance, and the diurnal variations of vertical motion in tropical weather systems.

IMPROVED UPPER-LEVEL TROPICAL CYCLONE STEERING TECHNIQUES

(Hamilton, H., Systems and Applied Sciences Corporation)

Current automated objective steering forecast techniques incorporating HATRACK and MOHATT algorithms are operationally termed CYCLOPS and may be run in analysis or prognosis modes at seven different atmospheric levels including 1000 mb, 850 mb, 700 mb, 500 mb, 400 mb, 300 mb and 200 mb. Since tropical cyclones vary greatly in areal and vertical extent and may be representatively steered at varying atmospheric levels dependent on state of development/intensity, continuing research is ongoing which will attempt to identify, given certain tropical cyclone input parameters, a "best" steering level or a "weighted scheme" that takes into account several steering levels.

AIRBORNE EXPENDABLE BATHYTHERMOGRAPH OBSERVATIONS IMMEDIATELY BEFORE AND AFTER PASSAGE OF TYPHOON PHYLLIS (AUG 75)

(Schramm, W.G., NEPRF and NAVPGSCOL)

Ocean thermal response to an intense typhoon was analyzed on the basis of data collected during the passage of Typhoon Phyllis (Aug 75) in the Philippine Sea. A unique data set was collected using calibrated Airborne Expendable Bathythermographs dropped from a Navy P-3 aircraft. There were three flights: the first, 14 hours before storm passage, the second 10 hours after passage, and the third two days later. The results indicate a dramatic upward movement of isotherms, relative to the sea surface, in a narrow band under the storm path, with a reversal toward pre-typhoon conditions within three days.

MESOSCALE EFFECTS OF TOPOGRAPHY ON TROPICAL CYCLONE ASSOCIATED SURFACE WINDS

(Brand, S. and Chambers, R., NEPRF, Woo, H., Cermak, J., and Lou, I., Colorado State University, and Danard, M., University of Waterloo)

An analysis was made of the influence of topography on tropical cyclone associated strong surface wind conditions for Subic Bay, Republic of the Philippines by means of an environmental wind tunnel. Surface flow patterns were deduced by smoke and surface oil films, while isotach and gust values were obtained by hot wire anemometers. The laboratory results show the significant effects of the mountainous regions surrounding the Subic Bay harbor complex and indicate preferred sheltered locations. The results were compared with synoptic observations and a high resolution (0.19 nm) diagnostic, one-level, primitive equation model. Where direct comparison could be made, all techniques appeared to show qualitative agreement.

TYPHOON HAVEN STUDIES

(Stevenson, G.A. and Brand, S., NEPRF)

The Typhoon Havens Research Program, the results of which have been summarized in NEPRF Technical Paper 5-76, has been resumed. COMSEVENTHFLT has identified an additional 12 ports and harbors for evaluation as typhoon havens. Work has commenced on Palau, Saipan and Tinian.

## ANNEX A TROPICAL CYCLONE TRACK DATA

L WESTERN NORTH PACIFIC CYCLONE TRACK DATA

#### TYPHOON ALICE

	HEST THACK		NG FRR() 35	Se HUIII	FOHECAST EHHJAS	48 HOUR FOHFCAST + #2045	FZ 40UR FRRECEST
40/04/45	POSIT JING	POSIT «IN)		PASTE WI	LNO DOF #IND	POSIT WIND OST 41	CHIE 720 CHIE 1209 ON
0101007	2.3 170.7 20	0.0 0.0 0.	-0. 0.	0.0 0.0	0. +U+ n.	n.n n.e 00.	0. n.0 0.0 00. 0.
0101067	3.1 170.1 25	0.0 0.0 0.	-0. U.	0.0 0.0	0U. n.	0.0 0.0 00.	0. 0.0 0.0 00. 0.
010112/	3.7 149.4 30	0.0 0.0 0.	-0. 0.	0.0 0.0	Qv. n.	0.0 0.0 00.	0. n.0 0.0 Do. n.
0101187	4.6 149.2 35	4.4 168.7 25.	3210.		10. 125. 425.	7,7 161.3 35. 409, -1	
0102007	5.2 14A.7 4n	5.7 168.5 45.	13. 5.	7.7 164.4	5. 213. n.	7.9 159.7 60. 495.	5. H.4 195.2 60. 588. 5.
0102067	5.7 148.2 45	5.4 167.4 30.	25. 2.	7.3 164.3 :	S. 240. S.	7.4 159.5 50. 495.	5. P.3 194.9 60. 547. 0.
0105152	6.2 147.8 50	6.5 156.4 50.	85. 0.	7.7 161.9 4	b0. 376. in.	a. 1 157.2 65. 571. 1	0. 9.2 192.3 65. 667. 0.
0105195	6.7 147.7 35	6.9 167.7 >5.	12. 0.	9.2 165.4 6	h5. 160. 1c.		0. 11.6 187.0 70. 339. 5.
0103002	7.2 148.0 55	7.2 167.5 >5.	30. 0.		h5. 136. In.		5. 11.6 lb6.5 70. 306. 0.
0103067	8.0 14A.7 59	7.9 168.4 55.	B. 5.		. ni .tSl .čd	14.1 169.9 65. 415.	5. 17.6 170.7 60. 64515.
0103157	d.> 148.2 50	8.9 168.9 35.	49. 5.		65. <u>20</u> /• 1n.	15.7 169.0 65. 463.	0. 19.9 171.3 50. 70930.
0103187	B.9 148.1 50	9.6 168.0 55.	42. 5.		5. 226. 1n.	14.3 169.5 65. 479.	0. 18.8 1/1.0 SO. 81535.
0104002	4.2 148.0 55	9.3 167.8 50.	135.		5, yy. n.	12.2 162-6 60. R41	
0104067	9.4 147.a 55	9.5 167.4 30.	175.		5, 1244.	12.3 162.7 50. 1301	
0104122	9.0 146.H 45	9.7 167.0 50.	175.		5. de. ejn.	12.3 160.9 60. A92	
010+185	9.5 156.0 SS	9.5 165.9 50.	65.		55. 53. 910.	10.H 158.0 60. 912	
0105002 7605010	9.5 145.1 55	9.6 165.0 50.	95. 195.		55. 59. 914.	11.5 157.2 60. 59. =3	
0103007	9.7 154.4 66 10.0 153.6 65	9.7 164.1 55. 10.1 163.2 55.	195. 2410.	10.5 160.1 6	60. 72. •15. 60. 74. •2n.	11.7 156.2 b0. 433	
0102182	10.6 142.7 45	10.1 152.7 55.	010.		5. 68. 42n.	11.6 155.6 70. 77. 03	
0106002	11.1 141.7 70	11.2 161.7 55.	615.		b5. 27. 425.	12.6 153.7 70. 514	
0106062	11.6 150.4 75	11.9 160.4 70.	175.		85. 78. Th.		5. 17.0 148.6 105. 117. 30.
0106122	12.0 159.4 40	12.0 159.4 75.	05.		VO. BU10.		0. 12.9 146.3 105. 71. 35.
0106182	12.2 158.6 45	12.3 158.7 80.	195.		VG. 73. 015.		5. 17.4 145.0 105. 52. 30.
0107002	12.3 157.4 90	12.3 157.4 85.	125.		45. 70. *15.		5. 11.4 146.1 110. 183. 35.
010706Z	12.3 156.4 95	12.3 156.7 90.	65.	11.0 152.9 10		11.5 148.9 110. 139. 3	5. 11.4 144.8 120. 186. 40.
010/122	12.3 155.4 100	12.2 155.4 95.	195.	11.0 151.0 II		11.5 147.8 115. 145. 4	5. 11.5 143.8 120. 192. 40.
0101182	12.2 154.4 105	12.5 154.0 105.	29. 0.	12.2 149.3 1			5. 17.5 139.1 120. AB. 35.
0100002	12.1 153.0 110	12.2 153.1 110.	9. 0.	12.0 144.2 12			5. 17.0 139.0 115. 48. 25.
0108062	12.0 151.5 100	12.0 151.7 115.	12. 15.	11.9 146.5 1			5. 12.0 135.5 110. 169. 15.
OIORISS	12.0 150.> 40	12.0 150.5 115.	18. 25.	11.0 144.7 14			5. 12.0 134.7 110. 102. 15.
0108182	11.9 149.0 45	11.9 149.1 105.	5. 20.	11.0 147,9 10			0. 13.5 133.6 95. 2325.
010+00Z	11.9 147.0 60	11.8 147.7 100.	13. 20.		90. 30. 15.		5, 12.0 131.9 80. 33020.
010-062	12.1 146.4 75	11.4 146.5 95.	19. 20.		45. 25. 4.	11.9 136.4 80, 1211	
010918Z	12.1 145.4 70	12.0 145.7 90.	13. 20. 13. 5.		75, 415. 70, 64. <del>-</del> 15.	12.3 134.6 65, 192, +3	
0110002	12.0 144.2 75	12.) 144.0 80. 11.9 143.0 80.	13. 5.	11.0 137.9	70. 64. #15. 70. 66. #2n.	12.2 132.7 60. 2824	
0110062	12.1 141.7 #0	12.1 141.5 75.	125.		5. 124. •3n.	12.2 131.0 55. 367. •4	
0110122	12.2 140.4 40	12.2 140.1 75.	295.		5. 190. ¶3n.	12.5 129.4 35. 435. +3	
0110182	12.2 139.8 BS	12.2 139.0 85.	47. 0.		45. 233. •15.		5. 12.9 123.9 60. 741. 20.
0111002	12.4 138.9 90	12.3 139.0 85.	95.		15. 94. 415.	12.1 132.8 75. 296.	5. 12.5 128.0 60. 517. 30.
0111062	12.7 138.3 95	12.5 137.9 90.	265.		10. 198 •2n.		5. 17.2 124.8 45. 687. 25.
0111122	13.1 137.4 95	13.0 137.7 95.	9. 0.		80. 79. •1n.		5. 0.0 0.0 00. 0.
0111187	13.4 117.6 100	13.3 137.1 95.	305.		10. 146. n.		0. n.D D.O DD. 0.
2002110	13.7 147.7 100	13.9 137.2 90.	R10.	15.8 137.4 F	40. 52. In.	18.7 140.0 70. 235. 4	0. 1.0 0.0 00. 0.
0112062	14.1 137.0 100	14.2 136.9 90.	810.		70. 29. 15.		0. 0.0 0.0 00. 0.
0115155	14.5 136.4 9n	15.2 136.4 85.	435.		65. 8j. zn.	n.o 0.0 00.	0. n.0 0.0 D0. 0.
0115182	15.0 136.4 90	15.2 136.5 BO.	12. 0.		ho. 43. 2n.	n.0 0.0 00.	0. 0.0 0.0 00. 0.
011300Z	15.4 136.4 70	15.5 136.5 80.	B. 10.		60. IZ4. 3n.	n.n 0.0 0a.	0. 0.0 0.0 00. 0.
0113067	15.6 136.9 55	15.9 136.7 70.	13. 15.		5, 194. 35.	n.a 0.0 00.	0. 0.0 0.0 00. 0.
0113127	16.1 137.3 45	16.1 137.2 65.	6. 20.	0.0 0.0	0U. n.	n.o 0.0 DO.	0. 1.0 0.0 0 1.
0113187	16.1 137.0 40	16.4 137.5 55.	34. 15.	0.0 0.0	00. n.	0.0 0.0 00.	0. A.O 0.D DO. A.
0114002	16.1 136.5 30	16.1 136.5 45.	0. 15.	0.0 0.0	0U. n.	0.0 0.0 00.	
0114062	16.0 136.0 20	16.0 136.0 30.	n. 10.	0.0	00· n.	n.() 0.0 D0.	0. n.o 0.o 0o. a.

	AI L	FORECAS	15	
	HMNG	24-4R	46-H3	72-46
AVG FORFRAST POSIT FRHAR	18.	105.	555*	378.
AVG HIGHT ANGLE EROPR	11.	A3.	175.	271.
AVE INTENSITY MAGNITUDE ERROR	A.	17.	23.	23.
AVG INTRUSTLY STAS	2.	2.	1.	-3,
NUMBER OF FORECASTS	51	47	43	35



## TYPHOON BESS

	RFST THACK				VARVI				24 4	SH F				48 40	)114 F	HFCA.			12 4	OUM FO	14F(4	51
			•		•		4045		_		EHH.											
HIVAC/ON	POSIT	A [ AU	P 25		FIND		4[4)	Pns		# f A0		. [ -+1)	PITS		4140		#IND	P30		9147		41 411
0318002	7.1 150,		0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	n .	0 • 11	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
0318065	7.8 149.		0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0-	a •	0.11	0.0	Ű.	-0.	0.	".0	0.0	٥.	-0.	0.
0319152	8.6 147.		0.0	0.0	٥.	-0.	υ.	0.0	0.0	٥.	-0.	۰.	V . II	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0-	٥.
0318185	9.3 146,		0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0•	۰.	0.0	0.0	0.	-0.	0.	4.0	0.0	٥.	-0-	0.
031900Z	9.8 145,		6.0	0.0	٥.	-0.	٥.	0.0	0.4	٥.	-0.	n.	0.0	0.0	Ú.	-0.	a.		0.0	0.	-0.	0.
0314062	10.2 144.	V 50	0.0	0.0	v.	-0.	٥.	0.0	0.0	٥.	-0.	η.	U . II	0.0	v.	- U .	0.	r.0	0.0	0.	-0.	ο.
0314157	10.4 143,	- 20	0.0	0.0	٥.	-0.	U.	0.0	0.0	0.	-0.	4.	0.0	0.0	U.	- J -	٥.	0	0.0	0.	-0-	о.
031+16Z	10.6 142.	7 25	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	~ U •	٠.	0.4	0 • 0	0.	-0.	0.	n • 0	0.0	. 0.	-0.	0.
0320002	10.5 141.	7 30		14].9	25.	27.	-5.		134.4	٠٥٤	130	۰.		13203		115.			141.7		446.	
0320062	10.6 140.	7 30	10.5	140-5	JO.	12.	٥.	10.H	136.0	<b>55.</b>				131.5		243.			1/7.8		443.	
0350155	10.7 139.	g 3n	10.5	139.8	30.	13.	U.	10.0	135.4		150.			131.4		407.			177.0		£44.	
0320182	11.0 139,	2 31	11.0	139.0	30.	12.	0.	11.7	135.5	JQ.	102.	•2n.		1 12-4		213.			1 40.4		440.	
0321002	11.7 138.	6 31	11.2	138.7	30.	35.	0.	11.0	134.4	35.	107.	•2n.		132.5		240.			1.40.0		542.	
0321062	12.3 138.	0.40	12.3	138.2	35.	12.	-5.	14.7	137.0		105.			137.4		176.			1 44.1	30.		-58.
0321122	12.8 136,	9 45	12.4	137.5	40.	35.	-5.	15.7	136.4	>0.	llu.	<b>-20.</b>		138.0		114.			140.8	35.	۸l.	-25.
0321182	13.3 136.	1 50	13.6	136.1	45.	19.	·>.	17.0	134.4		102.	45e*		138.4		92.			142.3	Jō.	***	
0322007	13.7 135.	A 55	14.1	135.1	35.	39.	٥.	17.2	137.0	/5.	117.	٠.	20.0	134.5	50.	193.	-30.	21.4	1 40.4	45.	7 48.	20.
0322062	14.1 135.	3 60	14.0	135.5	60.	13.	0.	16.0	134.0		91.	-4.		133+1	90.	375.	-10.	0.0	0.0	0.	-0,	۰.
0322122	14.7 135.	n 7n	14.6	134.9	70.	9.	0.	16,5	137.7	85.	175.	۸.	18,5	133.3	9u.	**1.	30.	0.0	0.0	0.	-0.	0.
0355182	15.3 174.	A 75	15.1	134 . 6	75.	17.	0.	16.0	134.6	40.	210.	n.	19.3	134.1	<b>#</b> U.	486.	45.	0.0	0.0	0.	-0.	e.
0323002	16.1 134.	7 75	15.4	134.7	75.	14.	0.	18.0	134.7	H5.	202.	-5.	20.5	136.6	15.	440.	50.	0.0	0.0	0.	-0.	п.
032306Z	17.0 115.	2 40	17.0	134.A	HO.	23.	0.	20.3	134.5	HO.	151.	AIN.	0.0	0.0	0.	- U .	0.	0.0	0.0	۰.	-0.	0.
0323127	17.8 116.	0 85	17.7	136.2	В0.	13.	-5.	20.4	140.7	60.	30.	۰.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	e.
0323182	18.7 136.		19.3	137.1	80	25.	-10.	21.5	142.1	50.	32.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
032400Z	19.5 117.			137.4	85	6.	-5.		147.6	50.	95.	Ž4.	0.0	0.0	0.	-0.	0.	0.0	0.0	v.	-0.	a.
0324062	20.3 139.			139-1	75.	6.	-15.	0.0	0.0		-0.	٥.	0.0	0.0	Ű.	-0.	0.	0.0	0.0	0.	-0.	0.
0324122	21.2 140.			140.4	75.	13.	15.	0.0	0.0	ō.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0324182	22.0 142.			141.9	65.	23.	30.	0.0	0.0	o.	-0.	n.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	Λ.
0325002	22.9 144.		23.4	143.8	30	41.	5.	0.0	0.0	0.	-0.	n.	0.0	0.0	Ú.	-0.	0.	0.0	0.0	0.	-0.	٥.

	AI L	FORECAS	175	
	MMNG	24-4R	48-H₹	72-4
AVG FORFCAST POSIT FRANK	19.	114.	265.	34H.
AVG HIGHT ANGLE EROOM	15.	73.	164.	240.
AVG INTENSITY MAGNITUDE ERROR	5.	10.	32.	71.
AVG INTENSITY HIAS	-0.	-6.	-13.	-26.
NUMBER OF FORECASTS	21	17	13	•

#### TYPHOON CECIL

	HEST TRAC	ĸ	dARNTNG FRROR		HNIN FOREL	ASI HJ4S	48 MU((**	FOMFCAST FRADAS	12 4384 FAVEC451
40/J4/HR	POSIT WIN	P7517	WING DET WI	7 POST	¥1 ¥0 ∪>	[ 4]ND	POSIT WI	NU DSI WIND	CIPTS TO: CPER TECH
U40800Z	3.3 143.4 1	0.0 0.0	00.	. 0.0 0.	. 00	. n.	n.9 0.0	00. 0.	0.0 0.0 00. 0.
0408062	3.4 143.4 19	0.0 0.1	n 00.	. 0.0 0.	n 0v	. n.	n_0 0.0	UO. O.	n.u 0.0 0o. n.
040812/	3.6 143.3 19	0.0 0.0	n 00.	. O.n n.	# Qu	• n•	n.n 0.0	u0. 0.	n.0 0.0 0n. n.
0404187	3.8 143.1 19	0.0 0.0	n 00.	. 0.0 0.	n 0u		0.0	uu. 0.	n.0 0.0 Uu. 0.
040900Z	4.2 14Z.R 19	0.0 0.0		. 0.0 0.	n 0u	• ^•	0.0	UU. Q.	n.0 0.0 U0. n.
040406Z	4.6 142.5 1			. 0.0 0.			0.0	UO. O.	0.0 0.0 00. 0.
2516040	5.1 142.7 19			. 0.0 0.			0.0	00. 0.	0.0 0.0 00. 0.
0409182	5.5 141.9 20			. O.n n.		-	0.0	uu. a.	".0 0.n 0h. h.
041000Z	5.7 141.5 70			. 0.0 0.			0.0	00. 0.	0.0 0.0 00. 0.
0410062	5.9 141.1 20			. 0.0 0.			n.n 0.0	00. 0.	0.0 0.0 00. 0.
0410122	6.1 140.A 25			. 0.n ".			0.0	ua. o.	0.0 0.0 00. 0.
0410187	6.2 140.2 2			. O.n n.		_	n.() 0.0	v0. O.	0.0 0.0 00. 0.
041100Z	6.4 139.5 30			. 7.n 137.				U. 505.	4.2 141.2 50. 495.
0411062	6.5 139.0 30			7.7 134.				5. 59. 0.	4.5 140.6 55. 57. 0.
0411122	6.7 138.4 3			. 7.7 134.				D. 21. 9.	9.3 110.7 55. 4510.
0411182	6.9 137.a 30			. 7.1 137.				u. 27. O.	H.7 1/9.7 60. 7810.
0412002	7.0 137.3 39			. B.2 134.				0. 54. 5.	9.9 1/4.5 70. 465.
041206Z 041212Z	6.8 136.7 4			. B.n 131.				30. 10. 3. 124. 0.	4.6 1/7.6 75. 46. 4. 4.6 1/3.4 75. 1905.
0412182	7.0 136.0 40 7.2 135.5 49			. 7.6 134. . 7.7 134.				124. N. 15. 173. +5.	9.2 1/7.5 75. 228. 0.
0413002	7.5 134.8 44			. 7.7 134. . 7.8 137.				5. 13510.	4.5 1/5.5 75. 245. 5.
041306Z	7.7 134.2 4			8.3 131				5. 16810.	10.0 1/6.0 75. 245. 10.
0413127	B.D 133.4 4			. 8.9 131.				5. 20115.	10.0 103.2 60. 238. 0.
0413182	8.2 132.4 5/							5. 17410.	11.0 124.0 50. 15910.
0414007	B.3 171.6 5			9.7 128				u. 10510.	12.4 1/0.9 50. 415.
0414062	B.4 170.4 5			9.5 124				o. 11310.	11.7 119.3 55. 205. 0.
0414122	8.5 129.3 64			9.0 124				0. 100. 0.	12.1 117.9 65. 294. 15.
0414187	8.9 128.4 7/			9.7 124				0. 132. 0.	12.4 116.4 65. 361. 15.
0415002	9.4 127.5 7			10.3 124.				5. 123. 10.	12.8 117.2 70. 359. 25.
041506Z	10.1 126.5 7			11.9 123.				2. 160. 10.	13.8 115.6 70. 448. 25.
0415122	10.8 125.4 8			. 12.3 121.				5. 257. 15.	15.3 114.7 70. 536. 25.
0415182	11.5 124.4 70			. 12.0 120.				0. 360. 20.	17.2 114.9 75. 546. 30.
0415002	12.0 123.2 7/	11.9 123.		. 13.1 110.	3 65. 163	. in.	14.4 115.9 7	U. 415. 25.	14.5 114.5 75. An5. 25.
0415062	12.4 122.4 60			. 13.5 114.	A 65. 215	. 10.	15.1 115.4 /	0. 473. 25.	1H.2 115.6 75. 593. 25.
0416122	12.7 122.2 40	12,4 122.0	n 60. 13.	. 14.n jla.	A 65. 226	• 15.	15.6 115.8	0. 472. 25.	17.9 115.3 75. 445. 25.
0416182	12.9 172.1 6	13.0 121.0	5 60. 35.	. 14.2 11H.	4 65, 255	. 15.		U. 494. 25.	14.3 116.2 75. AAR. 25.
041700Z	13.1 122.1 5	12.9 122.		. 13.7 12n.				U. 337. O.	14.1 120.5 50. 514. 5.
0417062	13.5 122.3 5			. 13.A 121.				0. 379. 0.	16.5 119.3 50. 719. 10.
0417122	13.9 122.5 50			. 16.0 122.				5. 175. 5.	19.2 127.7 60. 339. 30.
0417182	14.3 172.A 50			. 16.4 124.				5. 156. 5.	19.7 1/9.3 60. 345. 35.
041800Z	14.6 123.1 4			. 16.2 125.				0. 167. 15.	19.6 1.13.7 60. 259. 35.
0418062	15.0 123.4 4			. 16.7 124.				0. 197. 20.	n.0 0.0 0n. n.
0418122	15.6 124.0 49			. 17.0 127.				0. 149. 30.	0.0 0.0 00. 0.
0418182	16.3 124.4 4			. 17.9 127.				0. 195. 25.	0.0 0.0 00. 0.
041-00Z	16.9 125.n 5			. 19.2 124.				4. 192. 25.	0.0 0.0 00. 0.
041906Z	17.5 125.8 S			. 19.0 130.			n.n 0.0	00. 0.	n.0 0.0 00. 0.
0419122	18.2 127.6 50			. 20.n 131.			n.0 0.0	00. 0.	0.0 0.0 00. 0.
041+182	19.6 127.A 5			. 23.A 134.				00. 0.	0.0 0.0 00. H.
0420002	21.0 129.1 4			. 24.A 13A.				00. 0.	
0420062	22.1 110.6 4							00. 0.	0.0 0.0 00. 0.
0420122	22.8 132.4 3							00. 0.	0.0 0.0 00. 0.
0420182	23.0 174.4 29			. 0.0 0.				00. 0.	0.0 0.0 00. 0.
042100Z	23.0 136.4 2	. 0.0 0.	n uo.	. 0.0 0.	.n C. +u	• ^•	0.0	00. 0.	n.0 0.0 00. n.

	41 L	FIRECAS	TS	
	SHNG	24-4R	48-43	72-48
AVG FORFAST POSIT FRHOR	15.	A7.	191.	320.
AVG HIGHT ANGLE ERONH	11.	62.	131.	215.
AVG INTENSITY MAGNITUDE ERROR	1.	7.	11.	14.
AVG INTENSITY REAS	1.	э.	7.	1).
NUMBER OF FORECASTS	40	37	33	23

#### TROPICAL STORM DOT

	TIREN WILL FIRE CHAPMA				1 46 = R	#n-25		54 HI	IIIK F	HECA:			48 40	hid F	PRECA			P2 4	UR F	nefC4	41
43/34/H2	POSET AL	\$11	PASIT	# INT	OST	~ [ Y 3	Pas		w 1 Vo	051	#1+0	909	TT	Or Lu	nst	dINO	400	. 1 •	disp	nsf	# 1 M()
0500007		15	0.0 0.		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.	0.0			-0.	
0500062		is	0.0 0.		-0.	o.	0.0	0.0	ŏ.	-4.			0.0						ō.	-0.	ā.
020005											0.	0.0		0.	-0.	٥.	^.0	0.0			
		15	0.0 0.		-0.	٥.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	٥.	-0.	٥.	n • 0	0.0	0.	-0.	٥.
0200185		14	0.0 0.0		-0.	0.	0.0	0.0	٥.	-v.	Λ.	Λ.0	0.0	0.	- v .	٥.	0.0	0.0	٥.	-0-	0.
0507007	4.3 143.4	15	0.0 0.0	٠ ٥.	-0.	٥.	0.0	n • n	0.	-0.	٠.	0.0	0.0	0.	-0.	0.	٥.٠	0.0	٥.	-0.	0.
050/06/	4.5 142.1	15	0.0 0.0	٠ ٥.	-0.	0.	0.0	0.0	٥.	-u.	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	9.	-0.	٥.
751/000	4.7 141.0	15	0.0 0.0	٠ 0.	-0-	υ.	0.0	0.0	0.	-0.	٥.	0.0	0.0	U.	-0.	J.	0.0	0.0	0.	-0.	٥.
050718/	5.3 139.A	ر م	0.0 0.		-0.	0.	0.0	0.0	0.		n.	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	٥.
0503002		20	0.0 0.0		-0.	Ü.	0.0	0.0	ŏ.	-0.	٥.	0.0	0.0	0.	-0.	õ.	0.0	0.0	ě.	-0.	ñ.
0504062		20	0.0 0.		-0.	ű.	0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	ő.	0.0	0.0	ě.	-0.	0.
0209152		20	0.0 0.		-0.	o.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	0.	0.6		· .	-0.	i.
0202185		20									_							0.0			
					-0.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	v.	-0.	٥.	0.0	0.0	••	-0•	8.
0504007		24	0.0 0.		-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	-0.	0.	n.0	0.0	٥.	-0.	0.
0204005		بر	0.0 0.0	- •	-0.	υ.	0 • n	0.0	٥.	-0.	n.	n , ()	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	٥.
0207152		25	0.0 0.0		-0.	0.	0.0	0.0	٥.	-0.	n.	0.0	0.0	0.	-0.	٥.	n.0	0.0	٥.	-0.	е.
0504182	7.3 133.2	24	0.0 0.0	ν υ.	-0.	0.	0.0	0.0	٥.	-0.	ο.	0.0	0 - 0	0.	-0.	0.	0.0	0.0	٥.	-0.	n.
0510002	7./ 132.0	25	0.0 0.0	٠ ٥.	-0.	0.	0 . n	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.
0510062	8.2 130.4	٩n	8.2 130-	20.	19.	-10.	9.4	127.0	25.	130.	0.	11.4	123.2	20.	162.	-10.	12.5	119.3	25.	6.	-5.
0510127	8.7 129.0	30	8.9 129.0		30.	+5.		125.4	JO.	123.	5.		121.6	20.	116.	-10.				111.	-10.
0510187	8.9 127.3	3 n	9.4 127.		46.	-5.		121.6	25.	104.	0.		119.7	25.	43.	-5.		116.5		219.	-5.
0511002		30	9.0 125.		30.	-5.		120.1	25.	65.	0		116.8		152.	ő.		115.9		255.	-5.
0511067		25	9.9 124.		13.	Ü.		110.4	25.	41.	-5		116.6		163.	0.		115.8		298.	0.
0511127		25	9.9 123			Ů.			25.												
					0.			114.3		35.	-5.		115-1		245.	-5.		113.3		474.	15.
		25	10.5 155.		6.	0.		117.3		134.	-5.		114.4		320.	-5.		113.0		531.	50.
		25	10.5 151.		9.	0.		117.7		124.	6.		114.4		379.	٥.		114.4		491.	55.
		10	10.5 120.		29.	-5.		114.4		175.	٠,		114.5		375.	10.		116.4		430.	25.
		30	10.7 119.		49.	-5.		115.4		243.	۰.		114.3		474.	20.		116.6		459.	75.
0512182	11.7 119.5	30	11.9 118.		36.	0.	15.0	117.0		193.	۸.	18.5	116-6	<b>&gt;0.</b>	299.	25.	20.6	122.5	50.	248.	25.
0513007	12.2 119.4	30	12.5 118.	7 30.	45.	0.	15.1	117.7	40.	167.	n.	14.3	119-1	٠O٠	277.	25.	21.0	123.2	50.	255.	25.
0513067	12.5 119.4	31	12.6 118.	7 3u.	41.	0.	14.7	117.9	40.	164.	۴.	17.1	116.1	٥a.	311.	25.	20.0	181.4	50.	351.	75.
0513127	13.0 119.4	15	13.1 119.	, 35 Č	24.	0.	15.7	119.5	40.	134.	15.	18.5	120.7	30.	238.	25.	21.1	174.6	40.	255.	15.
		40	13.7 119.		39.	-5.		119.7		154.	15.		121.3		241.	20.		195.1	35.		10.
		4.0	13.7 120.		0.	Ü.		121.4	25.	60.			124.2		119.	15.		128.0	45.		>0.
		36	14.0 120.		12.	ō.		122.8	30.	29.			125.7		121.	20.	0.0	0.0	0.	-0.	0.
		25	14.2 120.		31.	0.		127.A	30.	80.	Ξ.		125.5		244.	15.	0.0		ö.	-0.	ő.
			14.5 121.															0.0			
		25			31.	0.		123.4	30.	95.	٩.		126.5		307.	15.	n.0	0.0	٥.	-0-	٥.
		25	12.5 155.			v.		124.7	30,	104.	٤.		127.5	35.	365,	10.	0.0	0.0	0.	-0.	٥.
		55	15.4 123.		13.	0.		124.1		170.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	۰.
		25	16.2 154.		6.	0.		124.7		iei.	۲,	0.13	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
051518/	17.0 175.1	25	16.7 124.		25.	0.	18.0	127.9	30.	552.	۴.	6.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
0516002	17.8 126.2	25	17.6 125.	25.	21.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	
0516u6Z	18.8 127.5	25	0.0 0.	٠ ٥.	-0.	0.	0.0	0.0	0.		n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٠.
		25	0.0 0.		-0.	o.	0.0	0.0	õ.	-0.		0.0	0.0	ű.	-0.	ŏ.	n.D	0.0	Ď.	-0.	ě.
		25	0.0 0.		-0.	ō.	0.0	0.0	ŏ.	-4	0.	0.0	0.0	0.	-0.	ŏ.	0.0	0.0	ō.	-0.	0.
		کخ	0.0 0.		-0.	ō.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	ō.	0.0	0.0	ŏ.	-0.	ŏ.

	AI'L	FORECAS	15	
	HNG	24-4R	4B-H1	72+48
AVG FORFCAST POSIT FRHOR	23.	130.	244.	315.
AVG RIGHT ANGLE EROOR	16.	79.	171.	247.
AVG INTERSITY MAGNITUDE ERROR	2.	4.	13.	16.
AVG INTENSITY HTAS	-2.	3.	10.	13.
NUMBER OF FORECASTS	24	23	20	14

#### TROPICAL DEPRESSION 05

	4-51-1	Jark		444+146 244 145					11 H FC				4H H	net Fo				12 4	OUR Fr	IPF CA	ST.
					: 4	m 132				EMM.	J45				F 447.	15					
40/34/41	P3511 4	1 -11	w7511	-147	1151	+1 +3	Pai	NT T	-141	ادن	4 [ 4-13	4115	11	4140	OST	d I N()	404	<b>[ *</b>	#[4)	051	# ( MI)
051/00/	19.1 115.7	10	0.0 n	.n u.	÷0.	υ.	0.5	0.0	٥.	-0.	O .	0.0	0.0	0.	-0.	0.	0	0.0	0.	-0.	0.
401/00/	18.8 115.0	-0	it n ii	.n u.	-0.	0.	<b>₽</b> •0	0.0	٥.	- Ú •	٠.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	n.
051/12/	14.5 114.5	20	0.00	.n u.	- n .	υ.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0	0.0	0.	-0.	0.
191/187	10.7 114.2	10	<b>0.</b> 0 0	.n u.	-0.	u.	0.0	0.0	٥.	-0.		0.0	0.0	Ű.	-0	0.	0.0	0.0	0.	-0.	G.
U515007	17.8 114.0	14	0 0 0	.n u.	-0.	ď.	0.0	0.0	0.	-0.	٥.	0.0	0.0	υ.	-0.	0.	D = 0	0.0	٥.	-0.	a.
101516/	17.3 113.4	/5	0.0 0	·n u.	-0.	υ.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	9.0	0.	-0.	0.
1210151	16.7 113.7	10	U.n n	an u.	-0.	J.	0 • n	0.0	0.	- U -	n.	0.0	0.0	v.	-0.	٥.	0.0	0.0	0.	-0-	п.
/p1=1c0	10.2 113.4		0.0 0	.n u.	-0.	n.	0.0	0.0	٥.	-0.		0.0	0.0	Ú.	-0.	0.	0.0	0.0	0.	-0-	٠.
ひつままいひと	15.5 112.0	16	0.0 0	.n 0.	-0.	U.	0.0	0.6	0.	-0.	n.	0.0	0.0	Ű.	-0.	0.	0.0	0.0	0.	-0.	0.
ひつまずいわく	15.5 117.6	15	0.0	an u.	-0.	υ.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.
0214151	15.3 112.2	15	0.0 0	n u	-0.	0.	0.0	0.0	0.	-U.	0.	0.0	0.0	u.	-0.	ō.	0.0	0.0	0.	-0.	٠.
0214187	15.1 111.0	15	0.0 0	. n u .	-0.	υ.	0.0	0.0	0.	-0.	Λ.	0.0	0.0	0.	+0.	0.	0.0	0.0	0.	-0-	0.
U520U0/	15.0 111.4	111	0.0 0	.n u.	-0.	0.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
ひつとひひわり	15.7 112.2	10	0.0 0	.n u.	-0.	0.	0.0	0.0	0.	-v•	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
ひちとひまとり	16.5 112.4	10	0.0 0	•n v.	+0.	υ.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
025018/	17.6 113.2	20	0.0 0	en u.	-0.	0.	0.0	0.0	0.	-6.	٨.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	ο,
052100/	18.6 113.4	20	0.0 0	∙n u.	-0.	ν.	0.0	0.0	o.	-0.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1951767	19.3 114.4	10	U.O 0	.n u.	-0.	υ.	0.0	0.0	o.	-0.	n .	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0-	0.
125115/	20.1 115.4	10	0.0 0	.n U.	-0.	0.	0.0	0.0	0.	-v •	۰.	0.0	0.0	0.	-0	0.	0.0	0.0	0.	-0.	n.
1911500	20.4 116.4	69	0.0 0	.n n	-0.	υ.	0.0	0.0	Ó.	-u.	n.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
0522307	21.4 117.7	20	0.0 0	∙n ũ	-0.	0.	0 . n	0.0	ō.	-U.	n .	0.0	0.0	v.	-0	0.	0.0	0.0	0.	-0.	0.
0522067	21.6 119.0	20	0.0	∙n u.	-0.	0.	0 . n	0.0	o.	-U•	ο.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0-	ο.
0522121	21.7 120.4	25	0.00	.a u.	-0.	0.	0.0	8.0	0.	-0.	٠.	0.0	0.0	ű.	-0.	0.	0.0	0.0	0.	-0.	0.
7912260	21.8 172.1	15	0.0 0	.n u.	-0.	ø.	0.0	0.0	0.	- U •	n,	0.0	0.0	0.	-0.	0.	0.0	0_0	0.	-0.	0.
7006240	22.1 124.1	25	0.0 0	an U.	-0.	U,	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0523062	22.5 126.3	ŝη	22.5 126	. » 3n.	5.	0.	25.7	134.4	¢5.	76.	Α.	0.0	0.0	U.	-0.	0.	n.0	0.0	0.	-0.	0.
0523127	22.8 128.A	.in	22.4 128	. s 3u.	11.	0.	25.4	137.5	e5.	181.	Α.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
0253145	23.6 110.9	31	23.7 130	.7 30.	21.	0.	26.5	134.4	e5.	421.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
リラとキロリノ	24.9 172.4	15	24.5 133	an Ju	14.	5.	0.0	0.0	0.	- v •	n.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
0524067	20.6 114.4	25	25.5 134		6.	0.	0.0	0.0	o.	- v .	۸.	0.0	0.0	0.	-0.	ò.	0.0	0.0	0.	-0.	٠.
0524127	28.2 116.2	24	28.1 136	.1 25.	3.	n.	0.0	0.0	0.	-0.	**•	0.0	0.0	U .	-0.	0.	0.0	0.0	٥.	-0.	٥.
0254185	24.0 13A.n	25	0.0	.n v.	-0.	J.	0.0	0.0	0.	- u .	n .	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.

	AI'L	FIRECAS	TS	
	WHNG	>4 HR	44-44	72-48
AVG FURECAST POSTT FRHOM	12.	158.	0.	ο.
AVG HIGH! ANGLE ERROW	12.	150.	0.	n,
AVG INTENSITY MAGNETHOF FROM	1.	0.	0.	ο.
AVG INTENSITY HTAS	1.	0.	0.	0.
MINALD OF FRAFFAFTE				

#### TYPHOON ELLIS

	HEST THACK WARNING FRRORS							24 41	VIR FO	DHECA:	s f		48 H	oud Fr	IRFC4	ST		72 H	OUR FE	ner C4	41	
						ER	Rの45				EHH.	)4S				FRAD	35					
40/U4/HD	POSIT	w ( No	P 35	ŢΤ	#IN)	DST	WIND	FAS	11	₩1 <b>₩</b> 0	051	#IMD	PNS	1 1	₩I ND	951	<b>GIND</b>	POS	17	MI 49	951	MIMO
0624007	11.7 135.	- 50	0.0	0.0	0.	-0.	ο.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
062406Z	12.2 115.	0.5	0.0	0.0	υ.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
062+122	12.6 134.	5 20	0.0	0.0	0.	-0.	٥.	0.0	0.0	o.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0629187	12.9 134.	25 5	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
0630007	13.2 113.		0.0	0.0	0.	-0.	0.	0.0	0.0	ě.	-0.	ο.	0.0	0.0	Ű.	-0.	ė.	0.0	0.0	ō.	-0.	0.
063006Z	13.4 113.	5 30	0.0	0.0	U.	-0.	0.	0.0	0.0	Ď.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
0630122	13.5 133.		0.0	0.0	Ü.	-0.	o.	0.0	0.0	ŏ.	-0.	۸.	0.0	0.0	0.	-0.	o.	0.0	0.0	Ď.	-0-	0.
0630187	13.6 132.		0.0	0.0	ō.	-0.	o.	0.0	0.0	ō.	-0.	n.	0.0	0.0	ō.	-0.	ō.	0.0	0.0	Ö.	-0.	0.
0701002	13.7 131.			132.0	35		0.	14.5	124.4	45.	68.	eln.		127.4	50.		-35.		175.2	60.	223.	-5.
0701067	13.7 131.				40		õ.	14.4	129.0	45.			16.2			137.			124.2		235.	0.
070112Z	13.8 130.			130.9	40.		o.	15.0	12A.7		104.	•is.	14.5	126.4		199		18.7	124.0	60.	248.	0.
0701162	13.9 129.	5 50		129.1	50.	13.	o.	14.4	125.4	60.		.15.		121.6		173.			117.8	50.	197.	-10.
0702002	14.1 128.			A.RS	55.	ś.	ō.		125.3	65.		-2n.	15.6	121.0		205.	ŏ.		118.0	50.	225.	-5.
0702062	14.4 127.			127.4	55.	17.	-5.	14.0	123.4	65.	110.	.15	16.3		45.	191.	-15.	17.0	116.2	55.	205.	0.
070212/	15.0 176.	9 65	14.9	126.9	<b>55</b> .	5.	-10.	16.2	127.7	65.	111.	-14.	17.0	117.9	50.	149.	-10.	10.5	115.0	55.	1 40.	٥.
0702187	15.5 125.		15.4	125.8	55	ä.	-10.	16.5	121.4		127.		17.3		25.	171.	-5.	19.5	113.8	60.	103.	10.
0703002	16.1 125.	n 45	16.0	124.9	85	9.	0.	17.4	120.H	75.	77.	10.	19.6	117.2	90.	42.	35.	21.5	113.5	85.	111.	40.
0703067	16.8 124.			124.0	90	17.	10.	18.5	120.1	HO.	60.	Zn.	20.4	116.4	85.	47.		22.3	112.8	75.	150.	50.
0703122	17.8 123.			123.4	85	16.	5.	20.1	120.2	75.	40.	is.	21.9		75.	150.	50.	0.0	0.0	0.	-0-	0.
0703182	18.4 122.	4 70	18.4	122.7	70.	13.	0.	22.2	114.4	MO.	121.	20.	24.1	114.2	65.	197.	15.	0.0	0.0	0.	-0.	٥.
0704002	19.0 121.	9 65		121.3	60	0.	-5.	20.4	114.6	60.	21.	5.	21.7		50.	61.	5.	0.0	0.0	0.	-0.	٥.
0704062	19.5 120.			120-0	60	13.	o.	20.5	115.4	>5.	25.	٠.	22.1		40.	49.	15.	0.0	0.0	0.	-0-	0.
0704127	19.8 119.	4 40	17.7	119.0	60.	23.	0.	21.0	114.A	45.	49.	91n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
0704162	20.1 117.	9 60	20.1	117.9	60.	0.	0.	71.4	117.7	40.	51.	·in.	0.0	0.0	o.	-0.	o.	0.0	0.0	0.	-0.	n.
070500Z	20.2 116.	7 55	20.3	116.2	60.	ä.	5.	21.4	111.4	50.	16.	4.	0.0	0.0	ō.	-0.	ō.	0.0	0.0	٥.	-0.	0.
0705062	20.3 115.			114.9	60.		5.		109.7	40.	37.	15.	0.0	0.0	Ö.	-0.	ō.	0.0	0.0	Ö.	-0.	0.
0705122	20.5 114.			114.2	60.	6.	5.	0.0	0.0	ō.	-0.	٠,٠	0.0	0.0	o.	-0.	ò.	0.0	0.0	0.	-0.	٥.
0705187	21.0 112.			113.1	50.		ö.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	0.	-0.	ò.	n.0	0.0	0.	-0-	0.
0706002	21.6 111.			111.4		269.		0.0	0.0	õ.	-0.	0.	0.0	0.0	Ö.	-ò.	ě.	0.0	0.0	ō.	-0.	0.
0706062	22.0 110.		21.7	110.2	25.		0.	0.0	0.0	ě.	-0.	n.	0.0	0.0	ō.	-0.	ō.	0.0	0.0	ė.	-0.	n.

	A: L	FIRECAS	TS	
	HNG	24-4R	48-H3	72-48
AVG FORFCAST POSTT FAROR	25.	71.	145.	145.
AVG HIGHT ANGLE ERRON	21.	57.	103.	113.
AVG INTENSITY MAGNITUDE ERROR	3.	13.	19.	12.
AVG INTENSITY HIAS	-0.	-3.	-0.	۸.
NUMBER OF FORECASTS	22	15	14	11

# TROPICAL STORM FAYE

	HEST TRACK JAHVING FRROAS					2025		24 40	HH F	HELA:			48 HG	nd Fr	HECK!			16 4.	) set of	DNE C 45	1	
40/J4/H4	POSIT .	11 90	2351	T	41N1	DST	WIND	205	11	-140	160	4 ( MI)	905	11	4140	OST	dian	434	.11	4IV)	251	4190
0628182	2.8 155.0	15	0.0	0.0	0.	-0.	0.	0.0	0.6	0.	-0.	٠.	0.0	0.0	ű.	-0.	0.	0.0	0.4	0.	-0.	
0629002	6.5 154.5	15	0.0	0.0	o.	-0.	ō.	0.0	0.0	ŏ.	-0.	n.	0.0	0.0	ű.	-0.	ō.	0.0	0.0	U.	-0.	
7904290	2.6 153.9	15	0.0	0.0	o.	-0.	o.	0.0	0.0	o.	-0.	٥.	0.0	0.0	v.	-0.	o.	0.0	0.0	0.	-0.	0.
1214290	2. + 153.5	İs	0.0	0.0	ō.	-0.	ō.	0.0	0.0	ō.	-0.	۸.	0.0	0.0	u.	-0.	o.	0.0	0.0	ŭ.	-0-	8.
0629182	3.2 193.2	15	0.0	0.0	Ü.	-0	o.	0.0	0.0	ŏ.	-0.	n.	0.0	0.0	ű.	-0.	õ.	0.0	0.0	Ö.	-0.	0
063000Z	3.5 152.9	15	0.0	0.0	Ű.	-0.	υ.	0.0	0.0	ò.	-0.	0.	0.0	0.0	o.	-0.	0.	0.0	0.0	ű.	-0.	0.
0630062	3.9 152.5	Şn	0.0	0.0	o.	-0.	0.	0.0	0.0	Ö.	-0.	η.	0.0	0.0	0.	-0.	n.	0.0	0.0	0.	-0.	
0630127	4.4 151.R	50	0.0	0.0	ó.	-0.	0.	0.0	0.0	o.	-0.	٥.	0.0	0.0	ű.	-0.	0.	0.0	0.0		-0.	n.
3810690	4.9 151.2	50	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
0701002	5.3 150.4	20	0.0	0.0	υ.	-0.	0.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	Ū.	-0.	o.	0.0	0.0	0.	-0.	0.
070106Z	5.7 150.0	25	0.0	0.0	0.	-0.	υ.	0.6	0.0	0.	-0.	٥.	0.0	0.0	U.	-0.	0.	0.0	0.0	Ű.	-0.	0.
0701122	6.0 149.2	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	r.	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	Α.
0701182	0.2 147.0	25	6.R 1	49.7	25.	A5.	υ.	8.0	144.4	45.	140.	٠.	10.7	142.9	25.	130,	15.	17.2	144.2	62.	177.	35.
070200Z	0.5 146.4	25	6.5 1	45.8	30.	36.	5.	7.3	141.0	.0.	139.	10.	9.7	137.5	⊃u•	145.	10.	4.1	143.3	60.	1-6.	30.
0702062	7.3 145.5	54	7.0 1	45.1	3u.	30.	5.	7.0	141.2	٠0.	112.	5.	R.4	130.6	20.	140.	15.	4.4	112.5	60.	203.	15.
0742122	8.0 144.0	25	7.6 1	44.A	30.	25.	÷.	9.4	141,0	.0.	ju.	5.	in A	136.8	<b>&gt;0</b> .	60.	15.	12.3	116.5	60.	164.	35.
070218Z	8.6 144.1	3 n	9.2 1	43.A	30.	30.	o.	10.0	134.4	.0.	59.	n.	11.7	135.5	>p.	40.	20.	17.0	141.5	60.	142.	35.
07Q JUOZ	9.0 143.2	30	9.1 1	43.2	35.	5.	5.	11.1	134.7	>0.	48.	10.	12./	135.6	b0.	137.	30.	14.1	141.5	70.	147.	45.
<b>0703062</b>	9.4 142.2	35	9.4 7	<b>\$2.</b> 3	.0.	25.	٥.	15.2	134.4	no.	104.	24.		144.2	75.	211,	50.		1 40.0	<b>50.</b>	217.	55.
0703122	9.7 141.4	35	9.9 1	41.2	45.	13.	lu.	12.2	137.4		lov.	30.	15.1	133.5	15.	213.	50.	17.4	1/1.1	HO.	207.	57.
0703182	10.0 140.R	4.0	10.2 1		Ďΰ.	72.	10.	12.1	134.7		160.	40.	14.5	1 30 - 7	15.	2×5.	50.	17.7	1/5.4	80.	240.	40.
0704U0Z	10.3 179.4	40	10.2 1		ou.	17,	10.	11.4	137.5		lic.	40.	13.4		15.	25.	50.	15.1	1 40.3	A0.	47.	60.
0704062	10.5 139.0	35	10.4 1		45.	21.	10.	13.2	134.H	٩ŝ.	136.	40.	15.7			142.	50.	0.0	0.0	0.	-0.	4.
0704122	10.6 177.A	35	11.0 1	37.9	DO.	24.	15.	12.7	134.7	hō.	95.	• n •	14.0	129.8	/>.	125.	50,	P.0	0.0	0.	-0-	0.
070418Z	10.4 176.A	30	10.9 1	36 • 7	<b>75</b> .	30.	25.	12.3	132.2		141.	40.	14.1	127.7	75.	210.	55.	0.0	0.0	0.	-0.	0.
0705007	10.4 175.6	30	10.n t	35.7	25,	30.	25.	10.6	130.4		238.	40.	17.5	126.0	15.	320.	55.	0.0	0.0	0.	-0.	0.
0705062	11.1 135.5	25	10.2 (		50.	75.	25.		130.5		226.	30.	6.0	0.0	0.	-0.	٥.	11 . 0	0.0	0.	-n-	n.
0705122	11.9 135.1	25	11.1 1		J5.	47.	10.		133.4		250.	n.	0.0	0.0	0.	-0.	0.	·· 0	0.0	0.	-0.	٥.
0705187	12.6 174.6	25	11.5 1		35.	70.	10.	12.4	132.9	۷5.	535.	٠.	N.0	0.0	0.	-0.	٥,	P. 0	0.0	0.	-0.	٠.
070600Z	13.3 133.a	25	13.2 1		55.	5.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0706U6Z	13.8 113.4	25	13.9 1		25.	19.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	Ű-	-0.	0.	0.0	0.0	0.	-0.	٠.
0706122	15.2 171.9	25	14.5 1		45.	42.	0.	0.0	0.0	٥.	-0.	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.
0705182	16.1 170.7	50	0.0	0 • 0	0.	-D.	o.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	
970700Z	17.0 179.6	50	0.0	0.0	v.	-0,	0.	0.0	0.0	0.	-4.	n.	0.0	0.0	0.	-0.	0.	n.B	0.0	0.	-0.	п.

	AI L	FIRECAS	115	
	MMNG	>4-4R	48-H3	72-48
AVG FURFCAST POSIT FRHOR	35.	138.	167.	lan.
AVG RIGHT ANGLE ERDOR	21.	96.	97.	04.
AVG INTERSITY MAGNITUDE ERROR	9.	21.	37.	45.
AVG INTENSITY HTAS	9.	21.	37.	45.
NUMBER OF FORECASIS	21	17	14	1 2

#### TROPICAL DEPRESSION 08

	HEST THACK WARNING							24 4	nik Fi	DRECA:	1		48 M	out Fr	WFCA	<b>S</b> T		15 43	UR FO	HFC49	i T	
						7.0	Rn 35				EHH.	145				FRAN	45					
40/J4/H9	POSIT	WIND	פר פ	511	#IN1	OST	WIND	Pn	SIT	# [ No	051	#IMD	209	11	#IND	DST	#IND	209	1 *	4147	751	4140
0723062	19.5 140.	a 2n	0.0	0.0	Ü.	-0.	U,	0.0	0.0	0.	-u.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0723122	20.4 139.	0 20	0.0	0.0	0.	-0-	0.	0.0	0.0	٥.	-0.	۸.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	6.
0723182	21.2 137.	5 20	0.0	0.0	0.	-0-	0.	0.0	0.6	o.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
072400Z	22.0 115.	a 20	0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.0	0.0	o.	-0.	0.	0.0	0.0	٥.	-0.	0.
0724062	22.7 114.	20	24.3	133.4	20.	105.		28.0	124.2	20.	IAs.	ο.	20.0	119.0		396.		0.0	0.0	0.	-0.	0.
0724127	23.4 173.	n 2n	23.3	133.0	20.	5.	0.	25.0	127.2	20.	90.	٩.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	
0724182	24.0 131.						o.		127.0		203.	5.	0.0	0.0		-0.		0.0	0.0	ō.	-0.	n.
0725002	25.0 110.	20	26.	130.4	20.		0.		124.4		294.	-5.	0.0	0.0	ō.	-0.	0.	0.0	0.0	0.	-0.	0.
072506Z	26.0 128.			129.5		45.		0.0			-4.		0.0	0.0				0.0	0.0	Ď.		0.
9725127	27.4 127.		0.0				ŏ.	0.0				0.	0.0	0.0	0.			0.0	0.0	ò.		0.
0723187	29.4 127.		0.0	0.0				0.0	0.0			0.	0.0	0.0				0.0	0.0	ō.		0.
0726007	31.5 126.		0.0	0.0		-0	Ď.	0.0				0.	0.0	0.0	٥.			0.0	0.0	ö.		ő.
9726067	33.3 124.		0.0	0.0			o.	0.0			-0.		0.0	0.0		-0.		0.0	0.0	ō.		ů.

		AIL	FORFCAS	TS	
		MANG	24 - 4R	48-H3	72-48
AVG	FORECAST POSIT FRUCH	• 3.	195.	395.	0.
AVG	ALGUI ANGLE ERONH	>n.	70.	395.	n.
AVG	INTERSITY MAGNITURE ERROR	0.	4.	5.	α.
AVU	INTENSITY RIAS	0.	1.	-5.	0.
	400 -C CA 160400-		- 1		1

#### SUPER TYPHOON HOPE

	HEST THECK	I Al	RVING FRROAS	24 H	OIN FORECA		48 11	Dud FamfCas FARA		12 4	JUH FN	RFC451	ī
40/U4/H2	POSTT STAD	POSTT will	CMIW TRO CH	PostT		4[ND	POSIT			0511	CFIE	nST .	4140
0724067			)0. U.	0.0 0.0		0.	n_0 0.0	00.	0. n.		0.	-0.	0.
1214570	10.3 146.4 20		0. 4.	0.0 0.0		4.	0.0 0.0	00.	0. P.		0.	-0.	0.
0724162	10.3 146.2 20	0.0 0.0	0. 0.	0.0 0.0		٨.	n.0 0.0	00.	0. r.	0.0	٥.	-0.	n.
0752007	10.4 145.5 20		· -0. 0.	0.0 0.0		٠.	n_U 0+0	00.	0		٥.	-0-	n •
072506Z 072512Z	10.7 144.A 25		)n. 0.	12.5 140.4		10.	0.0 0.0 0.7£1 M.FI	0U. 35. 167.	0. n.	1 113.2		-0.	
072518/	10.9 144.0 25	11.0 144.1 25 11.1 143.0 25		12.7 134.4		15.	13.4 134.4	35. 246.		0 110.3		361.	16.
0726002	11.2 142.4 20	11.1 142.7 20			30. 92.	15.	17.4 134.8	35. 229.		9 140.4		325.	4
1404510	11.5 141.4 20	11.4 141.5 20		12.7 137.4		15.	17.4 133.4	Jo. 746.		2 179.2			-5.
0726127	11.8 140.7 20	11.4 140.R 2		13.0 137.0		lo.	14.1 132.7	35. 304.		7 178.5		345	
0726182	12.3 179.4 15	12.0 139.7 20		13.4 134.7		٠.	14.4 131.4	35. 305.		7 1/7.0		417	
0721002 0721062	13.2 140.3 15	12.7 139.7 20		14.4 135.4 0.0 0.0	25. 172.	٠.	14.0 131.4 n.0 0.0	30. 250. 00.	0. n.	0 0.0	0.	747	0.
0727122	15.0 139.4 20		). 34. 5. )0. 0.	0.0 0.0	00.	٠.	n.u 0.0	UO.	0. 0.			-0.	0.
072/182	15.4 138.4 25		0. 0.	0.0 0.0	00.	٥.	n.u 0.0	00.	0. 0.	0 0.0	ŏ.	-0.	0.
0724002	16.1 137.4 3n	16.2 137.A 25	65.	18.4 134.4	40. 160.	n.	10.7 129.4	50. 240.		3 1/5.2		257. •	
0728062	16.8 137.5 35	17.5 13H+A 2		20.7 134.4			27.1 133.1	50. 159.		9 179.5		1.9	
0729152	17.2 136.9 35	19.2 137.2 2		21.4 135.0			24.6 129.8	45. 345.		8 1/7.2		376	
07241H7 0729002	17.1 136.2 35	19.0 136.4 25 16.0 135.2 35	). 11410. ). 295.	22.2 131.5		-24	19.5 128.6	45. 197. 60. 45.		8 1/5.3		4n2	
0723062	16.6 175.4 50	16.2 135.1 40		16.7 132.4		•30.	17.1 130.1	60. 185.		6 147.2		341.	
0724122	10.5 114.9 45	16.4 134.0 6	9, 0,	17.1 132.4		<b>1</b> 10.	10.1 129.3	85. 192.		3 1/5.7		321. •	
072+182	16.7 134.2 /0	16.9 134.5 7		17.7 131.4		410-	10.7 128.7			6 1/5.1		39A	
073000Z	16.8 113.4 74	15.4 133.4 /		18.0 130.2		min.		100. 214.		9 1/2.9			-5.
073006/ 073u12/	17.1 132.7 MA	17.4 132.4 di		18.2 120.4	110. 121.		10.4 125.8	100. 269.		0 1/2.3			15.
0734182	18.0 130.4 40	17.5 (31.1 45			110. 197.		20.2 124.9			3 1/0.8			60.
0731007	18.6 129.4 100	19.5 129.3 100	A. 0.	20.5 124.4	110. 90.	450.	22.0 120.0			0 115.2			40.
0731062	19.3 127.4 115	13.5 158.0 10			110. 104.		22,4 117.9	80. 225.		B 113.8		479.	
0731127	19.6 126.2 130	19.7 126.0 130		21.5 120.1		٠.	24.0 115.7	35. 233.			0.	-0-	n.
0401002	20.1 124.7 110	20.1 124.4 130		22.4  11.2 22.4  17.2		*15.	25.0 115.1 0.0 0.0	25. 373. 00.	•25. n.		0.	-0.	0.
0801062	20.8 121.4 175	20.8 121.5 125		22 / 114.0			0.0	U0.	0. 0.		v.	-0.	Π.
0801157	21.5 120.1 120	51.4 15" 120		21.0 114.5		•2n.	n.II 0.0	00.	0		0.	-0.	n.
0801185	21.7 118.2 115	21.9 1180- 11	o. 15. O.	23.4 111.4			0.0	00.	0. n.		0.	-0-	0.
0805067	22.2 116.4 105 22.2 113.0 HS	22.0 116.5 1U		22.4 110.4 23.1 104.5		10.	0.0	00. 00.	0		0.	-0.	0.
0805127	22.7 111.7 70	22.4 114.0 VI		0.0 0.0		0.	n_0 0.0	U0.	0. n.		0.	-0.	0.
1812080	22.6 109.4 50	22.7 110-1 6		0.0 0.0		0.	0.0	00.	0. n.		0.	-0.	n.
060 100 5	22.2 107.9 35	22.5 10R.n 35	. 33. U.	0.0 0.0		n.	n.ii 0.0	UO.	0. ".		0.	-0.	n.
000 3067	21.7 115.4 30		n. 0.	0.0 0.0		٠.	0.0	UO.	0. "-		0.	-0.	n.
0807187 0807157	21.1 103.1 20 20.8 101.7 20		)n. 0.	0.n n.n		0.	0.0	00.	0. 0.		0.	-0.	0.
0404002	20.7 100.4 20		0. 0.	0.0 0.0			0.0 0.0	U0.	0. 0.		ő.	-0.	0.
0804062	20.7 99.2 20		0. 0.	0.0 0.0			0.0	U0.	0. 0.		a.	-0.	0.
080+12/	20.7 47.9 15		00. 0.	0.n n.n		۰.	n.0 0.0	00.	G. n.		0.	-0-	0.
0804182	20.9 96.7 10		)n. u.	0.0 0.0		n.	0.0	00.	0			-0-	0.
080500Z 080506Z	21.2 35.4 10 21.5 34.5 15		3n. 0.	0.0 0.0		٥.	0.0 0.0	00.	0. 0.		0. 0.	-0.	0.
0803082	21.7 43.5 15		0a. 4. Da. 9.	0.0 0.0			0.0 0.0	00.	0. 1.		0.	-0-	0.
0805182	22.2 12.7 20		n. Q.	0.0 0.0		۸.	0.0	00.	0. n.		0.	-0.	n.
0806U0Z	55.3 45.0 SU	0.0 0.0	vo. o.	0.0 0.0		r.	0.0 0.0	UO.	0. n.		0.	-0.	n.
UB06067	22.3 91.4 25		vn. 0.	0.0 0.0		٥.	0.0	00.	0. 0.			-0.	8.
080612Z 080618Z	22.2 90.4 25 21.0 00.1 25		vo. o. oo. v.	0.0 0.0		٠.	n.0 0.0	00.	0. 0.		0.	-0.	0.
0807007	21.7 49.7 25		v0. u. v0. u.	0.0 0.0		0.	0.0 0.0	00.	0. "		7.7	-0.	0.
0807062	21.7 49.		00. 0.	0.0 0.0		٥.	0.0 0.0	00.	0		ō.	-0.	0.
0807122	21.8 88.3 35	0.0 0.0	00. 0.	0.0 0.0		۰.	0.0	00.	0. 0.		0.	-0.	0.
0807187	22.2 47.2 30		oo. o.	0.0 0.0		۸.	0.0	v0.	0. 0.		0.	-0.	0.
080400Z 080406Z	22.4 96.4 29 22.5 95.5 25		00. 0. 00. 0.	0.0 0.0		ñ.	n_0 0.0	00.	0			-0.	n.
0806122	22.5 94.4 20		00. 0.	0.0 0.0		n.	0.0	00.	0. 0.		ű.	-0.	n.
				• • • • • • • • • • • • • • • • • • • •		ŕ		••					

	AI L	FIRECAS	T5	
	MNG	24-4R	48-H3	72-48
AVE FORFCAST POSIT FRHOM	23.	134.	265.	37h.
AVG HIGHT ANGLE EROOM	16.	75.	140.	lon.
AVG INTENSITY MAGNITUUF FREDR	3.	14.	22.	74.
AVG INTENSITY RIAS	-1.	-9.	-19.	-14.
NUMBER OF FORECASTS	33	2+	> 3	21

#### TROPICAL STORM GORDON

	4651	INACK			24KVI	NG			24 H	41M F	UHELA:	s f		45 M	0114 F	MFCA			12 4:	WR FE	narca1	L1
						- 01	2045				ERN.	145				F#41	14					
40/34/89	POSIT	<b>21 YO</b>	₽as	7 T	dINT			Pns	t T	4140	וכנ	d[n()	POS	113	WIND	nSī	#IND	100	11	4117	ารโ	4 ( m)
1510510	18.8 1 12.		0.0	0.0			0.	0.0	0.0	0.	-0.	٠,	0.0	0.0	Ű.	-U.	0.	0.0	0.0	0.	-0.	•.
0725187	19.0 111.0		0.0	0.0	0		Ü.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	٠.
0726002	19.5 110.		0.0	0.0		-0.	Ů.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ď.	-0.	0.	0.0	0.0	0.	-8.	
0720067	1949 129.		0.0	0.0	ő.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.8	0.8	0.	-0.	0.	0.0	0.0	٥.	-0.	в.
0720122	50.2 128.			129.5		45.			127.7		2000			125.2		305.	-5.	25.8	1/2.4	60.	449.	48.
									12A.H					124.3		324.	0.	0.0	0.0	٥.		0.
0159181	20.4 127.			154.0			-10.							110.5		43.	ő.	0.0	0.0	ō.		
072/002	20.5 176.			150.5				21.4				•15.								ŏ.		
072/06/	20.6 125.						-5.		151.4			•ln•		117.8		100.	.5.	B • 0	0.0			
0727122	20.8 124.	2 50	20.7	124.7	٠0.	6.	-lv.	21.2						115.6			30.	^.0	0.0	٠.		•
072/182	20.6 122.	A 55	20.9	123.1	45.	17.	-10.	21.4	lla.I	75.	70.	٠.	6 ° 0	0.0	٥.	-0.	٥.	٠.٥	0.0	٠.		•
0728002	20.9 121.	7 60	20.4	121.5	o0.	13.	-10.	20.0	114.2	65.	150.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	9.	-0.	٠.
0728U6Z	21.3 120.	. 40	20.3	120.5	35.	79.	-5.	20.9	115.4	10.	130.	25.	0.0	0.0	0.	-0.	٥.	0.0	0.0	۰.	-0.	٠.
072812/	22.0 120.			150.7	55.	6.	ŭ.		114.2		211.	6.	0.0	0.0	0.	-0.	0.	0.0	0.0	9.	-0.	۸,
u728182	2245 118.			119.1		33.	š.	0.0	` 0.0			0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	•.
072+002	22.7 117.			117.3		9.	ő.	0.0	0.0			0.	0.0	0.0		-0.	ō.	0.0	0.0	ō.	-0.	
									0.0			0.	0.0	0.0			o.	0.0	0.0	٥.		٠.
0724067	23.1 116.			116.2	45.	11.	٠0.	0.0				-	0.0	0.0		-0.	ŏ.	0.0	0.0	Ď.		
0154755	23.1 114.	1 50	23.5	115.7	JU.	30.	10.	0.0	0.6	٥.	-0.	٠.	10 , 11	0.0	0.	-0.	٠.					

	AI'L	FORECAS	15	
	HHNG	24-4R	48-43	72-49
AVG FORFCAST POSTT FRHOR	23.	129.	173.	444.
AVG RIGHT ANGLE ERAPH	12.	90.	151.	274.
AVE INTENSITY MAGNITUUF ERRUR	6.	11.	э.	AP.
AVG INFENSITY HTAS	- 3.	1.	5.	40.
MUMMER OF FORECASTS	13		5	1

## TROPICAL DEPRESSION 11

	HF\$1	THACK			JAHV				26 40	11 M F				48 m	Just F				12 4	JUH FE	19664	41
						: Q1	41135				ENM.	)4S				► B 43.	7 <b>4</b>					
40/J4/HD	F3517	-141	ودب	11	HINT	DST	WINT	Pne	t y T	4140	υsί	4 [ ***)	Pri:	116	dind	051	#1 NO	100	517	WI VJ	nsi	4 [ 40
1805181	11./ 135.	4 15	0.0	0.0	v.	-0-	u.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	٠.	-0.	٥.	0.0	0.0	٠.	-0.	
0405155	12.3 114.	9 14	0.0	0.0	υ.	-0.	U.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	
0805191	12.0 110.	4 15	0.0	0.0	v.	-0.	U.	0.0	0.0	0.	-4.	۸.	0.0	0.0	ø.	-0.	٠.	0.0	.0	٠.	_0.	
9893907	13.4 133.	1 15	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	ø.	-0.	٠.	0.0	0.0	٠.	-0.	
9003062	13.7 132.	1 15	14.0	131.7	lo.	24.	v.	15.4	124.0	25.	60.	٩.	17.9	123.7	jo.	164.	10.	24.4	118.6	50.	145.	15.
1516080	14.2 131.	3 IS	14.4	130.7	₹0.	37.	٠.	16.2	127.0	30.	6/.	10.	14.4	122.7	37.	158.	10.	20.9	117.5	50.	156.	15.
1615080	14.5 110.	4 20	14.4	154.4	₹0.	47.			124.2		los.	15.	14.5	155.2		ING.	25.	0.0	0.0	٠.	-0.	
9444447	14.4 129.	4 50	14.0	129.7	ev.		0.	16.0	124.0	40.	***	10.	14.7	155.0	.0.	74.	20.	P.0	0.0	٠.	-0.	
8804067	15.3 179.	1 20	15.7	124.5	20.	42.	0.	16.5	127.4	40.	4155	٠.	20.1	118.4	.0.	197.	25.	0.0	0.0	٠.	-0.	
2514080	16.0 128.	20	16.0	124.4	20.	121.	v.	18.0	122.7	25.	193.	۸.	20,2	116.0	jo.	137.	20.	0.0	0.0	٥.	-0.	
080+18/	16.7 178.	0 20	16.7	125.4	20.	144.	0.	19.0	121.4	25.	lise.	٩.	0.0	0.0	٥.	-0.	٥,	0.0	0.0	٠.	-0-	8.
000007	17.7 127.	4 20	17.5	127.4	25.		٥.	20.4	124.7	30.	44.	ı۸.	0.0	0.0		-0.	٥.	4.0	0.0	٥.	_0.	
0805062	14.6 176.	5 24	18.5	158.2	25.	95.	0.	22.0	124.4	10.	285.	14.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0-	
0MU312/	19.1 125.	4 /4	19.5	125.4	25.	30.	0.	23.0	121.1	30.	132.	15.	0.0	0.0	0.	-0.	8.	r.0	0.0	٥.	-6.	٠.
8803187	14.2 174.	1 20	19.5	124.4	25.	29.	5.	0.0	0.0	0.	-0.	r.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.
*****	19.5 121.	0 50	19.7	123.1	25.	17.	٥.	0.0	0.0	0.	-0.	۸,	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	
0006067	20.6 121.	9 15	20.0	122.2	en.	40.	5.	0.0	0.0	0.	-0.	n.	0.0	0.0	v.	-0.	٥.	0.0	0.0	٥.	-0.	
0840155	21.0 120.	1 16	20.4	120.5		13.	5.	0.0	4.0	a.	-4.	٠.	0.0	9.0	٥.	-0.	0.	0.0	0.0	٥.	-0-	

	A, F	FORECAS	15	
	AKNS	24 - 4R	64-44	72-48
AVG FORECAST POSTE FRANCE	47.	144.	134.	171.
AND SIGHT ANGLE ESHOR	30.	94.	83.	124.
AVG INTENSITY ANGUITHDE ERROR	2.	9.	19.	15.
AVG [NTENSILY HIAS	2.	9.	19.	35.
NUMBER OF FURECASTS	14	10	6	,

#### TYPHOON IRVING

	AFST	THACK		WARY		1095		54 HI	HH F	DHELA:			46 H	Dirt Fr	PFC4			92 H	OUR FR	PFC4	<b>k</b> Ţ
40/J4/HP	P3511	WIND	POSIT	#IN1		WIND	Pns		WIND			POS	517	WIND		JIND	PDS	1 +	#1 4D	nst	w140
0807127	14.0 137.7		0.0 0.		-0.	0.	0.0	0.0	0.	-0.	٠.,	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0807182	15.0 138.0		0.0 0.		-0.	ŏ.	0.0	0.0	ŏ.	-0.	٥.	0.0	0.0	ű.	-0.	ŏ.	0.0	0.0	ů.	-0.	0.
2006060	15.6 138.1		0.8 0.		-0.	ō.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ď.	-0.	٥.
9805067	16.4 138.0		0.0 0.		-0.	Ö.	0.0	0.0	ě.	-0.	۰.	0.0	0.0	0.	-0.	ò.	0.0	0.0	0.	-0.	0.
0804151	16.8 117.5	. 25	0.0 0.		-0.	o.	8.0	0.0	o.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
9808185	17.4 136.4	. 25	0.0 0.	n o	-0.	o.	0.0	0.0	0.	-0.	٨.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	8.
1004080	17.7 136.0	30	17.9 136.	A 30.	6.	0.	19.9	132.4	35.	103.	٩,	21.0	124.2	45.	229.	15.	21.5	126.0	55.	719.	5.
080 <del>3</del> 067	18.0 115.4	30	19,3 135.	1 30	29.	0.	21.0	130.1	40.	188.	10.	21.7	124.5	٥O.	344.	15.	22.0	118.5	60.	528.	5.
2514040	16.2 114.5	3 n	19.3 135.		23.	۰.	19.7	137.7		150.	10.		129.5		264.	10.		1/3.5	60.	266.	5.
0604761	18.3 174.7	30	18.0 135.		49.	υ.		134.4		287.	10.		130.8		245.	10.		125.0		211.	0.
0810005	18.4 133.7		10.5 133.		13.	-5.		130.4		183.	5.		126.8		162.			182.5		742.	-50.
0410062	18.4 172.2		19.4 132.		37.	-5.		154.4		224.	Λ.		126.0		179.			171.3		101.	-25.
0810122	10.3 131.1		18.7 131.		29.	٥.		127.1		196.	٠.		123-4		243.			118.8		199.	
0010187	18.0 129.1		10.7 130.		44.	v.		150.7		198-	٠٠.		121.4			-15.		116.9		442.	+50.
0811005	17.2 17A.A		17.3 128.			٥.		124.4		187.	-5,		120.4			-25.		115.5		572.	-55.
0811167	16.5 128.5		17.0 127.		50.	-5.		123.7		200.			119.4		473. 341.			114.5		413.	-25.
0011107	17.5 178.4		17.2 129.		21. 31.	-5. -5.		125.4	***	80. 105.	•10.		121.5		330.			116.7			
0815005	17.8 127.4		17.5 128.		39.	5.		125.5		103.	0,0		121.7		321.			117.5		515.	-50.
0815067	10.4 127.1		17.9 127.		39.	ů.		124.4		168.			120.9		364.			116.7		597.	
0815152	18.7 176.9		18.5 126.		26.	ŏ:		127.4		213.	-5.		119.6			-10.		115.5		483.	
0812182	19.2 126.4		18.4 125		61.	-5.		122.4		250.	-5.		118.8		419.			115.5		713.	
0013007	20.0 126.7		20.1 126.		8.	0.		124.0		50.	٥.		127.5		193.			141.0			-10.
18067	21.1 126.4		21.1 126.		11.	0.		120.4		₹36.	٥.		128.5		749.			132.9			-10.
0613155	22.0 126.0	70	22.0 126.	A 70	33.	0.	25.0	127.0	75.	150.	-5.	79.5	129.0	80.	303.	-10.	31.7	132.9	80.	467.	-5.
0013107	22.7 125.2	70	23.2 125.	7 70.	41.	0.	27.4	127.1		203.	٠٩.	31.0	131.2	85.	416.	-5.	32.6	137.0	85.	453.	٩.
0614407	23.5 125.6	75	23.7 125.	1 70.	13.	-5.	27.4	125.4	BD.	128.	-ln.	31.8	127.2	80.	273.	-10.	35.0	190.6	70.	292.	0.
0014062	24.0 124.5		24.1 124.	a 75.	٩.	٥.	27.4	125.2	45.	66.	-5.		150.8		143.		34.5	130.0	70.	174.	15.
0814155	24.6 124.4		24.6 124.		16.	٥.		124.7			10.		126.7					129.0		167.	55.
081+187	52.5 154.4		25.3 124.		۹.	٥.		124.4		51.	14.		150.5			30.		149.5		301.	55.
0615007	25.9 124.1		25.7 124.		13.	٥.		124.0		68.	10.		124.7			30.		197.5		524.	55.
0812065	26,9 124.1		26.5 124.		29.	٥.		124.2	95.	86.			125-1		201.	35.		128.3		626.	50.
9015127	27.5 123.1		27.5 123.		11.	٥.		121.4	45.	72.	in.		125-1		270.	60.	0.0		٥.	-0.	0.
08151HZ 081600Z	28.5 173.1		20.3 123.		13.	º.		127.4	45.	76. 39.	15.		126.0		395.	35.	0.0		٠.	-0.	٥.
0419095	30.6 123.1		29.5 123. 31.1 123.		6. 30.	5. 0.		124.5	45. He.	68.	15. 25.		127.7		347.	35. 20.	0.0	0.0	0.	-0.	0. P.
0819155	31.7 123.7		31.6 153.			5.		124.5		219.	50.	0.0	131.2	73.	-0.		0.0	•.•	0.	-0.	0.
9819182	32.8 124.0		32.9 123.		10.	0.		124.7		285.	50.	0.0	0.0	٥.	-0.	0.	7.0	0.0		-0.	٥.
001700Z	34.0 125.0		34.1 124.			ŏ.		124.4			24.	0.0	0.0	ŏ.	-0.	ě.	0.0	1.0	· .	-0.	ä.
001706Z	35.6 126.7		35.2 126.		34.	5.		130.9		362.	10.	0.0	0.0	٥.	-0.	0.	0.0			-0.	
0917122	37.1 120.9		36.6 128		31.	ō.	0.0	0.0		-0.	۸.	0.0	0.0	0.	-0.	ě.	0.0			-0.	
9617182	39.5 131.4		38.9 131.		36.	5.	0.0	0.0	ě.	-0.	n.	0.0	0.0	0.	-0.	ō.	0.0	0.0		-0.	
081 000 Z	42.0 113.4		42.1 134.	1 25.	36.	ō,	0.0	0.0	i.	-0.		0.0	0.0	0.	-0.	ě.	0.0	0.0	Ů.	-0.	
6814665	14,2 175,7	25	44.9 137.	n 25.	81.	0.	0.1	0.0	0.	-0.	٠.	n.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	•.

	AI'L	FORECAS	75	
	HHMG	24-4件	FM-B4	72-48
AVG FORFCAST POSTS FRHOR	26.	163.	286.	441.
AVU 41641 AVOLE EJOOR	17.	98.	203.	344.
AVE INTENSITY MAGNITUDE ERROR	2.	11.	19.	20.
AVG INTERSITY BIAS	-0.	6.	3.	-1.
MIMAGR OF FRAFFARTA	30	3.	3.0	94

#### SUPER TYPHOON JUDY

	HFST	TRACK			dakut		1045		24 40	YW F	PHELA: EHH,			48 #6	nd Fr	## C4			12 4.	OUN Fr	DPF C &	41
40/04/H9	POSIT	WIND	POS	1 T	CHIL	OST	WINS	Pne	* T	WIND	ast	4140	905	17	-Lup	057	41ND	POS	11	#1 V3	751	at 1 40)
0615122	10.5 151.	0 15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.		0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	
081518Z	11.3 150.		0.0	0.0	6.	-0.	Ŏ.	0.0	0.0	ě.	-0.	٥.	0.0	0.0	ű.	-0.	ě.	0.0	0.0	0.	-0.	
9816002	11.8 149.	0 15	0.0	0.0	υ.	-0.	o.	0.0	0.0	ě.	-0.		0.0	0.0	v.	-0.	i.	0.0	0.0	o.	-0.	0.
0816067	12.3 147.		0.0	0.0	ō.	-0.	ě.	0.0	0.0	i.	-0.	0.	0.4	0.0	ŭ.	-0.	0.	0.0	0.0	0.	-0.	a.
1516180	12.8 146.		0.0	0.0	Ü.	-0.	ö.	0.0	6.0		-0.		0.0	0.0	Ŏ.	-0.	ő.	0.0	0.0	i.	-0.	0.
0616182	13.3 144.			144.5	35.	21.	5.		140.3	00.	107.	10.		136.5	70.	192.			112.9	85.	210.	-40.
981700Z	13.8 143.				90	13.	45.		134.3	90.	64.			134.5	70.		-40.		131.4	85.	144.	-45.
0817062	14.2 142.	2 35		142.0	40.	15.	5.	16.3	137.4	no.	52.	*15.	10.6	133.0		121.			1/9.0	65.	248.	-50.
0817122	14.5 141.			140.6	45	30.	š.		135.4		111.	•15.		130.9		221.			127.0			-50.
0817182	15.0 140.			139-4	50	35.	o.		134.5		114.			130.0	15.	257	-50.		176.4		312.	-40-
081800Z	15.7 139.	0 55	15.4	138.9	55.	19.	ō.		134.1		101.		19.3			239.			126.7		766.	-30.
081806Z	16.4 138.	> 75	16.0	137.6	60.		-15.		133.1		150.			124.0		245.			125.7	90.	247.	-20.
081812Z	17.1 137.	3 40	16.8	137.3	70.	18.	-10.	18.7	133.4		*>.	•35.	20.2	129.1		245.			175.8	95.	774.	٠٠.
0919192	17.6 136.	4 90	17.4	130-4	75.	12.	-15.		132.4	H5.	121.	940.	21.1	128.2		217.		24.0	1/5.3		198.	-5.
2006100	18.2 175.	4 110				6.	0.		132.1		99.	۸.	22.4	129.5			15.		148.5	135.	40.	40.
081 706Z	19.0 135.		19.9	135.0	115.	8.	o.	21.3	131.5	130.	104.	-5.	21.5	129.0	133.	97.	25.	24.2	178.9	135.	111.	45.
0819122	19.7 134.	7 120	19.7	134.5	125	11.	5.		131.2		81.	n,	25.0	129.5	135.	42.	35.	27.7	129.7	125.	240.	35.
081918Z	20.5 134.	4 125	20.2	134.2	130	21.	5.	72.3	132.3	135.	۶ż.	10.	24.6	130-5	135.	45.	35.	27.3	1 30.3	125.	251.	40.
082000Z	21.3 133.	a 130	21.3	133.4	135	0.	5.	74.5	137.7	135.	89.	15.	27.3	133.2	135.		40.	20.6	197.1	125.	449.	64.
0020062	22.2 173.	2 135	55.5	133.7	135.	0.	0.	25.4	131.5	135.	97.	25.	28.5	133.0	1320	375.	45.	30.6	117.2	115.	Tnd.	30.
2510540	22,7 132.	4 135	23,1	132.A	135	26.	0.	76.4	130.7	120.	134.	Z٠.	20.2	130.0	110.	360.	20.	31.6	144.5	95.	416.	10.
0850185	23.1 131.	9 125	23.3	131.2	130.	40.	5.	25.1	124.A	115.	151-	15.	27.4	125.3	105.	170.	20.	31.3	176.5	90.	757.	10.
085100Z	23.4 131.	1 120	23.4	131.0	120.	5.	٥.	24.5	124.0	110.	٠.	14.	74.7	125.7	100.	24.	15.	30.0	175.8	85.	170.	٠.
085109S	24.2 110.	A 110		130.4		16.	5.	24 . n	130.4	105.	160.	15.	24.2	127.7	→o.	176.	5.	32.5	147.5	85.	316.	15.
085115Z	24.3 179.	A 100	24.5	129.4		12.	15.	26.4	127.0	100.	155.	20.	2A.7	125.7	90.	127.	5.	31.2	176.1	60.	109.	20.
0851185	24.4 128.	9 100	24.7	128.7		21.	15.	27.0	124.7	100.	110.	15.	29.7	124.5	70.	91.	10.	31.6	1/5.1	75.	142.	₽#.
082200Z	24.4 128.	0 95	24.4	127.8	90.	11.	٠5,	25.0	124.4	65.	43.	-2^·	27.7	1-251	<b>&gt;0.</b>	73.	-30.	29.9	119.9	25.	175.	-30.
045504S	24.4 127.	5 90		127.7	45.	16.	-5.		124.4	60.		•2¢.	27.7	121.6	٥o.	104.	-20.	30.1	117.7	25.	715.	-25.
0055155	24.5 127.			156.4	85.	16.	-5.		124.1	60.	151.			121.5		177.		n.0	0.0	0.	-0-	۹.
0855187	25.1 126.			156-1	80	21.	-5.		121.3	>5.		925.		121.0		114.		n.0	0.0	٥.	-0.	0.
0853005	25.0 125.			125+7	65.	5.	٠.		127.1	70.		•l∩•		150.0		135.		0.0	0.0	٥.	-0.	٥.
082306Z	26.9 124.		26.7		90.	20.	-5.		121.5	50.		•5u•		119.4		215.		0.0	0.0	٥.	-0.	۸.
0823122	27.5 123.		27.5		80.	0.	-5.		120.7		100.		0.0	0.0	0.	-0.	٥.	0.D	0.0	0.	~P.	۰.
082318Z	28.2 123.			153.4	80.	16.	0.		150.1		134.		0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	٥.
0854005	28.7 122.		28.4		70.	12.	-10.		150.3		144.		0.0	0.0	٥.	-0.	٥.	٠.٥	0.0	0.	-0.	٠.
082406Z	29.3 172.			155.2	45.	24.	-5.		150.5		181.		0.0	0.0	٠.	-0.	0.	0.0	0.0	٥.	-0.	0.
085+155	29.8 122.		29.9		25.	17.	-5.		150.4		18/-	-10.	0.0	0.0	9.	-0.	٥.	0.0	0.0	٥.	-0-	0.
0824182	30.4 172.			155.5	55.	29.	٥.		150.7		24/+		n.0	0.0	٥.	-0.	٥.	٥.٠	0.0	٥.	-0.	٥.
082-00Z	30.9 123.			155.4	5u.	21.	-5.		123.2	₹5.		۰.	0.8	0.0	٥.	-0.	٥.	P . 0	0.0	٥.	-0.	۵.
082506Z	31.4 123.			123.5	45.	. 5.	-5.		F. 451	25.	•1•	٠.	0.0	0.0	v.	-0.	٥.	n.0	0.0	٥.	-0.	n.
0825122	31.8 124.			124-1	<b>*0.</b>	13.	٥.		127.2	25.	60.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	
0625182	32.5 125.			152.3	35.	15.	5.	0.0	4.0	٥,	-0.	٠.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	٥.
082600Z	33.2 126.		33.6		30.	39.	5.	0.0	0.0	0.	-0.	n.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	۰.
0826062	33.9 127.			127.4	₹5.	39.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	٥.	n.0	0.0	٥.	-0.	о.
0826152	34.4 128.	5 20	0.0	0.0	۰.	-0.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0-	۰.

	AI'L	FORECAS	TS	
	MMMG	24-4R	FM-RA	7>-4
AVG FORFCAST POSTT FRHOR	19.	105.	173.	277.
AVE RIGHT ANGLE ERDOR.	12.	Al.	139.	213.
AVS INTENSITY MAGNITUDE ERROR	6.	16.	29.	PA.
AVE INTENSITY HEAS	1.	-7.	->.	-1.
NUMBER OF FOOFCASTS	30	34	27	23

## TROPICAL DEPRESSION 14

	HEST	TRACK		dakut	NG			24 40	11H F	HECA	s f		48 H	0114 F	)RFCA	ST		12 4	JUN Fr	PFCA	41
					÷ R	Rnas				EHH	<b>)45</b>				FPRA	35					
40/J4/H0	POSIT	FIND	POSIT	CNIE	DST	WINT	Par	517	4140	120	4 I ND	PIS	11	WIND	OST	#INO	204	1 *	CFIW	151	d ( WI)
081#00Z	13.5 146.	4 15	0.0 0.0	0.	-0-	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	9.	-0-	
081806Z	13.9 166.	2 20	13.8 166.3	20.	9.	o.		164.A				14.5				30.	0.0	0.0		-0.	
0810127	14.5 145.	4 20	14.6 166.2	50.	35.	D.	16.0	164.4	30.	164.	10.	0.0	0.0	٠.	-0.	0.	0.0	0.0	ò.	-0.	0.
0816182	15.3 145.		14.4 165.4					163.7							-0.		0.0	0.0			0.
081900Z	16.1 144.		15.7 164.7					161.4			20.	0.0	0.0		-0.		4.0	0.0		-0-	
BB1906Z	17.1 163.	a 2n	17.0 163.8	20.	4.	0.	19.1	160.3	15.	120.	5.	0.0	6.0	0.	-0.	٥.	0.0	0.0	ó.	-0-	•.
0819122			17.9 163-1					n_n		-0.			0.0		-0.		4.0	0.0		-0-	0.
0819162	19.2 142.	0 15	15.4 162.2	20.	44.	5.	0.0	0.0		-0.		0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	0.
082000Z	20.0 140.	9 11	19.5 160-4							-0.			0.0				0.8	0.0		-0.	
2900580	21.0 159.		19.9 160-1		77.		0.0			-4.		0.0	0.0				0.0	0.0		-:-	0.

	AI'L	FIRECAS	15	
	WHM.	74-4R	44-44	72-48
AVG FORFCAST POSTT FRHOR	13.	157.	294.	٨.
AVE 41641 ANGLE EROOR	19.	43.	119.	0.
AVG INTENSITY MAGNITUDE FREDS	3.	12.	30.	n.
AVG INTENSITY ATAS	3.	12.	30.	0.
WINASO OF CONCLUSIO	-			

#### TROPICAL STORM KEN

	HFST	THACK			44KVI		1045		24 HI	) HIC F	DHELA: EHH			48 H	)ıs⊀ F:	18FC41			15 4	JUH F	nrf¢&4	¢ Ţ
40/04/H2	45517		۲٦5					200		eF1#			en:		al ND	DST		PD		#1 43	-61	4140
		9140					AIA)															
0840002	22.3 142.		0.0	0.0	0.	-0.	٥.	0.0	0,0	٥,		٠.	0.0	0.0	٠.	-0.	٩.	7.0	0.0	٥.		
0830062	22.5 141.		0.0	0.0	v.	-0.	٥.	0.0	n.a	٥.	-0.	٠.	0.0	0.0	0.	-0.	٠.	0.0	9.0	٠.	-0.	٠.
083015Z	22.4 140.		0.0	0.0	٠.	-0.	٥.	0.0	0.0	٥.		۰.	0.0	0.0	0.	-0.	٥.	0.0		0.		٠.
0839185	?3,3 17A.		0.0	0.0	υ.	-0.	0.	0.0	0.0	۰.	-U.	۸,	0,0	0.0	0.	-0.	۰.	0.0	0.0	٠.	-0.	٥.
DRITTED	23.7 1 17.	<b>A</b> 20	0.0	0.0	٥,	~0.	٥.	0.n	0.0	0.		٠.	0.0	0.0	o.	-0.	٥.		0.0	9.	-0.	0.
7001680	24.0 1 16.	6 en	0.0	0.0	٠.	-0.	٥.	0.0	0.0	٥.	-0.	n.	n.0	0.0	0.	-0.	٠.		0.0	٥.	٠٠.	٥.
0831155	24.4 1 15.	4 20	0.0	0.0	٠.		٥.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٠.	0.0	0.0		~O•	6.
0431185	24.6 174.	4 20	0.0	0.0	٠.	-0.	u.	0.0	0.0	٥.	• <b>U</b> •	n,	0.0	0.0	ű.	-0.	٥.	n.0	0.0	٥.	-0.	٥.
0901002	24.8 1 14.	1 25	23.4	132.5		105.	0.	27.4	124.5	35.	200.	٠.	79.H	150.5	35.	217.	-10.	37.6	129.5	30.	200.	
0901062	24.9 133.	5 25	55.5	132.0	25.	37.	0.	25.0	130.3	35.	64.	۸.	27.4	128.3	35.	100.	-25.	30.0	147.4	30.	485.	5.
0401157	25.1 133.	n 24	25.3	132.4		25.	0.	25.0	130.1	35.	80.	-5.	27.4	120.3	35.	265.	-2D.	30.7	127.6	30.	562.	5.
0941182	25.3 132.			131.4		43.	ů.	26.5	120,0	35.	111.	-5.	29.7	120.2	35.	276.	-10.	n.0	0.0	0.	-0.	0.
0902002	25.8 111.			131.7		19.	ō.		129.7		151.			127.6		450.		0.0	6.0	0.	-0.	0.
0902062	20.5 131.			131.0		42.	-5.		130.4	٠0.				130.4		343.		0.0	0.0	٥.		0.
090515Z	27.2 130.			130.0	45.	0.	5.		130.0	70.				133.5		205.	10.	0.0	0.0	0.		0.
0944187	27.8 130.			130.3	45		š.		130.5	50.		5.	0.0	0.0	ű.	-0.	ů.	0.0	0.0		-0.	8.
0903002	20.8 110.			130-7	40.	13.	-5.		131.0		173.	5.	0.0	0.0	ě.	-0.	ŏ.	0.0	0.0	0.		
0903062	30.0 170.			130.2								-										
					40,		-50.		132.4		137.	5.	0.0	0.0	۰.	-0.	٠.	0.0	0.0	٠.	-0.	••
7516960	31.3 131.			131.2	•0.		-15.	0.0	0.0	٥.		ŗ.	٥,٥	0.0	٥.	-0.	٠.	0.0	0.0	٥.		٠.
0903182	35.5 111.			135.0				0.0	0.0	0.		Α.	0,0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0+	
1904005	34.0 133.			133.0	30.		٥.	0.0	0.0	٥.	-0.	۰.	0.0	9.0	0.	-0.	٠.	0.0	0.0	٥.	-0-	٥.
0944062	15.2 134.		9.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-4.	٠.	0.0	0.0	0.	-0.	٥.	n.0	0.0	٥.	-0.	a -
094412%	36.5 136.	5 25	0.0	0.0	٥.	-0.	0.	0.0	0,0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٥.	n.0	.0	٠.	-0.	0.

	61 L	FIRECAS	15	
	WHMG	74-48	48-H3	72-4R
AVG FORFUASI POSIT FRADA	29.	116.	273.	415.
AVG RIGHT ANGLE ERROR	13.	60.	111.	105.
AVG INTENSITY MAGNITHOF ERRUR	5.	6.	14.	3.
AVE INTENSITY BIAS	-3.	-2.	-5.	٦.
NUMBER OF FORECASTS	13	10	7	3

## TYPHOON LOLA

	AFS	T THACK			dARVI		en as		24 H	nilk Fl	DHECA:			48 11	Dist Fr	AFC41			15 4	OUR F	AFC4	t <b>T</b>
40/24/H2	POSIT	#1 NO	ent	STT	dino	DST	HIND	Pne	117	<b>₩1</b>		CHIP	PNS	11	WIND		4IND	POS	11	#I 40	251	4140
0902007	21.3 141		0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	6.	-0.	0.	0.0		0.	-0-	0.
0902062	21.5 151		0.0	0.0	ű.	-0.	ě.	0.0	0.0	Ď.	-0.	n.	0.0	0.0	ŏ.	-0.	o.	0.0	0.0	Ď.	-0.	0.
9902122	21.8 151		21.4	151.2	3ú.	11.	ō.			95.		15.		150.5		200.			152.7			
0902187	22.1 151			150.7	30.	45.	ō.	25.2	140.8	45.	100.	in.	27.8	151.0		27).			174.2		447.	
090300Z	121 0.55		22.6	150.0	30.	62.	0.	23.9	147.9	.0.	61.		25.4	145.4		70.		26.5	142.0		246.	
0903067	22.8 150			150.5	30.	Zì.	ō.	23.2	144.6	45.	81.	- 5		147.3	50.		-25.		144.6		163.	
0903127	23.1 150	3 30	22.5	150.5	30.	37.	0.	73.7	144.4	Jō.	131.	•35.	24.4	147.3	40.	121.	+35.	25.6	144.6	45.	195.	-45.
0903182	23.4 149	7 35		150.2	30.	33.	-5.	24.5	144.9	35.	98.	*35.	25.8	146.8		45.		24.6	143.9		205.	
0904002	23.7 149	0 45	23.6	149.1	45.	9.	0.	25.2	144.4	60.	8.	-15.	26.7	144.0	70.	139.	-15.	24.4	141.7		245.	10.
0904067	24.0 148	.4 50	24.0	146.4	50.	0.	0.	25.4	144.0	65.	32.	-10.	27.7	143.6	70.	153.	-20.	29.0	141.9		271.	15.
0904127	24.4 147	A 65	24.3	147.7	55.	A.	υ.	26.0	145.2	75.	72.	n.	27.4	143.0	80.	177.	-10.	30.3	141.5	85.	794.	10.
9904182	24.7 147	.1 70	24.7	146.9	70.	11.	0.	26.R	144.2	75.	153.	-5.	24.4	142-1	40.	220.	0,	31.6	141.5	90.	324.	45.
3000000	25.3 146	.7 75	25.2	146-5	75.	12.	0.	27.3	144.0	85.	134.	n .	20.4	141.6	85.	218.	20.	37.1	142.0	85.	146.	45.
9995967	25.6 146	.4 75	25.8	146.0	75.	34.	U.	27.0	147.4	65,	13/.		30.2	141.9	85.	245.	25.	37.6	142.7	85.	745.	50.
0905155	20.3 146	.5 75	26.4	146.7	75.	12.	0.	29.7	146.5	HO.	47.	win.	72.7	150.0	65.	156.	10.		156.4	50.	255.	20:
0402185	26.8 146	. S MA	27.0	145.4	80.	13.	0.	29.9	147.2	75.	59.	-5.	37.7	151.0	60.	147.	15.	31.9	157.5	45.	251.	15.
0406007	27.4 146	. 5 45	27.3	146-5	60.	6.	-5.	29.A	147.4	75.	50•	ln.	17.7	150.9	60.	163.	20.	0.0	0.0		-0.	
090606Z	27.8 146	40	27.9	146.5	90.	9.	ø.	70.7	147.4	80.	64.	Sv.	32.5	151.7	60.	170.	25.	0.0	0.0	٠.	-0.	
0906127	28.5 146	. 7 90	28.5	146.4	40.	5.	٥.	31.1	148.0	75.	66.	50.	72.9	152.2	55.	IRO.	25.	0.0	0.0	٥.	-0-	٥.
0406182	29.3 146	7 6n	29.1	146.7	85.	n.	5.	71.R	144.3	05.	76.	50.	33.0	152.9	50.	216.	20.	n.0	0.0	0.	-0.	۹.
0907007	30.1 146	.4 55	30.7	146.7	65.	٩.	0.	4.55	148.8		119.	5.	33,5	154.1	40.	270.	10.	0.0	0.0	0.	-0.	0.
990706Z	30.0 146	60	30,¤	146-4	60.	10.	٥.	73.0	149.6	45,	130.	10.	0.0	0.0	٠.	-0.	٠.	0.0	0.0	0.	-0.	٠.
090/122	31.7 147	.0 55	31.7	147.2	>5.	10.	٥.	13.4	152.4	.0.	ist.	10.	0.0	0.0	٥.	-0.	Θ.	0.0	9.0	0.	-0.	٠.
0901185	33.0 147	.7 45	33.0	147.7	45.	0.	0.	0.0	0.0	٥.		٠.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٠.	-0.	0.
804007	34,4 146	40	34.?	148.4	40.	21.	٥.	0.0	0.0	0.	-0.	n .	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-f.	
0904065	35.1 150		0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-6.	٠.	4.0	0.0	0.	-0.	٥.	0.9	0.0	٠.	-0.	0.
040RISS	35.9 151	.A 30	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	п.	0.0	0.0	۰.	-0.	٥.	0.0	0.0	0.	-0.	٠.
09uB182	36.6 153		9.0	0.0	Θ.	-0.	٥.	0.0	0.0	٠.	-0.	۰.	0.0	9.0	۰.	-0.	٥.	0.6			-0.	••
300406	37.1 159	.1 30	0.0	0.0	٥.	~6.	٥.		0.0	٥.	-0.		0.0	0.0	0.	-0.	0.	٠.9	9.0	٠.	-0.	

	AI L	FORECAS	75	
	welma	24-4R	48-43	7>-49
AVG FONFCAST PARTY FRYAR	16.	AB.	172.	247.
AVG ALGAI ANGLE ERONA	10.	64.	149.	276.
AVG INIFASILY MAGNETUME ERRUR	1.	12.	20.	31.
AVE INTENSITY HTAS	-0.	-0.	-2.	1.
Milmard of FORFCASTE	22	21	10	1.4

#### TYPHOO: HAC

	REST TO	HAFK				enas		50 H	<b>''' F</b> (	MELAS ENH.			68 M	hi4 F-	FP41			15 43	UN FR	146 C 6 9	r I
40/JA/HG	POSIT #	1 vn	P3511	ul Na		w1 w)	Pag		⇔ I wo		4100	205		al vo		dina	209		CFIR	351	#T WU
	12.0 179.4	15	0.0 0.0	·	-0.	9.	0.0	```^	- 0,	-0.	۸.	0.0	``		-0.	0.	0.0		· 0.	-0-	0.
	12.0 138.8	15	0-0 0-0	ű.	-0.	ě.	0.0	0.0		-0.		0.0	0.0	ű.	-0.	ě.	0.0	0.0	ö.	-0.	0.
	11.0 137.0	15	0.0 0.0	ű.	-0.	ě:	0.0	0.0		-0.		0.6	0.0	ŭ.	-0.		4.0	0.0	· ::	-0.	0.
	11.0 137.3	15	0.0 0.0	ě:	-0.	ŏ:	0.7	0.0	ĭ:	-0.		0.0	8.8	ě.	-0.	0.	0.0	0.0	ö.	-0.	9.
	11.8 136.4	15	0.0 6.0	0.	-0.	ě:	0.0	0.0		-0.		0.0	0.0	٥.	-0.	0.	0.0	0.0		-0.	ë.
	11.8 135.7	15	0.0 0.0	ŏ.	-0.	i.	0.0	0.0	•:	-0.	0	0.0	0.0	ě.	-0.		0.0	0.0	0.	-0.	a.
	11.8 134.8	15	0.0 0.0	ŏ:	-0.	i:	0.0	0.0		-0.		0.6	0.0	ű.	-0.		0.0	0.6	ě.	-0.	ö.
	12.0 113.8	15	0.0 0.0	ŏ:	-0.	ŏ.	0.0	0.0		-0.		0.0	0.0		-0.	i:	0.0	0.0	Ď.	-0.	0.
	12.3 113.0	15	0.0 0.0	ŭ.	-0.	ŏ.	0.0	0.0		-0-		0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
	12.7 131.0	15	0.0 0.0	ű.	-0.	i.	0.0	0.0	i.	-0.	0.	0.0	0.0	ă.	-0.	ě.	n. 0	0.0		-0.	0.
	12.9 141.0	20	13.0 131.0	20.	5.	ŏ.	14.0	127.7	10.		• 30.	16.4			147			1/0.5		122.	0.
	13.2 130.0	30	13.3 130.1	50.	3.	-10.	15.1	124.4	30.		• 16.	17.0			210.			111.5	40.	239.	-5-
	13.5 129.0	• 11	13.5 129.2	25.	12.	-15.		124.9	30.		440.	17.4			232			116.7		347.	5.
	13.7 127.9	55	13.4 127.4	2U.	4.			123.4			-10-	14.4			792.			115.1		179.	30.
	13.7 127.3	50	14.1 126.0	>0.		-10.		122.7		184.	-4.	17.2			324.	10.		114.4		145.	30.
	13.7 126.7		14.3 125.4	25.		-10.		121.9		¿01.	0.	17.8			340.	15.		114.3		140.	10.
	13.7 126.2	7 n	14.5 124.R	25.		-15.	15.3	120.7	>5.	200.		15.5	117.4	эō.	240.	10.	15.5	113.3	60.	315.	26.
	13.7 125.7	74	14.0 124.8	25.		-15.	14.8	121.4	45.	130.	-4.	14.4	114.0		100.	20.			65.	249.	25.
0917122	13.8 125.2	45	13.4 125.2	75.	0.		14.4	127.4	>5.		٩.	14.4	120.0	15.	15.	0.	15.3	5.011	bā.	1 19.	>0.
0917182	13.8 124.5	55	13.9 124.7	55.	13.	0.	14.5	122.5	>0.	51.	٠.	15.0	120.3	35.		0.	15.5	117.6	60.	149.	10.
0914002	13.8 123.4	50	14.0 124.0	25.	13.	5.	14.7	121.3	40.	46.	۸.	15.4	119.6	>0.	56.	10.	14.4	115.5	60.	140.	30.
091 #06Z	13.6 123.3	50	14.0 123.0	<b>&gt;5</b> .	30.	5.	14.0	120.5	35.	30.	۸.	15.4	117.6	>v.	173.	10.	14.5	114.4	68.	2.9.	25.
0910127	13.6 172.7	50	13.2 122.7	>5	24.	5.	14.0	120.3	>5.	40.	20.	15.0	110.0	50.	157.	25.	14.4	115.5	bo.	217.	75.
0418185	13.7 122.1	45	13.7 122.0	>0.	5.	5.	14.7	119.4	>5.	78.	20.	15.1	117.5		173.	30.	14.7	115.2	65.	275.	25.
0919002	13.9 121.4	40	13.4 121.3	40.	9.	v.	14.4	119.0		104.	10.	14.3	116.7	75.	205.	25.	14.7	114.2	67.	259.	25.
7919165	14.3 170.4	34	13.4 120.5	40.	30.	5.	14.4	114.7	45.	153.	٩.	15.9	115.6	25.	227.	20.	17.8	113.6	65.	>>5.	30.
091415Z	14.8 120.2	35	14.4 119.0	35.	33.	0.	15.5	117.1		156.	٩.	14.4	114-6	45.	230.	5.	17.6	111.9	55.	297.	>n.
	15.5 119.8	35	14.6 119.1	35.	67.	v.	15.7	114.4	•0.	174.	10.	14.4		45.	380.	5.		189.4	bė.	371.	>0.
	16.1 119.1	40	16.0 118.7	35.	24.	-5.		114.5		103.	٩.	10.3	114+1		145.	٠.	10.1	111.6	43.	212.	٠.
	17.1 118.A	4.0	17.2 118.5	30.	14.	-10.		114.4			·le.	4.0	9.0		-0.		0.0	0.0		-0.	۵.
	17.6 118.4	34	17.5 118.5	JG.	13.	-5.	0.0	0.0	0.		n.	0.8	0.0		-0.	٠.	***	0.0	٠.	-0.	٠.
	17.9 118.3	30	19.3 118.0	30.	27.	٥.	0.0	0.4	٥.	-0.	۰.	n.a	0.0	٠.	-0.	٠.	A. 0	0.0	٠.	-0.	п,
	10.4 118.1	30	18.3   18.1	JO.	6.	0.		110.0	٧5.		-15.	A.U	0.0	٠.	-0.	٥.	n.0	0.0	٥.	-0.	٠.
	19.0 117.4	35	18.8 117.5	×0.	26.	-5.		115.5	25.	54.	-10-	0.0	0.0	0.	-0.	٥.	n	0.0	٥.	-0.	я.
	19.5 117.4	<b>4</b> n	19.2 117.1	30.	29.		0.0	0.0	٥.		٠.	^.0	0.0	0.	-0.	٥.	n.0	0.0	0.	-0.	٥.
	20.1 116.0	4.0	19.5 116.5	30.		-10.	0.0		٠.	-0.	۰.	n.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	0.
	20.5 116.4	• 0	20.5 116.5	30.	5.					41.	ele.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	٥.
	20.8 116.n	35	21.0 116.0	30.	15.	->.				64.	••••	0.0	0.0	••	-0.	٥.	0.0	0.0	0.	-0.	۰.
	20.9 115.4	35	21.3 115.7	30.	25.	-5.			35.	3/.	^.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.
	21.2 115.n	35	71.2 115.2	35.	11	Ů.		113.5	35.	14.	٠.	0.0	0.0	٠.	-0.	٥.	0.0	0.0	٥.	-0.	п.
	21.5 114.4	4.0	21.5 114.6	35.	11.	-5.		112.4		35.	٠.	0.0	0.0		-0.	٥.	0.0	0.0	٥.	-0.	۸.
	21.8 114.0	4.0	21.4 113.9	*5.	5.	5.	0.0	6.0	٠.	-0-	٠.	0.0	0.0		-0.	٥.	0.0	0.0	٥.	-0.	٠.
0923127	22.0 113.n	35	22.6 113.4	35.	44.	٥.	0.0	4.1	٠.	-4.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٠.	-0.	٥.
	22.3 113.5	30	22.3 113.4	30.	6.	٥.	0.0	8.0	o.	-0-	٠.	P.0	0.0	٠.	-0.	٠.	0.0	0.0	0. 0.	-0.	
0924002	?2.5 112.9	25	22.5 113.0	25.	6.	٥.	0.0		٥.	-4-	۰.	0.0	0.0	0.	-0.	٥.	0.0	0.0	v.	-0.	

	AI L	FIRECAS	TS	
	HMNG	24-49	48-41	72-49
AVG FORFLAST PORTT FRUNK	23.	93.	195.	279.
AVG 41G41 ANGLE ERDON	16.	66.	152.	221.
AVG INTENSITY MAGNITUDE ERROR	5.	12.	13.	21.
AVG INTENSITY BYAS	-4.	-5.	۹.	21.
WIMAER OF FRAFCASIE	14	22	1.0	13

## TROPICAL STORM NANCY

	HEST	TRACK			JARYI				24 40	nim F				48 M	Dij 4 F	JWF CA			15 4	) ) )	74FC 8	41
						F Ri	2511				ENN	J45				FRAT	45					
40/D4/H4	POSIT	₽I%n	POS	T T	JINO	OST	CPIN	Pn	111	# 1 WD	051	414-0	Pit	517	WIND	051	#IND	PO-	517	CFIP	051	# 1 W
091/122	16.0 113.4	0 20	0.0	0.0	0.		0.	0.0	0.0	0.	-0.	۸.	0.0	0.0		-0.	0.	0.0		٥.		
0917182	16.8 112.	2 20	0.0	0.0		-0-	Ŭ.	0.0	0,0	ě.	-0.	۸.	0.0	0.4	0.	-0.		0.0	1.0	0.		
	17.3 111.		0.0	0.0	ě.	-0.	ő.	0.0	0.0		-0.	٥.	0.0	0.0	v.	-0.		0.0	0.0			
	17.7 111.		0.0	0.0	٠.	-0.		0.0	9.0		-0.		0.0	0.4								
	10.1 111.		0.0		٠.		e.					-			0.		٠.		0.0	•		٠.
				0.0	υ.	-0.	0.	0.0	0.0		-0.	٠.	0.0	0.0		-0,	٠,	1.0	•.•	•		
	18.6 111.		0.0	0.0	Ģ.	-0.	٠.	0.0	0.0		-0-	٠.	۸.0	0.0	٥.		٥,	٠.0	0.0			
	16.0 111.		0.0	0.0	_0.	-0.	υ.	0.0	H.D		-0.	٠.	٥.0	0.0	Ű.	-0.	٥.	r.0		٠.	-0.	٠.
	18.6 11].:			111.7	30,	24.	-5.		117.4		201.	jn.	77.7	110.6	35.	304.	٠.	n. 8			-0.	٠.
	18.6 110.	y 34	19.		45.	13.	10.	19.7	IIn.A	45.	yu.	10.	70.1	108.7	⇒e.	179.	15.	20.6	145.8	35.	>>7.	15.
0414185	18.7 110.	3 45	19.3	110.4	>0.	36.	5.	78.1	100.7	45.	136.	10.	70.0	107.1	>U.	197.	20.	A.8	0.0		-0-	
0920007	18.7 109.	7 35	18.7	109.1	40.	23.	5.	18.5	104.4	30.	134.	٠٩.	18.2	104.3	25.	141.	-5.	0.0	0.0		-0-	
492406Z	18.4 109.	15	19.4			26.	5.		10A.H		132.	۸.	0.0	0.0	-		é.	0.0		0.		
	18.2 ln9.		15.4		15		ő.		104.0				0.0	0.0	•	-0.	0.	0.0	0.0			
	17.9 109.		19.3		35.		0.				120.		0.0	0.0	٥.			0.0				
	17.7 110.		17.5													-0.	n.		0.0	•••		٠.
					15.	36.	٠.		104.7			-10-	A.1	0.0	••	-•.	٠.	n.0		•.		٠.
	17.6 148.		17.4		15.	31.	٥.	0.0	_^,^	٠.		۰.	n. n	0.0			٥.	0.0		•	-0.	e,
	17.4 147.0		15.0		35.	36.	٥.			<b>45.</b>	30.	٠.	n. 0			-4.	٠.	0.0		٠.	-9.	
	17.3 117.	4 30	17.7	107.7	JU.	21.	٠.	0.0	0.0	•.	-4.	٠.	0.0			-0.	٠.	4.0	0.4		-0.	
0922002	17.2 117.	3 n	17.3	107.1	ć5.	11.	-5.		0.0	٠.		٠.	4.0	0.0		-0.	0.	0.0	0.0		-0.	
0922062	17.1 147.	0 30	17.3	106.5	25.	17.	-5.	0.0	0.0		-0.	٥.	0.0	0.0	٥.	- 0.	Ü.	0.0	0.0			
	16.9 146.		16.5		20.		6.	0.0	0.0		-0.	٠.	0.4	0.0		-0.	i.				-0.	

	A1 L	1 JAG C 9 2	13	
	mme G	24 <b>- 48</b>	48-44	7>-48
AVG FONECAST POSTT FRUNK	78.	116.	214.	2>1.
AVG 41GHI ANGLE EROOM	19.	96.	184.	210.
AVE INTENSITY MAGNITURE ERROR	3.	7.	10.	14.
AVG INTRASLIY HTAR	١.	1.	9.	14.
NUMBER OF FORECASTS	1 6			i

#### TYPHOON OWEN

	4FST	THACK		MARVI		24 +	INHE FURE		48 H	Out ForFCant	15	13UH FROFCEST
					FRRARS			SPCH		145		
40/Ja/HQ	POSIT	4140	PIST		DST WIND	PASIT	wind 9:		POSIT	ATAD USI ATM		#143 75T #140
005500S	12.6 138.4	50	13.0 138.0	₹0.	58. U.	13.4 13%.0	40. 12.	15.	14.4 131.8			5 70. 741. 0.
0455001	12,5 138.3	25	12.9 138.0	25.	25. 0.	13.4 134.9	45. 4	f. 15.	16.6 131.7	60. 274. 5	. 14.7 1/5.	5 7D. 127
0955155	12.1 137.7	25	12.5 137.3	25.	33. 0.	12.0 134.0	35. 14.	ie ne	17.4 130.9	45. 13715	. 17.5 175.	¿ 55. 34925.
0455185	12.1 137.2	25	12.3 136.7	25.	54. 0.	12.7 137.7	35. 220	. ·10.	17.6 129.1	50. 42410	. 15.3 1/6.0	0 60. 47940.
0923002	12.6 146.9	75	12.3 136.7	25.	21. V.	12.4 134.5	30. 220		17.7 131.2	35. 44735	. 11.2 1/5.0	45. 545. +55.
092306Z	13.3 136.6	3 n	12.3 136.1	30	65. D.	12.5 137.6	45. 31.	3. •1n.	12.4 130.3	55. 50520	. 13.3 127.	1 60. KJ150.
2515560	13.9 136.2	35	13.3 136.1	45.	35. 10.	13.0 134.1	50. 30	in.	14.7 131.4	bo. 44520	. 15.4 1/8.	70. 54640.
0923182	15.0 115.4		13.7 135.4			14.4 137.1	>5. 33.	45.	15.4 129.9	65. 47135	. 14.3 1/6.	75. 41610.
0924002	10.1 135.3		16.4 135.2		19. 0.	21.n 132.4			24.H 131.1	65. 14745		
0924067	17.7 134.3		17.9 134.5		13. 0.	22.1 131.			24.0 131.3	70. 14340		
0924122	19.0 133.2		19.2 133.4		16. 0.	24.0 130.0			27.4 130.2	85. 25025		
2010260	20.1 132.1		20.7 132.3		39. 0.	25.4 130.			24.7 130.5			
0925002	21.0 110.7		20.9 130.A		A. 0.	23.4 127.0			26.2 125.4	95. 2395		
092>062	21.3 130.3		21.7 130.0		29. 0.	24.1 127.1			24.2 125.8		. 20.3 1/7.	
8925122	22.0 129.R		21.9 129.4	8D.	23. 0.	24.7 127.0			27.1 126.5		30.7 1/8.	
0925182	22.6 129.5		22.5 129.0		2910.	24.0 127.4			27.5 127.0	750 161. 10		
0926002	23.1 129.1		23.3 129.2		1315.	25.5 128.1			27.H 130.0	90. 49. 5		
0459095	23.5 129.2		23.7 129.0			26.0 124.9			29.7 131.1	50. 10B. 5		
					1610.					55. At. 10		5 65. 24010.
0926127	23.8 129.3		24.0 129.1		1510.	26.0 124.1			24.4 130.6			
2819260	24.4 129.4		24.4 129.5		5. 0.	29.0 130.4			28.H 132.1	75. 135. 0		9 55. 31928.
2007560	24.9 129.4		24.R 129.4		12. 0.	26.4 124.6			29.4 131-7	70. 495		
0927062	25.5 129.7		25,3 129.7		12. 0.	27.7 130.4			29.2 132.7	65. 16210		1 43. 24720.
0951155	26.0 129.m		25.9   29.9		9. 0.	28.7 131.1			40.4 133.9	65. 21210		
0451185	26.5 179.R		26.5 129.7		9. 0.	29.0 130.6			11.5 133.7	bu. 14715		
0.658005	27.0 129.A		27.1 129.4		5. 0.	29.4 130.1			32.2 133.8	60. 14410		
0.054065	27.3 129.m		27.5   29.A		12. 0.	10.7 131.7			72.H 135.1	>>• 1∩3. <b>-</b> 10		
0254155	27.6 129.m	75	27.7 129.8	75.	6. 0.	29.5 130.0			12.1 132.0	50. 149. 5		
8959785	27.8 129.A	75	27.7 129.A	75.	6. 0.	28,5 124.5	70. W		31.2 131.2	60. 454. 15		7 00. 0.
0923005	28.1 179.9	75	28.0 129.A		9. U.	29.0 13n.e			12.4 132.5	60. 411. 25	. n.0 0.1	
0924062	28.5 110.1	74	28.7 129.4	15.	20. 0.	12.0 131.4	. 40. B	•• •25.	n.0 0.0	00. 0	. #.0 0.0	0 0 4.
7514560	29.1 130.3	75	29.1 130.2	75.	5. 0.	12.7 (31.4	1 55. 19	/. n.	n.# 0+0	U, -0. N	. 0.0 0.0	) 0g. n.
0454185	29.8 110.4	. 75	29.7 130.6	75.	6. 0.	12.0 132.	50. 33.		0.0	00. 0	. ".0 0.0	) Dn. n.
0930002	30.6 131.5	70	31.0 131.5		12. 0.	35.0 135.		15.	n_0 0.0	00. 0	. 0.0 0.0	00. 0.
0930062	32.4 133.1		32.0 132.5	70.	39. 5.	0.0 0.0			n_0 0.0	00. 0		
0430157	34.1 135.1		33.9 134.5		35. 12.	0.0 0.1			0.0 0.0	00. 0		
0430182	36.2 1 18.1		35.4 137.0		72. 5.	0.0 0.0		i n	0.0	00. 0		
100100/	39.8 141.9		39.0 141.3		55. 0.	0.0 0.0			0.0 0.0		. 0.0 0.1	
		, , ,	3.4. 1444		· · · · · ·		-•					• •• •••

		E 146 2 1 2	13	
	SMMG	24-4R	48-43	72-4R
AVG FORECAST POSTT FHHOR	25.	146.	250.	321.
AVG 41G41 AVGLF ERONH	15.	78.	159.	254.
AVE INTENSITY MAGNITHUF ERRUS	₹.	10.	15.	14.
AVG INTENSITY HEAS	-0.	- 3.	-4.	-14.
NUMBER OF FORECASTS	32	33	29	23

#### TROPICAL STORM PAMELA

	AFST	TOACH			#4H-1	<b>V</b> G			24 4	nile Fi	OHE LA	s f		48 40	).14 F	W# C 4	<b>\</b> T		#2 A)	UH **	.05061	41
						: Q1	<b>₽</b> 145				ENK	J45				254	<b>2</b>					
40/JA/HD	P3517	4140	P 75	11	w I N n	DST	#140	Pat	5 † T	A 1 AV	150	@ [ sup	#n\$1	1	HIND	751	#IND	POC	11	CFIB	251	m ( Mt)
0923007	18.0 150.	n }4	0.0	0.0	υ.	-0.	0.	0.0	0.11	0.	-0.	۰.	3.0	0.0	٥.	-0.	0.	7.0	0.0	Ú.	-0.	н.
1923067	18.2 148.	9 15	0.0	0.4	0.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	u.	-0.	ρ.	0.0	0.0	0.	٠٠.	в.
0923127	18.3 147.	4 15	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	۰.	A. A	9.0	ű.	-0.	٥.	0.0	0.0	0.	-P.	0.
0923182	18.5 146.	5 15	0.0	0.0	o.	-0-	0.	9.0	A. "	0.	-0.	۸,	0.0	0.0	0.	-0.	n.	0.0	0.0	в.	-0-	ð.
092+007	10.0 145.		0.0	0.0	0	-0.	0.	0.0	0.4	0	-0.	٠.	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	n.
8924862	18.7 145.	n 15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.		n.	0.0	0.0	٠.	-0.	0.	0.0	0.0	0.	-0.	0.
151+540	18.8 144.		0.0	0.0				0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	- J .	0.	4.0	0 . (1	0.	-0-	n.
0920182	19.0 144.		0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-4.	n .	0.0	0.0	0.	- 3.	0.	0.0	9.0	0.	٠٠.	в.
0925007	19.2 143.		9.0	8.0		-0.	o.	0.0		Ď.	-u.	۸,	A . 0	0.0	0.	-0.	0	n.0	0.0	٥.	-0.	٥.
0925067	19.0 103.		0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	6.0	0.	-0.	0.	0.0	0.0	0.	-0-	n.
1216760	19./ 142.			142.0		13.			130.0			. 26.	0.0	0.0	v.	- J -	0.	0.0	0.0	0.	-0-	٥.
0925182	20.1 1a0.			141.1		34.			130.1		10%		0.0	0.0	0.	-0.	0.	n . B	0.0	0.	-0-	٠.
0426407	20.5 139.			134.0				0.0					0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
4920467	22.0 137.			137.0		25.		0.0					0.0	0.0	ŭ.	-0.	Ö.	0.0	J. 0	ä.	-0.	٥.
0420127	20-1 117-			136.5			>.	0.0	0.0		-0.	٠.	n.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
0926187	26.0 176.			136.8		0.	5.	0.0	0.0		-0.	٠.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	.0.	n.

	A L	FRAFCAS	75	
	WMG.	24-40	48-44	77-48
AVG FORELAST PARTT FHYAM	2A.	154.	٠.	ο,
AVU 41GHT ANGLE FROM	22.	15.	٦.	Α.
AVG INTENSITY MAGNITURE FRAUE	3.	25.	٦.	n,
AVG INTENSITY HEAS	1.	n.	٠.	n ,
NUMBER OF FORECASTS		,	ō	ń

#### TROPICAL STORM ROGER

	4151	THACK		-444				24 4	NIM F				48 H	0114 F				72 4	JUR FE	THE CA	<b>5</b> 1
					F 01	4.745				Enn					FAST						
40/J4/HD	PJS11	# NO	₩351 T	-IN1	051	41 47	PAS	11	# L Wn	051	4 [ 44]	B(15	5 I T	- L ND	751	#IND	404	111	4 [ 40	251	# 1 WD
100200/	11.7 142.	7 /0	0.0	.n 0.	-0.	U.	0.0	0.4	0.	-0.	и.	0.0	0.0	U.	-0.	٥.	n.0	0.0		-0.	
100206/	12.0 142.	1 70	0.0	0.		0.	0.0	0.0	0.	+0.	۰.	0.0	0.0	٥.	-0.	0.		0.0		-0-	
1005152	12.4 141.	4 20	0.0	. 0.		ů.	0.0	0.0	ō.		0.	0.0	0.0	ő.	-0.		0.0	0.0		-0.	i.
	13.2 140.		0.0	.n u.		o.	0.0	0.0			4	6,0	0.0			ě.		4.6			
	14.2 140.			.n U.		ű.	0.0	0.0			ο.	0.0	0.0		-0.		0.0	0.0			
	16.1 119.		15.7 139		21.			137.1		201.			130.0					115.0		150.	
1003127	18.0 118.		15.5 134		85.		20.2					21.5			179.			1 67.4			10.
	19.4 137.		19.5 (3)		23.		24.8					29.0			347			142.2			-5.
	20.0 136.		21.0 136		24.		26.0				•10.		134.3			-20.		148.6			-76.
	21.2 175.		21.7 135		30.		26.4			374.		31,5				-15.	0.0	0.0			0.
	21.5 114.		21.5 130		17.		23.7			199.			133.0		123.		0.0	8.0	•:		
	21.0 133.						25.4						134.5		44.		n.0	0.0	•••		
	14.4 14.		20.2 13				>3.4						137.8		INO.		0.0	0.0			
	20.3 135.		20.2 130				>3.4				٩.		137.9		324.		0.0	0.0	•••		
	21.5 135.		51.4 135								۸.	0.0	0.0				0.0	0.0			•.
	22.8 1 15.	3 65					26.7	34,0		172.	٠.	٥.0	0.0	٥.	-0,	ο,	0.8	0.0	٠.	-0.	в.
1005002	23.8 114.	7 45	23.9 134	.7 40.	4.	-5.	29.0	134.4	35,	135.	٠.	0.0	0.0	ú.	-0.	٥.	0.0	0.0	0.	-0.	٠.
1000001	25.2 134.	4 45	25.1 134	.7 40.	17.	-5.	11.5	137.9	35.	205.	٩.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	•.
1000152	26.8 135.	3 45	26.4 135	. 3 40	24.	-5.	0.0	0.0	0.	-0.	۸.	0.0	0.0	o.	-0.	0.	0.0	0.0	0.	-0.	٠.
	29.1 116.		29.4 130				0.0	8.0	0.	-0.		n_n	0.0	0.	-0.	0.	0.0	0.0	0.		
100/002	32.0 117.	4 35	31.9 13		16.		0.0	0.0			٠.	0.4	0.0				0.0	0.0	0.		
1007062	30.4 140.			. 0		ŏ.		0.0		-0.	0.	0.4	0.0			ě.	0.0	0.0	o.		

	AI L	FORECAS		
	WHNG	74 - 4R	48-43	79-48
AVG FUNFLAST POSTT FRHOR	12.	195.	251.	3n3.
AVG 416-1 ANGLE ERUNH	19.	93.	109.	174.
AVG INTENSITY MAGNITHUS FRRDR	3.	5.	7.	11.
AVG INTENSITY HTAS	-3.	0.	-1.	-1.
MIMARN OF FORFCASIC	14	1.3		

## TYPHOON SARAII

	HEST THEM		4441	46 5880.45	24 4	n-IH FL				48 #6	)114 F			F2 HOUR FORECAST				
404 144 1	D31.17	105.7	. Laus		POSTT	-INO	ENH.		204			FRA 1.						
40/74/44	10.6 119.0 lb	47517 0.0 0.0	4107	DST WIND	0.0 0.0		-0-	o. €[mi]	P05	0.0	d I NU	751	41MI	n.0		div)		al ( Mr.)
0930187	14.6 139.4 15	0.0 0.0	Ů.	-n. 0. -o. 0.	0.0 11.0		-0.	η.	0.0	0.0	0.	-0.	0.	0.0	0.0	ŏ.	-0.	0.
1001007	14.5 119.8 15	0.0 0.0	v.	-0. 0.	0.0 0.0		-0.	Α.	0.0	0.0	0.	-0.	0.	0.0	0.0	ő.	-0.	a.
1001062	14.5 120.2 15	U.O 0.O	ö.	-0. 0.	0.0 0.0		-0.	n.	0.0	0.0	0.	-0.	0.	n.0	0.0	ő.	-0.	0.
1001122	14.5 120.4 15	0.0 0.0	ŭ.	-0. 0.	0.0 11.0		-0.	٥.	0.9	0.0	ů.	-0.	٥.	0.0	0.0	Ö.	-0.	a.
1001187	14.5 120.H 15	0.0 0.0	Ü.	-0. U.	0.0 0.0		-0.	n.	0.0	0.0	0.	-0.	õ.	0.0	0.0	ŭ.	-0.	0.
1002002	14.7 121.0 15	0.0 0.0	ō.	-0. 0.	0.0 0.0		-0.	0.	0.0	0.0	v.	-0.	ŏ.	0.0	0.0	Ď.	-0.	0.
1002067	14.8 121.1 15	0.0 0.0	u.	-0. 0.	0.0 0.0		-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	o.	-0-	n.
1005155	14.9 121.2 15	0.0 0.0	0.	-0. 0.	0.0 0.0	0.	-0-	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	۰.	-0.	0.
1005185	15.2 121.2 15	0.0 0.0	u.	-0. 0.	0.0 0.0	٥.	-0.	ο.	0.0	0.0	٥.	~0.	0.	0.0	0.0	٥.	-0.	0.
1003005	15.2 170.4 14	0.0 0.0	G.	-0. 0.	0.0 0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
1003067	15.0 170.4 15	0.0 0.0	٥.	-0. 0.	0.0 0.0		-0.	٠.	0.0	0.0	v.	-0.	٥.	n.0	0.0	٥.	-0.	п.
1003155	14.8 120.7 15	0.0 0.0	0.	+0. 0.	0.0 0.0		-0.	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
1003182	14.6 120.n 20	0.0 0.0	٥.	-0. 0.	0.0 0.0		-0.	n •	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	9.
100+002	14.4 119.7 20	0.0 0.0	0.	-0. 0.	0.0 0.0		-0.	^•	0.0	0.0	0.	-0.	٥.	0.0	0.0	o.	-0.	n.
1004062	14.2 119.5 30	14.0 119.7	. O.	-0. 0. 37. V.	13.4 119.7		-v.	n.	13.0	0.0	۷. 45.	-0. 555.	0.	0.0	0.0	40.	-0.	
1004182	13.5 118.A 35	13.9 119.7	35.	39. 0.	13.5 117.7		151.	10.	12.4			220.	8.		113.0		365.	
100-007	13.0 118.4 40	13.7 118.9	•0.	42. 0.	13.2 114.9		160.	in.	12.7			742.			111.6		436.	
1000062	12.7 119.0 40	12.5 118.5	+0.	31. 0.	12.5 114.5		70.	٠.	11.5		40.		-35.		117.0		130.	
1009155	12.5 119.3 40	12.5 119.3	.0.	0. 0.	12.0 114.9		45.	-5.	11.1		40.		-35.		116.4		159.	
1002187	12.5 119.5 40	12.1 119.0	+u.	34. 0.	11.0 11H.4			-10.	10.4	117.3		176.			116.3		141.	
1006002	12.5 119.7 40	12.3 119.n	*U.	43. 0.	12.1 114.7	40.	41-	•Sr.	11.5	110.0	is.		-40.		117.0	30.		-55.
1006062	12.4 119.7 40	12.4 119.9	.0.	12. 0.	12.4 12n.8	33.	40.	<b>4</b> 0.	12.3			160.		12.4	142.4	25.	277.	-65.
1009155	12.3 119.4 45	10051 4.51	35,	3010.	12.4 120.4		100-		12.7			179.		0.0	0.0	٥.	-0.	0.
1005182	12.2 119.5 Sn	15.4 119.8	35.	2115.	12.4 l2n.3			445.	12.5			157.		0.0	0.0	٥.	-0-	0.
1007002	12.2 119.4 50	12.2 119.4	*5.	n15.	12.2 119.4			40.	0.0	0.0	٠0٠	-0.	0.	0.0	0.0	٠.	-0.	0.
1007062	12.1 119.2 75	12.2 119.2	65.	510.	11.9 11H.4			-14.	11.5		50.		-40.		114.3	+0.	118.	
100712Z 100718Z	11.4 119.2 75	12.1 119.2	65. 65.	1210. 2510.				4]5.	11.6		>0.		-40. -45.		114.5	+0.		-60.
1008005	11.3 119.2 75	12.0 119.1	65.	510.	11.2 114.2			<b>43</b> 0.	11.1		÷0.		-60.		116.5	40.		-68.
1000002	11.0 119.2 75	11.1 119.2	65.	610.	10.4 118.0			-3n.	10.7		35.		•55.		115.2	50.		-40-
1009155	10.8 119.1 75	10.9 119.1	65.	0, -10,	10.1 119.0			•3n.	10.1		55.		-45.		116.9		119.	
1008187	11.0 118.4 /5	10.4 119.1	65.	3010.	10.2 114.2			#3n.	10.0		25.	117.			115.0		129.	
100+007	11-1 118.4 45	10.6 11H-2	55.	3220.	10.4 114.2	70.	72.	#4n.	10.4	114.3	65.		- 35.	11.6	112.3	65.	127.	-10.
100 + 062	11.3 117.8 Wn	11.3 117.8	90.	0. 0.	11.4 114.4	H5.	21.	425.	11.6	115.4	eu.	75.	-10.	11.8	114.2	80.	70.	10.
1003155	11.3 117.4 90	11.5 117.4	9v.	12. 0,	11.0 115.0			414.	17.7		80.	29.	-5.		112.7	80.	79.	15.
100-182	11.4 117.1 95	11.7 116.9		215.	15.3 174.0			ale.	17.4		60.	92.	5.		111.0		111.	15+
1010002	11.5 116.7 110	11.4 116.3		2420.	11.4 117.5		10++		11.5			176.	5.		1#8.9		241.	50•
1010067	11.6 116.7 110	11.5 116.4		610.	11.0 114.4		37.	10.	12.0		90.	93.	20.		110.4		126.	30.
1010122	11.7 116.n 10n	11.5 115.0		B. 0.	11.0 114.0		52.	15.	12.0		90.	100.	25.		110.0		176.	50.
1010182	11.8 115.4 190	11.9 115.3	90.	30. 0. 910.	12.5 114.4		48. 25.	25.	17.5		90. 70.	A1. 25.	25. 10.		149.6	60.	100.	15.
1011062	12.1 115.1 40	12.0 114.9		13. 0.	12.4 113.0		55.	5	12.6		70.	45.	io.		108.9	60.	76.	10.
1011152	12.2 114.8 HS	12.1 114.3	÷0.	30. 5.	12.3 111.4		95.	10.	17.4			176.	6.		107.7	20.	123.	- 30.
1011187	12.4 114.5 75	12.5 113.0	85.	36. 10.	13.0 111.3		94.	۸.	13.2			105.	790.	0.0	0.0	Ö.	-0.	0.
1012002	12.8 114.1 75	12.4 114.2	40.	25. 5.	12.5 112.5		48.	٠.	12.9	111.0	50.	79.	-5,	13.2	109.3	40.	35.	20.
1015065	12.9 113.8 7n	13.0 113.4	80.	13, 10,	13.5 112.1	65.	6.	۶.	17.4	110-5	50.	42.	0.	0.0	0.0	0.	-0.	0.
1015152	13.1 113.7 65	13.3 113.2	dO.	13. 15.	14.0 111.5		34.	٩.	14.6		65.	80.	15.	0.0	0.0	0.	-0-	0.
1015185	13.2 112.0 65	13.5 112.5	15.	29. 10.	14.4 130.3		76.	۶.	14.7		30.	101.	-5.	0.0	0.0	0.	-0-	0.
1013002	13.3 112.4 An	13.3 112.1	15.	29. 15.	13.2 110.2		50.	٠.	13.1		30.	29.	10.	0.0	0.0	0.	-0-	0.
1013062	13.4 112.1 60	13.2 112.0	75.	13. 15.	13.1 [10.]		13.	5.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	0.
1013122	13.4 111.7 60	13.5 111.5	70.	13. 10.	13.8 100.5		30.	٠.	٥.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0-	٥.
101318Z 101400Z	13.4 111.1 60	18.5 111.0	50. 25.	305. 0.	13.4 100.4		21.	٠	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0. 0.
1014002	13.4 110.4 55	13.5 110.9	>0.	19. 0.	0.0 0.0		-4.	10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1010122	13.3 119.6 50	13.7 104.4	20.	0. 0.	0.n n.n		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0-	0.
1014187	13.2 119.1 35	13.3 109.0	35.	4. 0.	0.0 0.0		-0-	0.	0.0	0.0	ö.	-0.	ŏ.	0.0	0.0	ö.	-0-	0.
1012002	13.1 1n8.7 2n	13.1 10H-5		12. 0.	0.0 0.0		-0.	n.	0.0	0.0	ø.	-0.	ō.	0.0	0.0	0.	-0-	n.

	AI L	FRECAS	15					
	AHNG	24 <b>- 네</b> 큐	48-H3	77-44				
AVG FORECAST POSTT FRUNK	26.	61.	112.	143.				
AVG 41GHT ANGLE EROOM	16.	40.	85.	107.				
AVG INTENSITY MAGNITUDE ERROR	6.	16.	47.	77.				
AVG INTENSITY RTAS	-5.	-9.	5.	-21.				
NUMBER OF FORECASTS	4.3	39	34	27				

#### SUPER TYPHOON TIP

	HEST THACK	. ⊿ARVING ≠RRORS	24 Hn	TCADENT HILL	48 HOHR FOMFCAST 643035	15 4308 EUMECREE
MO/JA/HD	POSIT WIND	POSIT WINT DET WINT	POSIT	WIND DOT 41ME		UNID 12, CHIR 11204
1004002	6.3 154.1 2n	0.0 0.0 00. 0.	0.n n.n	0U. n.		0.0 0.0 00. 0.
1004062	6.3 153.0 25	0.0 0.n 00. 0.	0.0 0.0	0u. n.		0.0 0.0 00. 0.
1004122	5.7 153.7 25	0.0 0.0 00. 0.	0.0 0.0	0v. n.		".0 0.0 0u. n.
1004182	5.4 153.9 25	0.0 0.0 00. 0.	0.0 0.0	00. 0.		n.0 0.0 0n. n.
1005007	5.4 154.5 25	5.4 154.5 25. 0. 0.	6.4 157.4	JO. 685.		4.3 147.1 45. >37. 5.
1005062	5.7 195.2 25	5.9 155.2 25. 6. 0.	7.4 157.7	30. 405.		10.4 145.0 45. 219. 5.
1005122	6.5 154.4 30	6.1 155.7 25. 485.	7.0 154.7	35, 48. n.		10.5 led.0 >0. 148. 4.
1005187	7.1 153.4 30	6.6 155.2 25. 995.	8.1 (57.4	35. 274.		10.5 147.0 50. 150. 0.
1006002	7.3 153.3 35	7.3 153.1 35. 12. 0.	8.7 150.2	45, 138. 4.		11.0 145.1 65. 173. 15.
100606Z 100612Z	7.5 153.1 35	7.7 152.4 35. 43. 0. 7.7 152.5 35. 24. 0.	8.9 144.6 9.1 150.0	45, 201. S.		11.8 144.4 65. 117. 10.
1006182	7.4 152.4 40	7.7 152.5 35. 24. 0. 8.1 151.9 40. 43. 0.	9.4 144.4	45. 18/. S. 50. 22J. 1n.		11.8 144.9 65. 49. 5. 12.0 144.4 70. 795.
100/002	7.7 152.3 40	8.0 152.7 40. 14. 0.	9.3 150.5	50. 124. 10.		12.0 143.0 70. 15010.
1007062	7.0 152.4 40	7.3 152.5 40. 19. 0.	8.7 151.5	45, 13, 5,		11.5 146.5 70. 31015.
1007122	6.6 151.9 40	6.9 151.7 40. 21. 0.	8.2 149.6	45. 11c. n.		11.4 144.5 70. 24120.
1007182	6.8 152.1 4n	6.7 151.5 40. 35. 0.	7.6 149.3	50. 207. n.		11.0 144.4 75. 24540.
100900Z	7.8 151.0 40	6.9 152.1 40. 61. 0.	7.7 151.3	65, 339. 15.	0.0 149.3 75. 4685.	10.5 145.4 75. 45955.
1008067	8.9 151.4 40	8.6 151.5 45. 19. 5.	13.4 147.2	60. llj. 5.		14.6 148.0 75. 14945.
1008155	9.8 150.4 45	9.7 150.3 45. 19. 0.	15.5 144.0	60, 105. n.		16.8 147.5 75. 14165.
	11.0 149.5 50	10.7 169.5 50. 18. 0.	13.4 145.4	05. 120. *In.		17.7 146.9 75. 14975.
	12.2 147.8 50	12.3 147.9 50. 6. 0.	16.0 141.9	05. 177. 415.		21.5 132.9 85. 43975.
	12.7 145.R 55	13.0 146.0 55. 21. 0.	15.n 142.4	65. 104. 42n.		21.6   11.2 B3. 445. +R0.
	12.8 144.7 50	12.9 144.7 60. 0. 0. 12.4 143.7 65. 1310.	13.2 134.5	65. 141. 425. 75. 113. 440.		15.2 1/3.6 85. 44890.
	13.1 142.5 An	13.0 142.4 80. 8. 0.		100. 74. 43n.		14.0 1/8.2 90. 51145.
	13.5 141.7 45	13.1 141.4 85. 25. 0.		105. 12/. •35.		15.8 1/8.6 130. 411. 0.
	13.7 141.1 90	13.7 140.9 95. 12. 5.		110. 80. 430.		16.2 141.3 130. 231. 5.
	13.9 140.3 115	14.3 140.0 100. 3015.		115. 11035.		17.1 129.0 130. 332. 5.
	14.2 139.5 130	14.3 139.4 100. 830.		145. 132. *15.		17.4 128.9 160. 20F. 35.
	14.5 139.4 140	14.4 139.7 130. 1310.		150. 12115.		17.0 140.0 160. 200. 15.
101112Z	15.1 139.2 [40	14.7 139.2 135. 125.	16.1 137.4	150. 53. *15.		14.8 144.7 160. 154. 15.
	15.7 138.4 150	15.8   38.9   135. 515.	17.2 134.4		. 18.H 134.8 155. 119. 30.	20.3 143.6 260. 191. 35.
	16.3 138.3 16n	16,4 138.7 135. 6, +25.	18.4 134.1			22.1 143.4 130. 277. 5.
	16.8 137.7 165	16.9 137.6 145. 820.	19.4 134.4			24.9 144.R 130. 563. 5.
	16.9 137.2 165	17.1 137.2 155. 1210.	18.0 134.8			24.0 133.0 130. 368. 5.
	16.8 176.9 155	17.3 136.7 155. 32. 0.	18.7 135.0			23.0 142.8 120. 306. 0.
	16.7 136.2 145	16.5 136.4 140. 175. 16.1 136.4 140. 54. 10.	16.9 137.5			20.9 144.9 110. 33710.
	16.7 135.7 125	16.1 136.4 140. 54. 10. 16.7 135.7 135. 0. 10.	16.0 (37.0			20.9 144.9 110. 341. 0. 14.0 127.1 110. 172. 0.
	16.8 134.9 125	16.7 134.9 130. A, 5.	17.1 132.2			19.0 1/6.6 110. 149. 5.
	17.0 134.0 125	16.9 134.2 120. 175.	17.7 131.7			19.1 146.2 100. 179. 0.
	17.1 133.5 125	17.2 133.7 120. 135.	18.0 130.6			20.5 126.3 80. 23015.
	17.3 132.5 125	17.1 132.4 120. 135.	17.5 129.0		10.4 125.5 100. 21510.	19.5 1/2.0 90. 3455.
1014182	17.6 131.9 125	17.5 131.5 120. 195.	18.3 124.1	100. 87. *2n.		21.0 1/1.0 90. 406. 0.
	18.1 130.9 125	18.0 131.0 120. 4, -5.	19.7 [ZA. 7			22.0 143.0 100. 321. 10.
	18.4 130.4 125	18,5 130 · n 115, 23, -10,	50.4 ISK.A			24.0 1/3.0 95. 777. 10.
	18.6 129.4 125	18.7 129.4 115. 410.	20.0 127.2			23.5 123.0 95. 641. 20.
	18.9 129.5 120	19.0 129.0 110. 2910.	20.7 124.5			20.3 1/3.0 90. 540. 15.
	19.4 129.1 12n 19.9 128.9 11n	19.5 129.4 110. 1410. 19.6 129.7 110. 37. 0.	21.4 127.4 21.0 128.5			25.4 125.7 90. 638. 20. 25.4 126.4 90. 807. 30.
	20.5 128.4 110	20.6 128.7 105. 85.	22.8 127.8	45. 12. n.		24.1 1/8.4 80.1145. 30.
	20.8 128.4 105	21.1 128-5 100. 195.	23.3 127.4	90. 43. n.		28.6 128.7 HU-1197. 10.
	21.5 128.1 100	21.5 128.2 95. 65.	23.0 127.2	90. 84. n.		n.0 0.0 0n. n.
1017062	22.4 127.9 95	22.0 127.A 95. 25. D.	24.6 127.0	M5. 143. n.		0.0 0.0 D0. 0.
1017122	23.0 127.9 45	23.2 127.7 90. 135.	26.0 127.4	15. 201. n.		n.0 0.0 00. n.
1017182	24.0 127.4 40	23.8 127.6 40. 12. U.	26.8 127.4	75. 284. n.		0.0 0.0 D0. N.
	25.1 127.4 90	25.1 127.A 85. A5.	29.2 129.4	70. 330. n.	0.0 00. 0.	n.0 0.0 0D. n.
	26.5 128.4 45	26.4 12R.4 BU. 125.	11.7 131.4	55. 4314.		0.0 0.0 00. O.
1018152	28.4 130.1 75	28.1 130.0 75. 19. 0.	14.4 137.4	50. 534. n.		0.0 0.0 00. 0.
	30.3 131.4 75	29.9 131.7 75. 24. 0.	16.9 141.4	50. 455. n.		0.0 0.0 00. 0.
	33.0 134.3 70	32.9 134.0 7u. 16. 0.	0.0 0.0	0u. n.		#•0 0.9 0• =0• P•
101906Z 101912Z	36.2 138.4 6n	35.4 138.7 60. 50. 0. 41.0 144.2 60. 54. 10.	0.0 0.0	00- 0.		0.0 0.0 0
	43.1 146.1 5n	42.8 151.0 55. 215. 5.	0.0 0.0	0u. n.		0.0 0.0 00. 0.

	ā: L	FARECAS	TS	
	⊭HNG	24-49	48-43	7>-4R
AVG FORFCAST POSTT FRHOR	24.	135.	257.	345.
AVG RIGHT ANGLE ERROR	15.	69.	142.	214.
AVG INTENSITY MAGNITUDE ERRUR	5.	10.	17.	22.
AVG INTENSITY HIAS	-3.	-6.	-5.	-7.
Manager of Francisco.		41	2	

#### SUPER TYPHOON VERA

	HEST THACK	# AR U 1 VG	24 HOUR FURELAST	AH HOW FORFCAST	12 HOUR FORECAST				
		FAR-145	EKHJ4S	FRINIS					
TH/BE/CH	POSIT WIND	POSTE AINT DAT WINT	Buell altu nel almi	UNID TER GRIN TIERO	UMIN 120 CHIN 112CH				
1102007	1.0 145.A 25	6.5 145.6 20. 325.	7.n 142.5 30. 112. #35.	7.6 139.4 40. 41595.	H.3 136.4 50. 47045.				
110206/	7.4 144.7 55	7.3 145.4 20. 545.	8.7 147.2 70. 24d. n.	9.7 140.1 80. 54160.	10.9 147.0 85. 72250.				
1106151	7.2 143.5 50	7.6 144.4 55. 815.	8.7 141.H 75. 274. 42n.	a.4 138.4 85. 578. <b>-</b> 55.	11.2 145.9 95. 71220.				
1105101	7.6 142.7 90	7.3 143.4 25. 955.	7.8 140.7 75. Joo. 455.	P. 7 137.6 35. 61950.	9.1 1.4.4 Yō. 7>2. N.				
1103007	8.0 140.9 hs	7.3 141.4 35. 6410.	8.4 13A.1 75. 222. 46n.	in.2 130.3 85. 29850.	12.6 1/4.4 95. 212. 0.				
1103062	8.6 119.n 7n	9.3 139.0 55. 145.	11.2 131.7 /5. 41. 465.	13.2 125.5 /5. 57. +60.	17.6 1/2.3 75. 78. +15.				
1103157	9.2 117.1 45	9.2 137.0 /U. 625.	11.7 124.4 45. 30. 454.	14.7 124.5 80. 3335.	14.7 122.6 73. 1n45.				
7816011	10.0 145.1 130	9.4 135.2 05. 1345.	12.5 128.5 110. 55. 425.	15.7 123.9 100. 54. 5.	19.8 1/2.4 80. 137. 35.				
1104007	10.5 143.0 135	10.5 133.5 125. 2910.	12.4 127.5 130. 955.	15.3 123.9 120. 70. 25.	19.0 1/2.2 110. 01. 70.				
1104062	11.1 131.0 140	10.9 131.4 125. 2515.	13.0 124.4 130. 245.	15.1 122.7 120. 44. 30.	17.8 1/2.1 110. 112. 75.				
110412/	11.6 129.2 140	11.4 129.1 130. 1310.	14.4 121.5 100. 151. 415.	19.1 121.1 50. 14020.	21.0 148.0 50. 670. 20.				
1104167	12.0 127.7 145	12.4 127.1 130. 425.	15.7 120.7 100. 170. 4.	19.4 121.8 60. 120. 15.	n.0 0.0 U0. 0.				
1105002	12.7 125.0 135	12.7 125.4 125. 510.	16.0 120.3 85. 141. 410.	19.3 121.3 50. 90. 20.	n.0 0.0 U0. 0.				
110006/	13.4 124.0 135	13.6 124.7 120. 1715.	16.3 120.4 80. 109. 410.	19.6 122.3 60. 142. 25.	n.0 0.0 00. n.				
1100122	14.3 124.1 115	14.2 124.1 120. 6. 5.	17.5 122.5 100. 34. 20.	20.7 126.0 70. 509. 40.	n.o 0.0 00. n.				
1100182	14.8 123.5 45	15.0 123.1 120. 25. 25.	18.4 127.4 100. il4. 54.	n.n 0.0 00. 0.	n.0 0.0 Un. n.				
1105002	15.5 122.7 45	15.3 122.4 45. 13. 0.	18.7 122.2 60. 76. 20.	n.0 0.0 00. 0.	n.0 0.0 00. H.				
1106067	16.3 122.3 Qn	16.4 122.5 90. 13. U.	19.0 123.4 /0. 202. 35.	0.0 0.0 00. 0.	n.0 0.0 0p. 0.				
1100122	17.0 122.2 40	17.1 122.7 40. 5. 10.	20.3 127.4 FO. 340. 4n.	n.n 0.0 vv. 0.	n.0 0.0 00. B.				
1106182	17.6 121.7 45	17.0 121.0 85. 15. 60.	0.n n.n 0y. n.	n.e 0.0 u0. 0.	n.0 0.0 00. 0.				
1107007	17.8 121.2 40	18.3 121.7 60. 41. 20.	0.0 0.0 00. 0.	n.# 0.0 00. 0.	n.0 0.0 0O. n.				
1107067	18.3 120.2 35	19.2 121.# 35, 105. 0.	0.0 n.0 0u. n.	n.u 0.0 u0. 0.	0.0 0.0 00. 0.				
110/12/	17.0 117.9 30	19.2 121.8 25. 2575.	0.n n.n 0u. n.	n.0 0.0 00. 0.	n.o 0.o 0o. n.				

	A, L	FIRECAS			
	MHNG	24 IR	48-4₹	72-48	
AVO FORFCAST POSTT FHHOM	43.	148.	247.	305.	
AVG RIGHT ANGLE ERDON	20.	69.	111.	247.	
AVG INTENSITY MAGNITUDE ERROR	17.	28.	30.	74,	
AVG INTENSITY STAS	-3.	-10-	-19.	>.	
NUMBER OF EDGECASTA	2.2	1.3	16		

# TROPICAL STORM WAYNE

HEST THACK ARRYING							24 HOUR FORECAST				48 HOUR FRAFCAST					12 HOUR FORFCAST						
						FRA	035				ERM.	J45				FRRA	₹5					
MU/JA/Ha	POSIT .	1100	P.35	1 1	rNI	DST	WINT	Par	118	₩ I YO	100	41.0	POS	17	WIND	nst	<b>∉IN</b> 0	404	11	WIND	251	WINU
1107002	9.9 141.5	15	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	- U •	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	и.
1101062	12.4 141.0	15	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	Λ.	0.0	0.0	0.	-0.	0.	0.0	0.0	D.	-0.	D.
1107122	14.4 179.9	15	0.0	0.0	υ.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1107182	14.8 137.7	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-O.	0.
1100002	15.0 135.7	20	0.0	0.0	0.	-0.	o.	0.0	0.0	Ď.	-0.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
1108067	15.0 113.6	25		134.5	25.	52.	ō.	18.1		>0.		10.		130.3		235.	5.		1.44.9	45.	504.	10.
1108122	16.4 132.1	30		132.7	30.	13.	o.		127.4		232.	Žn.		126.4		221.	15.		1/8.4		335.	15.
1108185	16.0 130.5	30		130.5	30.	65.	o.		12-4		252.	0		124+1		371.	5.		175.4		341.	10.
1107007	15.8 129.9	35		129.0	35.	53.	Ü.		124.1		290.	-5.		123.5		375.		0.0	0.0	0.	-0	0.
1109062	15.8 129.9	•0		128.0	35.	57.	-5.		124.4		276.		0.0	0.0	0.		0.	0.0	0.0	ö.	-0.	0.
110+127	16.2 129.7	45		129.7	45	24.	ő.		127.9	>5.				123.6		272.	20.	0.0	0.0	ů.	-0.	0.
1109187	16.9 129.3	45		129.7	ου.	33.	5.		129.2	60.		10.		129.5		107.	25.	23.0	143.3			0.
1110007	17.5 129.0	50		129.1	50.	21.	ő.		129.9		174.	20.		134.9		569	20.	0.0	0.0	0.	-0.	0.
1110062	17.8 128.9	50		129.2	50.	34.	ŏ.		120.0		185.	20.		135.1		h30.	15.	0.0	0.0	0.	-0-	0.
1110122	18.0 1/8.7	50		128.3	50.	42.	0.		126.4		137.	30.		127.2		351.	10.	0.0	0.0	0.	-0.	0.
1110182	18.2 128.4	50		128.7	20.	5.	0.		127.1	55.				126.2		295.	10.	0.0	0.0	0.	-0-	0.
1111002									124.4			3^•		128.9								0.
1111062	18.6 128.5	40		128.5	40. 35.	.6.	٥.		129.3		162.	ln.				477.	۶.	n.0	0.0	ŏ.	-0.	0.
1111122	18.8 128.5	35				13.	٥.			30.		٠.		158-9			5.	0.0	0.0	0.	-0-	
	18.9 128.2	55		128.5	25.	19.	0.	0.0	0.0	٥.	-0+	n.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	۹.
1111102	18.7 127.4	25		124.5	25.	40.	٥.	0.0	0.0	0.	-0-	٠.	0.0	0.0	0.	-0.	٥.	^.0	0.0	٥.	-0.	ņ.
	18.3 127.3	Š۲	0.0	0.0	٠,0	-0.	۰.	0.0	0.0	٠.	-0-	٠.	n_0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0-	٥.
1112062	18.1 126.R	30		150.0	30	_0.	٥.		124.2	45.		10.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.
1115155	17.8 126.2	30		150.2	30.	21.	٥.		124.9			30.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
1115187	17.4 125.4	3 n		156.2	30.	50.	٥.		124.5	30.		10.	n.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.
1113002	16.9 124.A	24		15200	25.	21.	0.	0.0	0.0	۰.	-0.	υ.	n. 0	0.0	0.	-0.	0.	٥.٠	0.0	0.	-0-	٥.
1113062	16.7 173.7	54		123.A	25.	25.	٥.	0.0	0.0	٥.	-0.	n.	٥.٥	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	۰.
1113127	15./ 172.4	25		155.4	25.	0.	٥.	0.n	n.n	٥.	-0.	ο.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	۰.
1113187	15.2 121.4	50	15.2	151.4	20.	6.	٥.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٥.	n . 0	0.0	٥.	-0.	п.

	AI L	FTRECAS				
	HMMG	24-4R	48-H3	72-48		
AVG FORECAST POSIT FRANK	27.	170	362.	443.		
AVG KIGHT ANGLE ERDAR	14.	115.	295.	413.		
AVG INTENSITY MAGNITOUF ENGIN	٥.	13.	12.	٩.		
AVG INTENSITY HEAR	o.	10.	10.	٠.		
NUMBER OF FORECASTS	22	16	12			

#### TROPICAL DEPRESSION 26

HEST THACK JAHATAG					SE HUIN ENHERS					48 HOUR FORFCAST					15 43AN EUSECECE								
							- Q1	4045				EHM	Jas					45					
HUNDELOP	P3511	× 1	VP.	PAS	1 T	HINT	031	#IN3	Par	511	4140	251	@ [ wif)	PHS	11	GFIF	051	dIND	POC	[ *	4[V]	251	4190
1154185	12.2 154.	5	15	0.0	0.0	٥.	-0-	0.	0.0	8.0	0.	-u.	۰.	0.0	0.0	U .	- 0 .	0.	0.0	0.1			0.
1130007	13.6 154.	4	15	0.0	0.0	O.	-0-	0.	0.0	0.0	o.	-0.	۰.	0.0	0.4	Ü.	-0.	0.	0.0	0.0	0.	-0.	0.
1110067	14.9 154.	4	15	0.0	9.0	ο.	-0.		0.0				۰.	0.0	0.0				0.0	0.0			
1130122	16.2 154.	2	ζ0	0.0	0.0	0.	-0-	U.	0.0	0.0	0.	-0.	٠.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
1130182	17.4 153.	3	24	0.0	0.0	v.	-0-	Ú.	0.0	0.0		-0-		0.0	0.0				0.0	0.0			
1201007	18.5 152.	3	25	19.7	152.7	25.	13.	n.	24.5	144.7	10.	17.	0.	0.0	0.0		-0.		0 . D	0.0			
1201067	19.7 151.	۸.	30	19.5	151.4	30.	5.	0.	25.9	150.0		60.		0.0	0.0				0.0	0.0			
1501157	20.9 150.	7	30	e. 05			33.				10.		15.	0.0	0.0				0.0	0.0			-
1501187	22.5 150.	n	10	25.5	150.5	30.	31.			0.0				0.4	0.0		-0.	0.	0.0	0.0			0.
1202007	24.2 149.	н	30	24.5			21.		0.0				0.	0.0	0.0	U.			0.0	0.0			_
	20.7 150.		30				19.		0.0					0.0	0.0	υ.			0.0	0.0			
	28.2 .52.		15	0.0	0.0				0.0		0.	-0.	0.	0.0	0.0				0.0	0.0		-0.	0.

	A: L	15		
	WHAS	74 - 4R	48-44	72-48
AVG FORECAST POSTT FRHOM	71.	55.	٠.	ο,
AVG HIGHT ANGLE EHADH	16.	28.	0.	ο,
AVG INTENSITY MAGNITUDE EPROF	n.	5.	٦.	n.
AVG INTENSITY HTAS	n.	5.	٥.	0
NUMBER OF FORECASTS	4	3	a	,

## TYPHOON ABBY

	HEST THACK		ARVING FAROAS			24 40	91H F(	HECA:		48 HOUR FORFCAST					15 HOUR FOURCAST				
40/J4/Hp	POSIT WIND	PISTT .	LING DST		Pasi	7 7	wi wo	Ust	41+0	ens	11	w140		dINO.	P)9	11	CFIE	451	w190
1129002	6.8 169.n 15	0.0 0.0	00.	0.	0.0	0.4	0.	-4.	٠	0.0	0.0	0.	-0.	0.	n.0	0.0	0.	-0.	0.
1129067	6.0 148.1 15	0.0 0.0	00.	Ü.	0.0	0.0	0.	-0.	۰.	0.0	0.0	<b>U</b> •	-0.	3.	0.0	0.0	ō.	-0.	0.
115-157	6.8 147.7 15	0.0 0.0	0n.	0.	0.0	0.0	o.	-0.	٥.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
1124187	6.7 166.0 15	0.0 0.0	Up.	n.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
1130002	6./ 156.3 15	0.0 0.0	00.	0.	0.0	0.0	o.	-0.	۸.	6.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1130067	6.6 145.4 20	0.0 0.0	00.	0.	0.0	0.0	ò.	-0.	ο.	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	0.
1130127	6.5 144.9 20	0.0 0.0	0n.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	v.	- J .	٥.	0.0	0.0	0.	-0.	0.
1130187	6.3 164.2 20	0.0 0.0	00.	0.	0.0	0.0	0.	-0.	n.	0.0	0 • 0	O.	-0.	0.	0.0	0.0	ø.	-0.	п.
150100%	6.2 163.4 20	0.0 0.0	VO.	0.	0.0	n . a	0.	-0.	0.	0.0	0.0	ø.	-0.	٥.	0.0	0.0	٥.	-0.	0.
1201067	5.9 162.0 24	0.0 0.0	00.	0.	0.0	0.9	0.	-0.	۰.	0.49	0.0	0.	-0.	٥.	n.0	0.0	0.	-0-	0.
1501157	5.8 141.0 25	0.0 0.0	UD.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	U.	-0.	0.	0.0	0.0	Ú.	-0.	ο.
1501181	5./ 160.4 30	5.7 151.1	25. 22.	->.		15H.1	JO.	77.	•16.		154.4	37.	/h].	-5.		120.4		297.	-25.
1505001	5.8 [60.1 An	5.7 (50.1	15. 13.	-5.		54.0	45.	184.	٠.		151.6		· nu	15.		147.9			>0.
1505001	5.4 159.4 41	5.9 154.1	35. 42.	-5.		151.0		361.	10.		120.0		409.	10.		196.4		449.	20.
1505157	6.0 159.4 45	5.9 159.1	35, 30,	-10.		144.4		148.	10.		153.6		155.	0.		150.0		225.	20.
1505182	6.1 159.1 45	5.4 15H.Q	35. 74.	-10.	6.9			120.	10.		152.7		184.	0.		144.5		276.	35.
1203007	6.3 159.1 45	5.3 159.0	55. 5.	10.	7.0		'nŝ.	78+	5u•		154+8	30.	70.	20.		170.6		127.	55.
1203067	6.5 149.0 40	5.3 159.0	60. 12.	٠٥٠	6.7		/5.	94.	50.		155.3	50.	46.	50.		151.4	90.	44.	60.
1203127	6.8 15R.0 40	5.4 159.0	45. 25.	۶.	7.5		05.	43.	٠.		154.9		106.	20.		151.2	90.	45.	40.
1203182	7.3 158.4 44	5.7 15H.4	•5. 3a.	.5.	H.A		00.	76.	۰.		154.2		114.	25.	10.5			142.	40.
1204002	H.1 158.1 45	8.1   54.5	55. 12.	10.	10.0			108.	5.		150.8		153.	٠0.		145.0		155.	40.
150+157	8.2 157.4 55 8.2 156 4 50	8.9 157.7	35. An.	٥.	10.P			170.	٠,	11.9			210.	45.		143.9		195.	55.
1204187		4.2 156.1	55. 14.	-5.		51.5		155.		11.6			202.	45.		143.2		140.	55.
1200107	8.2 155.4 An	9, 7 154.0	60. 59.	0.	9.0 1			161.	50.		145.8		140.	55. 55.		0.5+1		210.	50.
1203007	8.1 154.2 Fr	8.5 153.8 8.3 154.4	60. 79. 60. 17.	0.	9.5	150.7	70.	175.	35.		144.8		155.	50.		140.3		252.	40.
1203127	8.0 153.3 PO	7.2 153.2	60. 13.	Ü.	A.7		70.	22. 53.	40.		145.6	50. 50.	71.	50.		141.7	95.	67.	65.
120518/	8.3 152.5 50	1.9 152.0	35. 42.	5.	9.2		n5.	40.	35		143.8	50.	40.	45.	11.8		90.		
1500007	d.d 151.5 35	9.3 (5).4	55. 42.	20.	9.2		no.	71.	30.		143.4	50.	R 3.	25.		119.7	55.	13.	50. 20.
1205067	9.2 151.n in	9.4 150.9	55. 17.	25	10.r		70.	77.	15.		142.9	40.	75.	10.	11.6		30.	54.	-5.
1500157	7.2 149.A In	9.4 150.3	25. 30.	25.	11.0				15.		142.7	45.		15.		119.4		133.	-5.
1205187	9.8 148.1 30	9. 3 149.1	50. 54.	20.	11.2		>0.	17.	15.		141.0	45.	39.	15.		147.6		233.	-15.
		10.1 145.5	20. 71.	20.	11.0			460.	-	15.1			4 19.	-5.		141.0		455.	-30
		10.2 143.2	20. 159.	15.	12.0			450.	10	15.0			381.	-5.	n.0	0.0	ō.	-0.	n.
		10.4 143.0	DU. 135.	15.	12.0			283.	15.		133.3		354.		0.0	0.0	0.	-0.	n.
120/18/	11.0 144.4 15	11.0 145.0	45. 17.	10.	12.0			130.	10.		141.0		197.		0.0	0.0	٥.	-0.	n.
1509001	11.7 144.1 35	11.4 144.5	40. 29.	٠.	13.5 1	42.1	35.	235.	n.	14.2	140.3	¿0.	500.	+J0.	0.0	0.0	0.	-0.	0.
1509067	12.1 143.3 40	11.0 143.4	15. 37.	÷.	14.7	41.4	.30 .	314.	-4,	0.0	0.0	0.	- O .	0.	0.0	0.0	0.	-0.	0.
	12.2 142.1 30	162.2 162.1	35. 1.	5.	15.2	1.45	en.	545.	-20.	0.0	0.0	U.	-0.	0.	0.0	0.0	0.	-0.	0.
		15.5 140.0	J5. 45.	٥.	0.0	0.0	0.	-0-	n.	0.0	0 • 0	U .	-0.	٥.	0.0	0.0	0.	-0.	0.
		11.4 134.3	30. 23.	• > •	11.0		۲5.		474.		127.2			-60.	n • 0	0.0	0.	-0-	0.
		11.1 137.0	30. 30.	-5.		31.7	15.	85.	• 24.		152.1			-55.	0.0	0.0	٥.	-0.	п.
		10.4 135.1	45. 51.	٥.	10.0			2230			153.0		479.		0.0	0.0	٥.	-0.	0.
		10.0 133.7	45. 64.	.0.	9.0			244.		4.0	0.0	٠٠.	-0.	0.	0.0	0.0	0.	-0.	n.
		11. 1 133.4	Po 54.	10.	15.4			154.			12100		412.			117.6		094.	-AD.
		11.7 132.4	50. 24.	. " •	13.2 1			100.			155.5		737			117.5		103.	
		12.1 132.2	50. 13.	-10.	13.7			100.			124.0		-15			117.0		1.5.	-40.
		12.4 131.5	50. 21.	-12.	14.4			144.			154.4		445.			120.7		143.	- 10.
	13.7 [30.6 HO	13.7 130.7	HO. 5.	0.	16.0			174.			155.2		711.		0.0	0.0	٥.	٠٠.	ο.
	14.2 130.1 %	14.2 130.0	HU. 5.	-5.	16.4 1			2420			155.7		747.		n.0	0.0	0.	-0-	٥.
		14.7 124.7	HO. 23.		16.7			<790			123.3		473.		0.0	0.0	٥.	-0.	٥.
		15.8 130.2		-75.	20.0 I			12/-			134.3		140.		0.0	0.0	0.	-0-	n.
																		-0-	n.

1212067	17.1 141.0 100	17.4 130.0	9 100.	19.	<b>u</b> .	21.0	134.3	00. 13:	. 450.	24.H	147.0	j>.	276.	-5.	0.0	0.0	0.	-0.	0.
1515155	18.0 132.0 100	17.9 131-	a 45.	13.	-5.	21.R	134.1	00. je	. 43n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0-	
1515185	18.9 133.1 Lon	19.9 133-	2 45.	4.	-15.	23.0	140.1	45. 74	. 435.	0.0	0 • 0	٥.	-0.	0.	0.0	0.0	٥.	-0.	
1513001	19.8 114.5 110	20.n 134.	9 85.	25.	-25.	24.n	147.4	45. 13:	. *15.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	
121306/	20.5 136.2 110	21.1 136.5	BO.	53.	- 30.	25.n	144.4	J5. 261	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1519157	21.2 138.1 40	21.4 138.	> 100.	13.	10.	74.7	147.2	55. 123	. 24.	n_n	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	۰.
	21.8 140.1 HO																		
1214002	22.2 142.4 60	22.7 142.0	. 70.	13.	10.	0.0	0.0	0		n . ()	0.0	٠.	-0.	٥.	0.0	9.0	0.	-0.	0.
1214067	22.6 144.9 40	22.5 145.0	n 60.	٩.	20.	0.0	0.0	0		0.0	0.0	0.	-0.	0.	0.0	0.0		-0-	0.
	22.7 147.7 3n																	-0.	
1514185	22.8 150.7 3n	0.0 0.0	n U.	-0.	u.	0 • n	0.0	0		0.0	0.0	u.	-0.	٥.	n.0	0.0	0.	-0.	٥.
1512005	23.0 153.0 25	0.0 0.0	n 0.	-0.	٥.	0.0	0.0	0	٠ ٨.	0.0	0.0	u.	-0.	٥.	O.O	0.0	۰.	-0.	٥.

	AIL	FIRECAS	15	
	HMNG	24-48	48-44	72-46
AVE FURECAST POSIT FRANK	31.	164.	285.	37A.
AVG RIGHT ANGLE ERANN	17.	108.	199.	215.
AVG INTENSITY MAGNITUDE ERRUR	10.	20.	30.	47.
AVG INTENSITY HTAS	₹.	-2.	-1.	27.
NUMBER OF FORECASTS	5>	4.8	39	25

#### TROPICAL STORM BEN

	HEST T	44CK			dAHVI		303S		54 HL	Y## F(	HECA			46 H	DISR F	HFC4			72 H	OUR Fr	RFC4	<b>L</b> Ţ
40/36/Ha	POSIT W	IND	POS		din-	051	WIND	Pns	. 7	w1 NO		d I NO	PO!	517	wIND	DST	JIND	209		GFIW	nST	M I MD
1217007	7.0 149.0	15	0.0	0.0	Ö.	-0-	0.	0.0	1.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	. 0.0		-0.	0.
121/06/	7.3 148.0	15	0.0	0.0	ŏ.	-0.	o.	0.0	0.0	ŏ.	-0.		0.0	0.0	٥.	-0.	ö.	0.0	0.0	ě.	-0.	ö.
		15		0.0	ŏ.		ŏ.	0.0	0.0	ŏ.	-0.	n.	0.0	0.0	0.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.
151/157	7.5 147.0		0.0			-0.						-		0.0	0.			0.0		ŏ.		ö.
1217182	7.7 146.0	15	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0-	٠.	0.0			-0.	٥.		0.0	٧.	-0.	
1518005	8.0 145.0	15	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٧.	-0.	0.
1518065	8.2 143.9	15	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٠.	-0.	0.
1579151	8.5 142.7	15	0.0	0.0	0	-0.	٥.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٠.	-0.	٥.
1518187	8.7 141.4	15	0.0	0.0	٥.	-0.	٥.	0.0	0.0	ο.	-0.	۰.	0.0	0.0	۰.	-0.	٥.	n • 0	0.0	٠.	~0.	٥.
1514005	9.0 140.0	15	0.0	0.0	ů.	-0.	0.	0.0	4.0	٥,	-0.	۸.	n.a	0.0	۰.	-0.	٠.	0.0	0.0	0.	-0.	٥.
1514065	4.4 13B.A	15	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	٥.	0.0	0 • 0	٥.	-0.	٥.	0.0	0.0	۰.	-0.	о.
1519155	9.9 137.0	15	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	-0.	0.
121+18Z	10.4 135.5	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0-	٥.
122000Z	10.9 134.0	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.
1220062	11.3 132.5	20	0.0	0.0	6.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	g.	-0.	ø.	0.0	0.0	0.	-0.	0.
1250152	11.6 130.A	25	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.
1220182	11.6 129.2	30	0.0	0.0	0.	-0.	o.	0.0	0.0	o.	-0.	٥.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	٥.
1221007	11.5 127.6	4.0	0.0	0.0	o.	-0.	ō.	0.0	0.0	0.	-0.	0.	4.0	0.0	o.	-0.	0.	0.0	0.0	٥.	-0.	n.
1221062	11.4 126.0	50		125.4	50.	ă.	ō.		127.1	35.	93.	415.		119.3	35.	199.	0.	0.0	0.0	٠.	-0-	٠.
1551155	11.8 124.3	• 0		124.4	45	21.	5.		121.2	35,			15.1	118.6	35.	375.	10.	0.0	0.0	٥.	-0.	0.
1221182	12.2 123.0	• 0		155.7	•0.	30.	ŏ.		114.0	35.		.25.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
155500Z	12.7 121.8	45		121.4	50	6.	š.	14.3			130.		0.0	0.0	٥.	-0.	ö.	0.0	0.0	ě.	-0.	ñ.
122206Z	13.0 120.5	50		120.4	40	5.	-10.	15.4			281.		0.0	0.0	٥.	-0.	i.	n . 0	0.0	Ď.	-0.	0.
1555155	13.8 119.4	55		119.0	50.	24.	-5.	17.7		35.	380.	10.	0.0	0.0	ő.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	0.
1225192	14.6 119.2	66		118.2	50.	61.	-10.	0.0	0.0		-0.	10.	0.0	0.0	ă.	-0.	i.	0.0	0.0	ŏ.	-0.	0.
1553005				119.4	55.		0.	0.0	0.0		-0.			0.0	ă.	-0.	ŏ.	0.0	0.0	i.	-0.	0.
	15.6 119.5	55				٠.				٥.			0.0							ŏ.		0.
1223062	17.6 121.0	35		119.9	45.	75.	10.	0.0	0.0	٠.	-0.	٠.	0.0	0.0	٥.	-0.	٥.	0.0	0.0		-0.	
1553155	19.6 123.4	25	15.4	155+1	۲۶.	103.	o.	0.0	0.0	۰,	-0.	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.

	AI L	FIRECAS	TS	
	HNG	24-4R	48-H2	7>-4R
AVG FORFCAST POSIT FRROR	74.	181.	267.	٥.
AVG 41G41 ANGLE ERONR	18.	A9.	15.	n,
AVG INTENSITY MAGNITUDE ERROR	5.	14.	5.	۰.
AVG INTENSITY BIAS	-1.	-11-	3.	n.
MIMAED OF CONCLETE	1.0			

# 2. NORTH INDIAN OCEAN CYCLONE TRACK DATA

TC 17-79

		AEST T	RACK			HARVI		RORS		24 40	11 M F	HECA!			48 H	DIJR FO	FRED			15 45	OUR Fr	NFC4	47
MO/DA/HO	Post	7	IND	POS	7 7	wINn	DST	WIND	Pns	1 T	w I WD		GNIP	POS	I T	HIND	DST	dIND	PDS	19	GP I W	nst	-
050508Z	6.3	90.0	15	0.0	``0.0	0.	+0.	0.	0.0		0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0-	0.
050514Z	6.4	90.4	50	0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	0.	-0.	n.	0.0	0.0	ŏ.	-0.	ŏ.	0.0	0.0	ě.	-0.	0.
050520Z	6.5	49.7	20	0.0	0.0	ō.	-0.	ō.	0.0	0.0	ŏ.	-0.	0.	0.0	0.0	ů.	-0.	ó.	0.0	0.0	ë.	-0.	0.
0506022	6.6	89.1	25	0.0	0.0	ō.	-0.	0.	0.0	0.0	ō.	-u.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	ů.	-0.	٠.
0506482	7.0	A8.4	25	0.0	0.0	Ď.	-0.	ō.	0.0	0.0	0.	-u.	0.	0.0	0.0	ă.	-0.	Ŏ.	0.0	0.0	ŏ.	-0.	6.
0506147	7.5	A8.4	30	7.2	87.7	30.	45.	ŏ.	8.7	85.8	35.	129.	-5.	10.1	84.5	454	243.	-15.	12.0	#4.0		201.	-5.
0506202	7.6	98.0	30	7.4	87.5	30.	35.	õ.	8.0	85.5	35.	148.	910.	10.A	84 - 1	45.	259.	+15.	12.7	M4.3		155.	-5.
0507022	7.1	47.A	35	7.9	88.0	35.	49.	ů.	9.6	88.2	45.	264.	-5.	11.2	88.7	25.	257.		13.3	#9.7	65.	123.	0.
0507082	6.7	97.2	35	7.2	87.7	35.	42.	ō.	8.7	87.5		174.	915.	10.5	88.2	>>.			12.6	4.64		308.	-5
0507142	6.7	86.6	60	7.6	87.1	40.	61.	o.	9.4	87.0		222.		12.0	89.0		247.	5.	14.0	¥0.7		420.	-5
0507202	6.4	86.1	45	7.5	86.4	45.	72.	ō.	9.4	64.4		148.	0.	11.6	86.7		113.	10.	13.0	MH . B		327.	0.
0508027	5.8	86.0	50	6.9	86+0	50.	66.	v.	7.6	83.2		184.	-5.	A . S	80.0			-10.	4.4	16.7	50.	412.	-25
0508087	5.9	86.4	60	5.6	96.0	60.	30.	ō.	4.0	83.4		254.	۸.	6.4	80.2		470.	0.	5.3	17.1			
0506142	6.5	A6.4	60	5.2	85.4	60.	98.	o.	4.0	82.4		330.	٠.	5.0	79.2		511.	-5.	4.5	76.1		590.	-15
0508202	7.1	H6.4	60	5.9	86.7	60.	73.	o.	5.7	85.1		275.	5.	5.4	84.0		439.	-5.	5,4	H0.5	70.	521.	-15.
0509022	7.6	86. T	65	7.3	86.2	65.	19.	٥.	8.2	84.2	70.	181.	٩.	9.0	81.5	65.	249.	-10.	9.4	18.7	60.	128.	-20
050908Z	8.2	86.1	65	7.A	85.A	65.	30.	٥.	9.0	84.1	70.	161.	n.	10.3	81.5	65.	191.	-15.	11.0	18.7	50.	264.	- 30
0509142	9.2	45.9	60	8.8	85.4	60.	30.	0.	10.4	87.5	55.	114.	-20.	11,9	61.2	50.	111.		17.7	18.9	45.	198.	-15.
050920Z	10.3	45:1	60	10.4	85.2	60.	в.	0.	12.7	82,7	60.	42.	915.	13,0	80.0	>5.	70.	-30.	13.3	18.9	30.	276.	-20.
0510022	11.2	94.6	65	10.9	84.7	65.	25.	0.	12.3	61.A	60.	6/.	.15.	11.0	80.0	60.	101.	-20.	0.0	0.0	٥.	-0.	
0510082	11.7	84.7	7 n	11.6	83.9	75.	19.	5,	12.5	81.4	65.	75.	۶.	13.1	79.4	55.	132.	-25.	0.0	0.0	0.	-0.	0.
0510147	12.3	43.7	75	12.1	83.4	75.	21.	0.	13.7	81.2	45.	44.	n.	14.0	79.4	50.	170.	-10.	0.0	0.0	٥.	-0.	Α,
051020Z	12.7	43.7	75	12.7	93.4	75.	15.	٥.	13.7	81.4	85.	33.	۰.	14.5	79.0	50.	178.	0.	0.0	0.0	٥.	-0.	٥.
0511022	13.0	A2.7	75	13.1	82.4	80.	۹.	5.	14.1	84.9	H5.	25.	5.	0.0	0.0	۰.	-0.	0.	0.0	0.0	٥.	-0.	О.
<b>051108</b> 2	13.4	45.3	KA	13.2	92,3	90.	12.	10.	14.7	80.5	105.	64.	25.	0.0	0.0	0.	-0.	۰.	0.0	0.0	٥.	-0.	0.
	13.7	A1.7	85	14.2	80.9	95.	55.	10.	16.5	78.2	30.	70.	<b>-3</b> n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
	14.1	91.7	H5	14.1	60.8	95.	23.	10.	16.0	74.5	30.	64.	<b>420</b> .	n.0	0.0	٠.	-0.	0.	0.0	0.0	٥.	-0.	n.
	14.5	90.R	40	14.4	80.5	90.	18.	10.	8.0	0.0	0.	-0.	۰.	n.u	0.0	۰.	-0.	0.	0.0	0.0	0.	-0.	n,
	15.2	40.1	AΛ	]4.R	90.5	85.	33.	5.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٠.	0.0	0.0	٥.	-0.	0.
	16.0	79.3	60	15.2	79.9	60.	59.	0.	0.0	0.0	0.	-0.	۸.	0.0	0 • 0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
051220Z	17.0	78.1	Sn.	17.0	78+1	50	0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	٥.	0.0	0.0	G.	-0.	0,

#1 L	FORECAS	113	
MHNG	24-4R	48-H3	72-4
36.	139.	233,	346.
17.	95.	195	296.
2,	9.	13.	12.
2.	-5.	-11.	-12.
24	22	18	14
	WHNG 36. 17. 2.	WHNG 24-4R 36. 139. 17. 95. 2. 9. 25.	76. 139. 233. 17. 95. 192. 2. 9. 13. 2511.

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#### TC 18-79

		AEST	TRACK			WARUT				24 H	nik F				48 H	011R F	nRFGA'			92 H	OUR FO	BECAS	ŧŢ
							FR	R045				EHH	245				FRED	45					
40/04/HR	POSI	Ŧ	#[ND	POS	T T	WINT	DST	WINS	Pns	TT.	₩1 NO	051	d [ MI)	PNS	IT	GM 1 w	DST	-IND	POS	11	WIND	nST	#190
0617142	17.7	66.	25	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	n,	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	'n.
0617202	17.9	45.	5 30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
0614027	18.0	64.1	a 3n	18.3	65.7	40.	34.	10.	19.5	64.6	>0.	238.	٨.	21.5	65.0	60.	426.	20.	n.0	0.0	٥.	-0.	0.
2808100	18.0	64.	35	18.4	64.0	40.	56.	5.	19.4		55.	248.	٩,	22.0	64 - 8	60.	482.	35.	0.0	0.0	0.	-0.	0.
9618147	18.2	63.	1 40	18.2	63.A	45.	40.	5.	19.4	62.3	55.	170.	٩,	22.6	63.5	60.	445.	40.	0.6	0.0	٥.	-0.	0.
9618202	18.2	61.	45	18.5	62.4	45.	38.	0,	19.7	59.7	>5.	40.	٩.	21.6	56.5	40.	100.	25.	0.0	0.0	٥.	-0.	0.
961902Z	18.0	60.	7 50	18.7	61.7	50.	70.	0.	20.0	54.4	50.	60.	10.	0.0	0.0	0.	-0.	٥.	0.8	0.0	٥.	-0.	٥.
9614082	18.4	59.	9 50	18.7	59.9	50.	IA.	0	20.7				۵,	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0619142	18.8	59.	5 50	18.5	58 - 4	50.	59.	0.	20.2	54.1	25.	115.	٩,	0.0	0.0	0.	-0.	٥.	n.0	0.0	٥.	-0.	0.
0619202	19.1	58.0	9 50	19.0	58.3	50.	29.	0.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	6.
062002Z	19.2	57.0	4.0	19.4	59.0	50.	69.	10.	0.0	0.0	٥.	-0.	٨.	n.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.
0620082	19.5	56.	4 25	19.8	58.7			20,	0.0	0.0	٥.	~ U •	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0-	٠.
2410560	19.8	56.	1 20	20.0	56.4	35.	41.	15,	0.0	0.0	٥.	~# .	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	0.
0620202	50.1	55.	7 15	20.5	55.4	25.	25.	10.	0.0	0.0	0.	-0.	٠,	0.0	0.0	0.	-0.	۰.	0.0	0.0		-0.	a.

	A1 L	FORECAS	TS	
	MMMG	24-48	48-43	72
AVG FORFCAST POSIT FAHOR	48.	137.	36 1.	0.
AVG HIGH! ANGLE EROOR	24.	78.	284.	0.
AVG INTENSITY MAGNITHUF ERROR	6.	5.	30.	ρ.
AVG INTENSITY HTAS	6.	5.	30.	0.
NUMBER OF FORECASTS	12	-;	- 1	

## TC 22-79

		HFST	THACK			JARVI		2025		24 M	nihi F	HELA:			48 H	Did F	PRECAT			15 4	UR Fo	RFC49	4
40/JA/HD	POS1	t	4110	₽g\$	T T	JINA			Pns	17	<b>4140</b>		91MD	Pns	17	w I NO		JINO	P05	1 +	CFIN	nST	W 7 NO
1500560	9.1	47.0		0.0	0.0			0.	0.0	0.0		-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0		-0.	0.
0920082	9.7	A7.4		0.0	0.0	ō.	-0.	o.	0.0	0.0	ō.	-4.	۸.	0.0	0.0	0.	-0.	ů.	0.0	0.0		-0.	٥.
0450142	10.1	46.4	4 2n	0.0	0.0	0.	-0.	v.	0.0	0.0	0.	-0.	۰.	0.0	0.0	٥.	-0.	٥.	4.0	0.0	0.	-0.	0.
0450505	10.4	46.4	20	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.
0451055	10.7	46.7	7 20	0.0	0.0	٥.	-0.	٥.	0.0	0.0			٨.	0.0	0.0	٥.	~0.	0.	0.0	0.0	0.	-0+	٠.
9357085	11.1	45.4		11.n	85.5		٩.	٥.	12.5	87.4		140.	lo.	14.7	80.9		137.	30.	0.0	0.0	0.	-0.	0.
0451145	11.6	95.2	24	11.0	84.0		79.	0.	12.7	82.3		191.	10.	13.1	80.5		209.	30.	A.0	0.0	٠.	-0.	۰.
0951505	15.8	45.		12.1	84.9		42.	٥.		83.0		130.		14.4	80.9			30.	0.0	0.0	٥-	-0.	٥.
2502560	14.0	44.1		12.5	64.4			5.	13.7	82.5		140.		0.0	9.0	٥.	~0.	ø.	0.0	0.0	٠.	-0.	٥.
0.0550.05	14.9	43.4		13.5	82.A		105.	10.	14.5	81.1		151.		0.0	0.0	٥.		o.	0.0	0.0	٠.	-0.	٥.
7415560	15.3	43.1		15.0	84.0		55.		16.7	61.4				0.0	9.0	6.	-0.	٥.	n.g	0.0	••	-0.	٠.
0255560	15.5	42.7		15.6	93.0			10.	18.0	60.7	10.	54.	^.	0,0	0.0	0.	+0.	٥.	7.6	0.0	ę.	-0.	٠.
0.45.1055	15.9	41.4		16.0	82.2	30.		10.	0.0	0.0		-0.	٠.	0.0	9.0	٥.	~0.	۰.	0.0	0.0	••	-0.	••
9953985	16.5	40.4		16.5	81.4	25.	34.	15.	0.0	0.0		-0.	ο.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٠.	-0.	••
0923147	16.6	40.		17.0	80.4	15.	29.	5.	0.0	0.0		-0-	٠,	0,0	9.0	0.	-0.	٥.	0.0	0.0	٠.	-0-	٠.
2021599	17.1	40.	3 10	0.0	0.0	٥.	-0.	٥.	0.0	0.0	ο,	-0.	٠,	0.0	0.0	٠.	~O.	٥.	0.0	0.0	9.	-9.	٠.

		AI L	FIRECAS	15	
		MMMG	24-49	48-47	77-48
AVG FO	DRECAST POSIT FRHAM	54.	122.	170.	0.
AVG K	IGHT ANGLE ÉROPA	74.	90.	122.	0.
AVG 1	STENSITY MAGNITHUE ERROR	6.	16.	30.	A.
AVG I	NTENSITY BIAS	6.	16.	30.	0
MUM 4F	A OF FORFCASTE	10	. ,	à	,

## TC 23-79

	,	4FST	THACK			gaRu;	NG			26 H	nille Ei	DHECA	51		48 HG	DUR F	nerca'	S T		72 H	NA Fr	AFC49	<b>.</b> T
								Ings				EHR					FR90	25					
40/DA/Ha	POSI	*	⊌ l vn	PnS	ŢŢ	WINS	051	WINT	Pns	17	₩I NO	051	#IND	POS	ĮŤ	WIND	กรา	= I ND	P09	11	W 1 WO	nST	4140
7508160	15.5	72.0	15	0_0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.
0916067	12.5	71.6	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	٥.
0918142	13.0	71.5	15	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	n.	0.0	0.0	ō.	-0.	ó.	0.0	0.0	0.	-0.	0.
0918505	13.4	71.4	15	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	o.	0.0	0.0	٠.	-0.	6.
2504160	13.9	71.4	20	0.0	0.0	o.	-0.	0.	0.0	0.0	٥.	-0.	Λ,	0.0	0.0	0.	-0.	ρ.	0.0	9.0	0.	-0.	
0919082	14.3	71.3	50	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٨.	٥.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.
2+14160	14.6	71.0	50	0.0	0.0	v.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	ο.
091 #20Z	15.0	70.4	20	0.0	6.0	0.	-0.	0.	8.0	0.0	ο.	-0.	0.	0.0	0.0	0.	-0.	o.	0.0	0.0	0.	-0.	0.
2500560	15.3	70.5	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	0.
0920087	15.6	70.7	25	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.0	0.0	о.	-0.	О.
0920142	16.0	49.9	24	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	0.
0920207	16.4	49.4	25	0.0	0.0	U.	-0.	0.	0.0	0.0	٥.	-4.	n.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.
0921027	16.8	49.7	25	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	0.
0451085	17.4	48.A	25	0.0	0.0	ø.	-0.	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	9.	-0.	٥.	n.0	0.0	٥.	-0.	0.
0921147	18.0	48.1	30	0.0	0.0	U.	-0.	٥.	0.0	0.0	٥.	-0.	0.	0.0	0.0	۰.	-0.	0.	0.0	0.0	٥.	-0.	0.
0921202	18.4	67.2	34	18.2	68.9	30.	97.	-5.	20.1	64.5	40.	294.	·ln.	77.0	68.6	45.	449.	5.	24.0	f0.0	20.	716.	-5.
0922022	18.6	46.2	<b>♦</b> n	15.7	68.7	30.	142.	-10.	20.7	64.5	40.	331.	-15.	22.7	68.9	45.	510.	10.	24.5	10.7	20.	879.	0.
7802260	19.0	45.7	45	19.2	65.7	40.	26.	-5.	20.2	67.5	45.	86.	-R.	20.8	61.6	45.	119.	15.	0.0	0.0	٥.	-0.	٥.
2415S60	19.3	44.3	45	19.0	64.4	40.	25.	-5.	19.4	61.3	>0.	13.	5.	20.5	58.0	0.	57.	-30.	0.0	8.0	٥.	-0.	0.
092220Z	19.6	43.7	51	19.6	63.7	50.	25.	10.	20.1	59.7	70.	51.	30.	20.4	55.9	20.	119.	-5.	0.9	0.0	٥.	-0.	n.
2506560	19.7	42.7	5.5	19.6	62.7	65.	5.	10.	20.4	SH.R	60.	73.	25.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٠.	-0.	•.
092308Z	19.9	42.0	50	19.9	61.7	65.	15.	15.	20.7	57.A	65.	107.	34.	0.0	0.0	0.	-0.	0.	n.0	0.0	٠.	-0.	0.
0923147	50.0	41.4	45	20.0	63.5	35,	118.	-10.	71.7	65.1	20.		<b>*</b> }^.	8.0	0.0	٥.	-0.	٥,	0.0	0.0	٥.	-0.	٥.
092320Z	20.2	40.4	40	20.3	60.3	35.	18.	-5.	72.1	57,7	20.	126.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	٠.	-0.	٠.
0924027	20.3	40.1	35	20.5	59.6	35.	33.	0.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٠.	-0.	٥.	A.D	0.0	٥.	-0.	0.
0924082	20.1	59.4	30	20.9	58.4	30.	61.	0.	0.0	0.0	0.	-0.	n.	0.9	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	
0924142	19.9	58.4	30	6.05	58.3	25,	37.	-5.	0.0	0.0	0.	-0.	п.	0.0	0-0	٠.	-0.	٥.	A.0	0.0	٠.	-0.	٥.
092420Z	20.0	57.8	25	19.8	58.0	25.	16.	0.	0.0	0.0	0.	-0.		0.0	0.0	٥.	-0.	٥.	n.0	0.0	٥.	-0.	٠.
0925U2Z	50.0	56.5	50	20.0	57.7	15.	45.	-5.	0.0	0.0	0.	-0.	۰.	0.0	0.0	٥.	-0.	0.	0.0	0.0	٥.	-0.	٥.

	AI'L	FTRECAS	15	
	PHNG	74-48	48-47	72-4R
AVG FORECAST POSTT FRHOR	40.	160.	253.	773.
AVE TIGHT AVELE FROM	21.	97.	184.	679.
AVG INTENSITY MAGNITUDE ERRUR	6.	16.	13.	٦.
AVG INTENSITY RTAS	-1.	6.	-1.	- 3.
NUMBER OF FORECASTS	14	9	5	,

### TC 24-79

	RFS	T TRA	-K		44R4	146			24 H	HIM FO				4d H	hid F	SRF CA	ST		72 H	UH FA	PFC&	t T
						FRI	1075				ENH	J45				FPRO	25					
HO/DA/HR	POSIT	w196	ר א	5 t T	dINT	DST	WIND	FAS	r T	4147	160	4[10]	PNS	17	WIND	720	#IND	404	11	CFID	251	4140
1053055	11.1 90	2		0.0	0.	-0.	٥.	0.0	0.0	٥.	-0.	n.	0.0	0.0		-0.	٥.	^.0	0.0	0.	-0.	0.
1029082	11.7 90	1.1 2	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	۸.	0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	٥.
1029147	12.2 45	. 4 2	12.5	89.4	50.	21.	o.	16.3	84.1	40.	250.	15.	10.0	91.9	30.	A 73.	-5.	14.8	45. R	15.1	036.	0.
1029202		20 20		89.0			o.	16.9	84.2		25/.	in.	19.6	90.2		629.		0.0	0.0	0.	-0.	0.
1030022	12.4 RF	1.2 2	13.6	88.7	25.	77.	Ü.	15.5	87.4		192.	5.	17.9	67.5		401.	10.	0.0	0.0	ō.	-0.	0.
1030082	12.6 81	7.1 2	5 12.6	88.2		65.		13.2	84.7	30.	163.	۸.	14.1	84.9	35.	295.	15.	0.0	0.0	٥.	-0.	0.
1030142	13.1 96	. 2		87.0		105.	o.	12.0	84.5		215.	-4.	14.0	85.1		355.		0.0	0.0	0.	-0.	a.
1030202		1.4 3		86.5			-5.	14+0	83.		121.	0.	0.0	0.0	0.			0.0	0.0	ě.	-0.	0.
1031022		. 9 3		84.4			-5.		80.4		167.	5.	0.0	0.0	v.	-0.	õ.	0.0	0.0	õ.	-0.	0.
1031002		3.9 3		83.5			ō.	15.0	80.1		197.	5.	0.0	0.0	ŏ.	-0.	õ.	0.0	9.0	ā.	-0.	0.
1031142		2.A 3		82.A			-5.	15.1	70.3		143.		0.0	0.0	0.		ŏ.	0.0	0.0	ě.	-0.	0.
1031202		1.0 3		82.4	30.		-5.	0.0	0.6	0.			0.0	0.0	ě.	- •	ŏ.	0.0	0.0	a.	-0.	0.
1101022		. 9 3		81.0			0.	0.0	0.0	0.			0.0	0.0	ŏ.		0.	0.0	0.0	0.	-0.	0.
1101062				79.9		17.	0.	0.0	0.0		-6.			0.0						ě.		8.
		1.1 2						2	-	٠,		4.	4.0		•	-0.		0.0	0.0		-0.	7
1101142	12.7 79	). ? I	5 12.7	79.6	15.	17.	٥.	0.0	0.0	0,	-4.	٠.	٥,٠	0.0	0.	-0.	٥.	0.0	0.0	۰.	-0.	a.

AVG FORECAST POSIT FHUNR 48. 100. 482. 107A.

AVG RIGHT AVGLE ERROR 26. 142. 332. 9A7.

AVG RITHRISITY HAGYLTUDE ERROR 2. 6. 11. 0.

AVG INTENSITY HAGYLTUDE ERROR 2. 6. 11. 0.

NUMBER OF FORECASTS 13 3 5 1

At the second of

### TC 25-79

	A	EST	TRACK			#AR VI				24 +	NIK F				48 H	Dijak Fr	THF CA'			12 43	JUR Fn	DFC & T	41
_							. 54	30.2S				EHH					FR30.	15					
MO/JA/HS	POSIT	'	A I AU	P05	1 <b>T</b>	u i No	DST	WIND	Pnsi	T	w I ND	051	4IND	POS	l T	WIND	nst	#IND	POS	[ *	#I NO	251	# T NU
1114027	12.3	70.1	20	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	۰.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	n.
1114087	12.8	70.0	50	0.0	0.0	0.	-0.	0.	0,0	0.0	o.	-0.	٥.	0.0	0.0	0.	-0.	ō.	0.0	0.0	0.	-0-	0.
1114142		49.9		0.0	0.0	ō.		ō.	0,0	0.0			0.	0.0	0.6	ō.	-0.	o.	0.0	0.0	ō.		0.
1114202		49.		0.0	0.4	ō.		ŏ.	0.0	0.0				0.0	0.0	٥.	-0.	ä.	0.0	0.0	ö.	-0.	0.
1112022		49.4		0.0	0.0	ŏ:	-0.	ŏ.	0.0	0.0		-0.	-		0.0		-0.						
1115087													٠.	0.0		٥.		٥.	0.0	0.0	٥.	-0-	n.
		49.1		0.0	0.0	٥.		٥.	0.0	0.0			Ů.	0.0	0.0	o.	-0.	٥.	4.0	0.0	٥.	-0.	4.
1115142		49.4		0.0	0.0	٥.	-0.	٥.	0,0	4.0			۰.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	٥.	-0.	۰.
1115202		49.4	30	0.0	0.0	٥.	-0.	٥.	0,0	0.0	٥,	-0.	٥.	0.0	0.0	v.	-0.	٥.	٠.٥	0.0	٥.	-0.	0.
1116027	15.0	49.9	35	15.0	70•^	40.	6.	5.	17.0	70.3	45.	72.	5.	10.5	71.4	ь0.	121.	45.	0.0	0.0	٥.	-0.	٠.
1116082	15.6	70.0	40	14.6	69.7	40.	62.	0.	15.4	60.0	45.	191.	10.	0.0	0.0	<b>u</b> .	-0.	0.	0.0	0.0	0.	_8.	О.
1116147	16.4	70.2	40	14.6	69.7		111.	0.	15.4	60.0	45.	234.	15.	0.0	0.0	0.	-0.	o.	0.0	0.0	o.	-0-	0.
1116202	17.3	70.4	40	17.3	70.4		23.	o.	20.2	74.7			ezs.	0.0	0.0	ō.		ō.	0.0	0.0	ö.	-0.	0.
1117027		70.2		18.1	71.5		76.	å.	0.0	0.0				0.0	0.0	a.			0.0				n.
1117482		70.1		17.9	71.9		115.											0.		0.0	р.	-0.	
1117142								o.	0.0	0.0			٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٥.
		70.1		19.7	70.1	30.	6.	٥.	0.0	0.0		-0-	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0	٠.	-0.	0.
1117202		70.>		20.3	70.7	25.	0.	٥.	0.0	0.0		-0.	۰.	n.a	0.0	٠.	-0.	٥.	0.0	0.0	۰.	-0.	۰.
1118022	21.3	70.4	15	0.0	0.0	۰.	-0.	٥.	0.0	0.0	٥.	-0.	۰.	0.0	0.0	0.	-0.	٥.	n.0	0.0	٥.	-0.	n.

	AIL	FIRECAS	15	
	WHNG	24-HR	48-47	72-4R
AVG FORFCAST POSIT FRROR	50.	169.	121.	0.
AVG RIGHT ANGLE ERDOR	26.	103.	73.	n.
AVG INTENSITY MAGNITUDE ERRUR	1.	14.	45.	0.
AVG INTENSITY RIAS	i.	i.	45.	n.
MIMAED OF FOOFCIETO			- ;	

### TC 26-79

		AFST	TRACK			MARUT	146			24 H	71 <b>84</b> F(	DRECA:			48 H	DIA F	ner Cas			15 40	WR Fn	RFC4	T.
							r pi	2025				EHH.	)4S				FRAN	15					
40/J4/H2	POSI	Ŧ	WIND	POS	11	#IN)	DST	WIND	Pns	11	w I wn	051	alw0	ens	11	#1 ND	757	#IND	<b>PD</b> 5	) †	CFIN	751	# 1 WU
1120142	8.0	94.	> 14	0.0	0.0	0.	-0-	0.	0.0	0.0	٥.	-0.	٥.	0.0	0.0	0.	-0.	0.	0.6	0.0	0.	-0.	٥.
1120202	8.8	93.		0.0	0.0	0.	-0.	0.	0.0	0.0	6.	-0.	۸.	4.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1121027	9.7	92.		0.0	0.0	ă.	-0.	o.	0.0	0.0	ă.	-0.	۸.	4.0	0.0	0.	-0.	ō.	0.0	0.0	0.	-0.	8.
112100Z	10.4	92.		0.0	0.0	ă.	-0.	ŏ.	0.0	0.0	ŏ.	-0.	۸.	0.0	0.0	0.	-0.	ő.	0.0	0.0	Ö.	-0.	0.
1121142	10.7	91.		0.0	9.0	o.	-0.	ŏ.	0.0	n,q	ŏ.	-0.	0.	0.0	0.0	0.	-0.	ō.	0.0	0.0	i.	-0.	0.
1151505				0.0	0.0	ě:	-0.	0.	0.0	0.0	ě:	-0.		0.0	0.0	ů.	-0.	ö.	0.0	0.0	ă.	-0.	0.
1124027	10.8	91.		0.0	0.0			ő.	0.0	0.0	۲.	-4.		0.0	0.0	٥.	-0.	ŏ.	0.0	0.0	Ď.	-0.	0.
	10.9	91.				g.	-0.				٠.	-0.		0.0	0.0	٥.	-0.	0.	0.0	0.0	0.	-0.	ö.
786687	10.4	90.		0.0	8.0	٥.	-0.	٥.	0.0	0,0	٠.										ů.		
1125145	10.7	90.		0.0	0.0	ů.	-0.	٥.	0.0	0,0	٠.	-4.	٠.	0.0	0.0	0.	-0.	٥.	0.0	0.0		-0.	٠.
1155505	10.5	18.		0.0	0.0	٥.	-0.	o.	0.0	0.0	٠.	-0.	٠.	0.0	0.0	٠.	-0.	٥.	4.0	0.0	Ģ.	-0.	n.
1151055	10.4	97.		0.0	0.0	٠.	-0.	٥.	0.0	_0,0	٠.	-4.	٠.	0.0	0.0	.0.	-0.	.0.	0.0	0.0	0.	-0.	٥.
1123082	10.6	46.	5 25	10.0	88.0	25.		٥.	10.7	84.4	30.		٠.	11.4	91.8	35.		10.	0.0	0.0	٥.	-0.	٠.
1123142	10.7	A5.	· 25	10.3	87.1		103.	5.	11.>	84.0	35.		٩.	12.0	80.9	35.	145.	20.	0.0	0.0	0.	-0.	٥.
1153505	10.7	H4.	3 30	10.5	84.0	35.	19.	5.	11.0	80.6	45.	30.	20.	0.0	0.0	U.	-0.	0.	n.0	0.0	٥.	-0.	0.
1124027	10.6	43.	30	11.0	92.5	J٥.	34.	5.	12.7	74.4	25.	124.	n.	4.0	0.0	0.	-0.	ο.	n.0	0.0	0.	-0.	0.
112408Z	10.6	92.	n 10	10.6	81.8	35.	17.	5.	11.>	77.0	20.	256.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	٥.
1124142	11.4	91.	3 30	11.0	80.4	35.	47.	5.	0.0	0,0	0.	-4.	٠.	0.0	0.0	0.	-0.	0.	0.0	0.0	٥.	-0.	٠.
1124207	12.2	HO.		11.9	79.4	30.	74.	5.	0.0	6,6	ä.	-0.	0.	4.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1125027	12.9	40.		11.9	79.A	30.	92.	5.	0.0	0.0	ŏ.	-0.	٥.	0.0	0.0	ů.	-0.	ō.	0.0	0.0	0.	-0-	0.
1125087	13.8	40.		13.0	90.0	25.	29.	ű.	0.0	0.0	ŏ.	-0.	٥.	0.0	0.0	u a	-0.	ā.	4.0	0.0	0.	-0-	0.
						50.	-		_	-		-0.	-	4.0	0.0	0.	-0.	ö.	0.0	0.0	ŏ.	-0.	0.
1125142	14.5	79.	7 15	14.5	79.4	eu.	٠.	٥.	0.0	0.0	G.	-0.	<b>~</b> .	11.0	0.0	٠.	-0.			0.0	••		

	AI L	FIRECAS	15	
	MHNG	24-4R	48-44	72-48
AVG FORECAST POSTT FRANK	<b>52.</b>	148.	163.	n.
AVG HIGHT ANGLE ERONH	٦1.	A3.	21.	ο.
AVG INTENSITY MAGNITUME ERROR	٠.	6.	ls.	Α.
AVG INTENSITY RIAS	٠.	4.	15.	0.
NUMBER OF FORECASTS	10	5	2	3

## ANNEX B TROPICAL CYCLONE FIX DATA

# L WESTERN NORTH PACIFIC CYCLONE FIX DATA

NOTICE - THE ASTERISKS (\*) INDICATE FIXES UNREFRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

### TYPHOON ALICE

### SATELL TIF FIXES

•							
FIX NU.		FIX POSTTION	*CC4Y	UVIDAK CODE	SATELL LITE	COMMENTS	SITE
			·-				
• 1	310900	1.44 1/2.2E	PCN 6		DECESE		PGTW
۷,	011536	1.9~ 140.5E	PCV h		Decose	**** ***	PGTW
3	011419	5.0v 167.3E	PCN 6	12.5/2.5	D44637	INI: JdS INI: JdS	KGWC PGTW
• ;	012336	4.90 186.0E 5.60 165.9E	PCM 6	15.0/2.0	044544	1411 253	KGWC
6	020351	5.54 167.5E	., .		GNFS3		PHIK
7	0 > 9 9 0 1	5.04 167.0E	PCN 6		DMSP47		PGTW
9	021518	5.94 167.0E	Pru b Pru b		044P35 0m4P37		PGT#
10	0>1+00 0>2133	4.9x 167.4E 7.0x 167.7E	PCN 6	12.0/2.0 /50.0/24HRS	045234		KG#C PGT#
11	022318	4.54 167.3E	PC4 C	120,7770 7 30007 241111	Dus0 15		KGWC
12	970741	H.SU IND. DE	PC4 6		Despa7		PGTW
13 14	046160	4.9N 169.3E	Prv 6 Prv 6	13.5/3.5 /01.0/29HRs	0w4P34 0w4P37		KG4C Phik
is	032115	9.54 IF4.1E	PCN 6	T3.0/3.0 /D1.0/24HRS	AFGPMO		PGT
16	072150	9.54 16H.DE			GOFS3		PHIK
17	240040	4.34 157.6E	PCN 5		DMENJE		PGTW
18	040350 040 <del>3</del> 57	9.90 157.1E 9.60 167.4E	PCN 6		60F57 0w5P74		PHIK PGT#
50	045005	4.64 165.6E	PCW 4		D=4277		PETH
51	042058	4.64 165.5E	Prv +	13.5/3.5 /DO.5/24HRS	DMERSA		PGTW
55	050024	9.54 165.UE	PCN 3		Dwspas		PGŢĦ
23	050350	4.9N 164.5E			GOFST		PHIK
24 25	050939 051305	10.1N 163.7E	PCM 6		DWSP36		PGT# PGT#
56	051743	11.04 162.4E	PCH 4	74.0/4.0 /00.5/23HRs	DMSP37		PETU
27	060006	11.14 141.7E	PCN 1		Duspas		PŠĪW
5.8 5.8	040323	11.94 150.0E	BUA 5		DMSP37 DMSP36		PGTW
30	040922 745140	11.74 150.7E	PCN 2		DMCP3A		PGTW PGTW
31	041923	17.64 158.1E	PCV I		Despa7		PGTW
32	045502	12.54 157.9E	PCN I	T5.0/5.0 /D1.0/26HRS	Duchar		PGTW
33	042348	17.4N 157.4E	PC4 S		DMSP35		PGTW
34 35	078350 078804	12.4N 157.0E	PC4 ?		GAFS 3 DWSP37	C1 UP	PHIK PGT#
36	071019	12.5% 155.AE			GOFST		PHIK
37	071047	12.4N 155.7E	PCN 2		Duchiv		PGTW
38	071230	12.44 155.3E	PCN 2	-4	DMCBSV		PGTW
39 40	072147 0#0112	12.24 157.2E 12.24 142.5E	PCM 1 PCM 1	T6.0/6.0 /01.0/24HR<	DMZDJY		PGT# PGT#
41	926080	12.04 151.2E	PCN 5		DMSP37		PGTW
42	040926	12.04 152.LE	PCN 6		Ducp17	INII JOS	RODN
43	041029	12.00 151.0E	Pru 5		DMCBSV		PGTW
44	091353 092025	11.90  5r.1E 11.90  48.6E	PCN 2		DWSP35		PGTW PGTW
46	040054	11.94 147.5E	PCN 4	14.5/5.5 /41.5/27HRC	DMSP35		PGTW
47	090706	17.3N 145.7E	PCN 6		DMSP37		PGTW
48	091011	12.34 145.7E	PCN 6		DHSP36		PGTU
49 50	091335	17.00 145.2E	PCN N PCN I	T3.5/4.5 /W1.0/23HRS	DMCP35 DMCP3A		PGTu PGTu
51	100217	12.0H 142.6E	PCN 1	12021402 18100162004	DMSP35		PGTW
52	100946	12.4W 140.2E	PCN 6		DMSP37		RODN
53	100846	12.24 140.9E	PCN 6		DMSP37		PGTW
54 55	101317	12.20 140.4E 12.20 140.1E	PCN 2		DWSPRA		PGTW PGTW
56	102127	12.3N 139.3E	PON I	T4.0/4.5 /WO.5/19HRS	DM4P37		RPMK
57	102127	12.3N 139.3E	PCN 2	T3.5/3.5 /50.0/23HRs	Dusp 17		PGTW
58	102536	12.3N 139.1E	PON 2		DMCPTA		PGTW
59 60	110159	12.7N 13A.7E 12.9N 13A.0E	PCN I		Dwsp34 Dwsp37		PGT# ROOM
61	111008	13.04 13A.0E	PCN I		DESPIT	CI UP	PSTW
65	111116	13.04 137.8E	PCH 2		DMERSE		PĢĪV
63	111441	13.3M 137.7E	PCN I		DMSP37		PSTU PSTU
65	112107	13.5N 137.5E 13.7N 137.4E	Pru 2		D45237		RODN
66	112518	17.4N 137.1E	PC4 2	13.5/3.5 /50.0/25HRS	DWSPRA		PETU
67	120141	14.0× 137.1E	PC4 1	T4.0/4.0 /S0.0/28HRS	Duspas		RPMK
68 69	120141	17.7N 177.1E	PCH I		Dw4P35		PGT u Remk
70	120949	14.9H 134.3E	PCN 6		045637		PGTU
71	121100	15.04 134.2E	PCN 6		DWSNIN		PGTW
72	121423	15.1N 134.4E	PCN 4		Dusp 15		POTU
73 74	122048	15.40 134.6E	PCN 5 PCN 3	73.5/2 5 /04 6/24UDa	Duspit Duspit		PGT# PGT#
• 75	120358	15.44 136.7E 16.74 137.5E	PCV 4	13.5/3.5 /50.0/26HR4	D=4937		PETE
• 76	140929	14.7N 137.6E	Pry 2		Duspay		HODM
• 7/ 78	171042	14.9N 137.7E	Prv 6		ひかくりょく		PGIW
, .	1 11 103	14.3M 137.4E	FF'4 B		0=7×47		PATH

• /9	172028	14.14 140.1E	PCN 6						KP17								RODN PGT#					
81	1 72325	14.14 134.6E	PC4 5	12.0/	3.0 /4	1.5/2	4HRS	D	AFYZ								PGTd					
88 88	140105	16.04 136.4E	PCN 6						4637 4637								PGT# ROD4					
84	140909	17.44 140.7E 14.24 134.4E							9977								PGT#					
45	142307	17.IN 137.1E	APCH 3	11.0/	5.0 /4	1.0/2	4HR<	D	4505								PGTW					
F14	Trac	#1X	FLT	70043	085	Max-			AFT F			dNn	ACC	.B.A	EYE	E YE.	ORIEN-	• 1	re TEI	1P (:	C)	uSN
NG.	(7)	POSTTION	LŸL	HGT	HSLP	VEL/	ARG/R	YG	n18/	VĒL/	'BH6/	, 4 MC	NAY/	ME T	SHAPE	D144/	TATION	(HIT)	/ 14/	0P/	CCT	₩O.
j	020115 021520	5.34 168.5E 6.54 167.6E	1508FT 700MH		986 984	65	180	35	770		5A0 1A0	35 30	12	?				+25	+26 ·	· 25		1
3	070053	7.24 168.0E	7 n 0 1445	>973		55		15	210	60	140	24	-	·					+16			
•	044310	7.74 168.3E	7 n 0 MH 7 n 0 MH		962 983	45 55		40	160		310 000	35 45	2	?				413	•15 ·	. 10		3
6	041523	9.54 166.2E	7 g g mtd	2931	763			-	410	54	San	40	4	5				+11	-11	-11		7
	041302	10.34 163.3E	7004H 7004H		972 969				170		100	30 30	10	3	CIRCHLAR	35			+15 ·			10
9	040529	11.54 161.0E	7 n 0 mH	2807	968	95	340	19	100	70	3+0	20	4	ř	ELLIPTICAL		010	+10	+14 4	-10		ii
10	041513	12.14 159.2E	7 n 0 m M		963				120		030 340	23		5	F1 . 7 - 7 - 6				-17	11		12
11	041427 87000B	12.24 159.0E	7n0=15 7n0=15		961				11411	<b>60</b>	300	10	*	6	ELLIPTICAL	25 13	030	+15	•15	.,,		13
13	070256	12.44 157.0E	700MH	2646	949	50	010	50	170			50		4	CIRCULAR	27		+14	-19 4	13		13
14	0714 <b>0</b> 7	12.5N 154.7E	700MH 700MH		937 930					96		24	15	٠	CIRCILAR	17		+13	-18	10		14
16	072040	12.24 157.5E	7 nomb	2477	928	100		.5	080	105	360	15	15	>	CLRCIILAR	15		+15	+24	- 10		14
17 18	0#0010 0#0247	12.2N 152.8E 12.1N 152.4E	700MH 708MH		938 935	100		50	170	115	140	10	5		CERCULAR	15		.14	.55			15 15
19	S0E in 0	17.24 149.BE	7 n 0 mH	2690	954	. , ,			120	60	040	30		-		-			.24			10
20 21	0a1508 0a2219	11.94 149.6E	7 n g m H 7 n g m H		957 964	110	250	10	330		510 390	6n	3	5	ELLIPTICAL CIRCHLAR	25 15 30	920		.53			16
55	202000	11.9N 147.4E	7 <i>0</i> 0 MH	>771	964	90	180	10	070	75	300	] n	4	ě	CIRCILAR	30		•11	+53	-10		17
23 24	000601	12.14 146.6E	700MB			95	>10		130	107	050	20						. 1	.53	. 9		16
25	091434	17.14 146.1E 17.18 144.8E	700MH 700MH	>849	974 973				140	90	040	ÌR	2	4	CIRCILLAR	35		+14	+19	-11		iy
26 27	092054	11.7N 147.6E	700MB		970	60	0 E O 0 P O	50 20	110	A7	040	3n	5	5 2	ELL[P[[CAL CIRCULAR	25 18	040		-15	10		50
58	100445	12.2N 141.8E	700MB		965 953	99	1,40	?0	350	86	280	16	=	4	CIRCILLAR	17			+19	-14		23
29	102105	12.3N 139.2E	70040		949				040	90	330	30	_		CLOCALAR				. 28	•13		23 23
30 31	111245	12.5N 13R-5E 13.3N 137-6E	700MH 700MH		943	95	160	15	180	105	100	30 15	•	,	CIRCULAR CIRCULAR	13		. 1 2	·21 ·			24
32	111530	13.3N 137.3E	71045	2563	938				090	R5	3+0	15	10	5	CIRCILLAR	10		•12	.51	• •		24
33	120104	13.9N 137.1E 14.0N 137.0E	700MH 700MH	2673	946	150		8	220	110	150	15		3	CIRCILLAR	12		•11	.55	11		25 25
35	1>1459	14.9N 136.5E	70046	>789	965		•		130	84	950	4	5	5	CLACILLAR	ln		+10	+15	-11		56
36 37	1>2013	15.1N 136.5E 15.2N 136.7E	7n0MH 7n0MH		963 961				100		360	7	10	3	CINCILAR	13		+11	-17	-11		76 76
30	130028	15.4N 13A.HE	710MH	2859		40	030	35	110	65	030	1.		,					• 23			27
39 40	170253	15.7N 136.7E	7n0=H 7n0=H		977 985	55	090	15	170		340 100	6n	•	7	CIRCULAR	1n		•14	-19	-16		28
41	111517	16.3N 137.ZE	70048	3017	989		_		040	57	580	30	5	4				+14	.58	-10		26
42	140004	14.5N 134.7E 14.1N 134.2E	700MB 700MB		1005	50 30	130 150	30 50	140	45 35	0+0 9tE	90	5	5				+14	-18	: :		29 29
							PA	749	£ 1 1 E	5												
F1X NO.	TTME: (7)	FTX POSTTION	RAUAR	ACCHY	EYF SHAP	E	EYF Dlaw		RATINE ASWAH					ď	COMMENTS			HAD Post I			<17# ##0 #0	
1	010330	1.7N 16R.2E	LAND	PoDR								þen	L CM	T#				8.7w	167.1	PE .	01366	,
2	030620	4.4N 1AA.DE	LAND	POOR								PSH	_ C#	14				8.78	167.1	TE .	01346	,
٤	030730 030830	4.3N 16A.2E 4.3N 16A.2E	LAND	FAIR FAIR									L FV						167.1		013A6	
5	074930	4.5N 164.2E	LAND	PODR								PSB	_ C=	TH				8. TA	167.1	76	41346	1
6,	011130	4.6N 164.7E	LAND LAND	POUR									L CH						167.1		91346	
ś	012230 040130	9.14 167.7E	LAND	POR														8. /~	167.1	7€	91 346	,
•	040530	9.44 167.6E	LAND	POR								PSA	C.	TH				8,7≃	167.1	'E	91 346	
10	040730 040500	9.4N 167.AE 9.4N 167.5E	LAND	6200 6200									L #Y					8.7W	167.1	rE	91356	
15	040830	9.54 107.5E	LAND	610D 610D								PEB	ĹFY	F				6. 7w	167.7	re .	91 346	1
19	040900	9.54 167.2E 9.54 167.1E	LAND	FAIR									L FY					6.7M	16 '- 7	, ,	41 3VP	
15	041000	9.5N 167.1E	LAND	FAIR								PCH	L FY	F				8.74	16"	re .	91 366	,
16 17	041100	9.5% 166.9E	LAND	POUR POUR									r					8. 7W	167.1	, E	91 746	
18	000435	17.3N 14K.ME	LAVO	POJR								WAL	L n	n <b>Y</b> 5	30F-44E			13.60	146-1	Æ	91216	ı
20	090510 090535	12.30 144.7E	LAND	POUR POUR														3.64	144.1	YE HE	41718	1
21	090610	12.3N 144.5E	LAND	POUH								WAL	ר ע	n vs	58L S#-M			3,64			41718	

55	090535	12.24 146.4E	LAND	POUR		WALL CLA VSGL SOU-N	13.64 144.9E	91516
23	090705	12.30 14A.3E	LAND	POOR		HALL CIR VSOL SSW-MINE	13.60 146.9E	
24	000735			PODH		MALL CIN VSOL SSW-W		01510
25	090505	12.44 144.2E		POR			13.60 144.9E	01510
						MALL FIR VSOL SSU-NNW	13.60 140.9E	41518
26	094935	12.34 145.82		FAIR		MALL (IN SSM-MME	13.60 144.9E	415(4
51		17.74 145.8E		PADR		WALL FIR W-N	13.60 144.9E	01718
26	090935	17.44 145.7E	LAND	FAIR		WALL FLO SW-N	13.60 144.95	91510
54	001010	12.44 145.7E	LAND	PODH		WALL CLD SSU-N-ME	13.00 100.9E	
30				FAIR		WALL CLO SON-ME		91518
31		17.44 145.5E		FAIR			13,64 144.98	91218
						WALL FLO S-MOR-NE	13.64 144.9E	91518
32		12,3N 145.3£		FAIH		WALL CLO S-N	13.60 140.9€	9[716
ود		12.74 145.3E		GAUD		BALL SSH-MME	13.00 144.96	91714
3+	0a1235	12,30 145.28	LAVO	FAIN		WALL 4-MW	13.64 144.9E	91718
35	001310	12,74 145.08	LAND	GADU	>0	GAGO CIR WALL CLO OPEN E-ESH	13.40 144.96	41210
36	091335			6000	20	GOOD CIR WALL CLD OPEN ENE-S-SH		
37		17. 34 144.8E		FAIN	711		13.64 144.9E	01514
						HVY ATTENUATION	13,6m 144.9f	91518
38		12.44 144.7E		FAIH		MAA TELMITION	13.00 144.9€	91716
3₩		12,44 144.7E		FAIH		HVY ATTFINIATION	13,00 140.46	91718
* U	091535	12.44 144.6E	LAND	FAIR		HUY ATTENUATION	13.00 144.95	91718
41	01510	12.44 144.5E	LAND	FAIR		HUY ATTEMUATION	13.00 100.95	91216
		12.30 144.4E		FAIR		HUY ATTENUATION	13.00 144.45	01218

# TYPHOOM BESS

FIA NU.	T145 (7)	F13	aCrRY	UVJPAK COUE	SATELL TIL	C344FNTS		SITE		
	•			2.7.2.						
į	141107	7.04  48.5E	PC4 5	TU-0/0.0	ひゅぐり えか	INI JOS		PGT# PGT#		
j	146313	10.0M 145.8E	Pry 6	11.5/1.5 /71.5/23HRs		1411 242		PGTH		
•	191157	10.54 142.5E	PCV 0		AF 4PMO			PGTM		
>	131306	10.54 143.0E	Pru b		DHENJE			PGTW		
•	102103	10.40 147.HE	PC4 6	12.5/2.5 /01.0/22HRC	0 MSP 16			PGTW		
	200108	10.4N 107.1E	Pru 5 Pru 5		Dada je Dada iv			PGT# PGT#		
Ţ	200148	11.24 142.2F	Prus	11.5/1.5.	Dreh 12	INII JOS		RPMK		
10	200943	10.54 140.1E	PC4 6		045011	• • • •		PGTW		
11	201140	11.44 130.4E	PC4 5		DRZh 3v			PGTd		
12	501430	11.24 130.HE	Pry n		Dachig			PGTW		
13	202043	11.04 13H.9E	Pry 6 Pry 3	-4 + -3 + 4113 A -2 E 1414	Dachie			PGT# PGT#		
15	214130	11.40 139.6E	Pry 4	73.5/3.5 /H1.0/25HRS	Dwen su			PGT		
16	210130	11.3M 138.4E	Pry 3	12.5/2.5./01.0/24HRS				RPHK		
17	210723	17.44 137.4E	Prv 4		DMENSI			PGfW		
16	210924	17.14   17.3E	PC4 •		DMCP37			RODN		
19	211155	12.74 1 17.3E	Prw 4 Prw 3		ひゃくちょう			PGTd		
20 21	211011	13.34 136.7E	PCN 6		044544			PGTH		
22	220004	11.4N 135.4E	Pru	T4.0/4.0 /00.5/25HHS				PGT		
23	220115	11. 20 135. HE	Prv .	, , , , , , , , , , , , , , , , , , , ,	DHSP35			PGT		
24	220115	13. PN 134.3E	PC4 3	t3.5/3.5	ひゃんり ゴイ	INII JOS		RUDY		
25	2>110+	14.44 134.0E	PCH L		ひゃくちょう			PGT#		
26 21	2>13>3	15.04 135.1E	Pry 3		Dach su Dach su			PGTW WTaq		
28	225144	15.4N 174.9E	Pry 2	14.0/4.0 /50.0/27HRS				PGTe		
24	222346	14.04 134.4E	Pru I	100.00000000000000000000000000000000000	Duch tv			PGTW		
30	214235	14.54 134.4E	Prw 1		Dadh 12			PGT		
31	210532	14.34 135.1F	PCN I	14.0/4.0	Dachit	SEC IINS		PGTW		
5£	231052	17.30 135.7E	Pow 1 Pow 1		D446 11			PGT# PGT#		
34	922122 922122	14.IN 134.3E	PCN		DMCD3V			RKSO		
35	231517	17.94 136.4E	Prv 1		Dusp 15			HPMK		
36	116115	14.14 116.5E	Prw 2		Dech 34			PGI		
3/	212125	14.14 137.7E		T3.5/4.0 /WU.5/24HKS				PGI#		
38	212328	14.34 117.4E	PC4 •		D=<634			PGTd		
40	240516	19.9N 13R.5E	PCV 3 PCV 5	13-0/4-0-/#2-0/24HR				PG TH HPMK		
41	247511	14.9N 13A.5E	Pru 5	13.0/3.0	D#50 15	INII JOS		RKSD		
42	241905	21.20 Jan.1E	Pru >		DUSP 17	CL DOWN		PGT#		
4.3	241005	54.34 Tec-0E	Prw 5		Dadhil			RKSO		
44	541510	21.34 Len.HE	Pry 5		Dw2b 34			PG i w		
• 46	242104	21.54 141.3E		T1.5/2.5 /47.0/24HRS				PGTd		
. 47		21.24 145.1E		11.5/2.5-/W1.5/19HRS	Duco 17			RKSO		
				•	13Cuaff F	RES				
FIA NO.	TTME (7)	0051110m	FLT	70044 185 MAX-SEC- MUT MSLP VEL/4RG/		FI-FAF-MAD WANN		VE ORIEN-	UNITY THE DEVICE	40.
						•-				
	445005	10.50 141.1E	15agF1	1005 35 100	40 060	50 300 4n 2	٠		.74 .25 +23 .25	1
Š	200330	10.74 160.ME	70046	1005 /5 .00	••					ī
3	てっしゅうち	10.54 140.3E	70040	1064 1001 30 050	50 130	30 U50 12n 5 1			*14 *15	2
•	201500	10.44 130.ME	70040	2001 1015	740 740	23 160 6n 5 1				s
,	2n1433 2n0213	11.94 139.5E	7 <i>00</i> 45 7 <b>00</b> 48	7090 1004 703> 944 35 740		32 310 30 4 1 46 340 54 4			•10 •11 •11 •11 •11	4
7	211500	13.14 134.1E	71040	2470 487	170		S CINCULAR 30		-14 -13 -12	,
	211744	11.34 135.8€	Toumm	2945 384					-	,
9	212006	13.34 135.0E	7npm8	292> 9M1	220		5 CIRCULAR 30		+14 +15 +11	5
10	5>0350	14.44 135.0E	70040	2812 969 75 090	30 1AB			10 360	+14 +17	7
11	210025	14.24 134.6E	7004H 7004H	2764 963 55 130 2731 959 90 120			? CIRCULAR 3n ? CIRCULAR 2n		· 1 · 6 · · · · · · · · · · · · · · · ·	ÿ
13	210935	17.44 135.4E	71040	2/47 961 78 140			CIRCILLAR 22		+1# +21	ý
14	211342	14.94 134.9E	7 namb	2841 972	190	43 170 Su			-	10
i s	535155	19.14 137.36	7 n B M M	2867 974 120 270	15 230 1	10 2JU H 7			*14 *54 * 4	10
10	244616	20.44   30.2E	700mm 700mm	2474 389 110 310 2479 990 100 310		20 160 lm 2 4			. # -15 +10	11
• •	240737	511.44 134.0E		>>> 990 100 110	10	de tie tu bu	••			• • •
				•	4)4u F176	i				
	TYME	FIY	usBr = :	EYF EYF			CAMMEN**		MADAR CIT	
<b>40.</b>	(7)	PRS1 110+1	HPDA9 A	CCHY SHAPE DIA	M MEMAN	TOUPF	COMMENTS		POSTTION WO	<del>-</del> 0.

13.14 137.3E NAMY

1 21,1200 12.70 134.4E SHIP GOOD

### TYPHOON CECIL

### SATELL LIP FIRES

FIA NU.	T14E (7)	FTX POSTTION	*CCRY	BUDS MARCAD	SATELL 17E	CJ446NTS	51 °E
1	0 > 6 5 2 5	1.04 147.6E	Pry 5	TH.0/0.0	0m2n 1v	1411 345	Pula
į	046399	3.64 167.AE	PCY N	TU.0/0.0 /50.0/25HR4	DESPIA		PGTH
٠	0 0 2 3 3 1	4.14 141.75	Pry 6	11.0/1.U /01.0/24HR	DMEN IV		PG Tel
•	101212	6.34 100.0E	PCV	11.5/1.5 /00.5/24HR			Pole
	110910	A. GN   JR. ME	PC4 h		Onch 11		PGTd
	110911	4. DH 1 30. 3E	Pry b		DMZN 17	INTO 342 STOOM ON EDUE OF DATA	PGI#
8	111155	4.3N 13A.5E	Pru b		0045614		2614
10	111434	5.44 139.4E	Pry n	_	044614	1411 Je2	RPMK
15	112151	7.84 137.6E 7.84 137.4E	Pry 5	43.013.0 101.3/5 HH	, () WSP 37 DWSP 34		PGT#
13	120134	7.94 134.1E	Pru 5	T3.0/3.0	Dechar	INII Jas	RODA
1.	120134	7.14 176.ME	Pry 5		Dachis		PGI#
1 >	120135	4.74 13n.6E 4.74 135.7E	Pry 5	t3.n/1.0.	044634	[NII JOS	PGT#
17	121416	7.04 135.ME	Pry 5		Darn te		RODA
18	122131	7.14 1 14 6E	Pry 5	T3.0/7.0 /57.0/24HH	Decesa Decesa		PG Ter
50 1 4	1 20 0 20	7.64 134.5E 7.64 136.4E	Pry 3		Daza 17		PGTu
21	141011	7.94 177.ME	Pry n		045037		PGTE
55	131114	HAIN THRAFE	PCN 6		Dechar		PGT# PGT#
24 24	131357	4.24 [17.2F 4.14 [17.2E	PCN 5		0 4 4 5 4		RODY
23	111158	4.3M 137.4E	PCS 5		Dadnar		RPMK
26	132111	4. 14 132.28	PCNS		DMCU 47		PGT
27 28	1.0002	4.14 (41.5E 4.64 (31.1E	Pry J	13.5/3.5 ///0.5/25MM	Dade ir	INII Jas	ROUN
24	140239	4.14 131.1E	PCY 1		Dech 14		PGIW
30	140539	7.2N 141.1E	Pry 3	13.5/3.5	0=4434	INTI JOS	RPMK
31 32	140952	4.64 124.4E 4.64 124.2E	Pry n		Dec 24		PGT#
ii.	101520	3,64 1/0.HE	PCV 0		Dadn se		PGT
34	141521	4.50 128.6E	Pry 5		Dadn 1r		RODA
35 36	142533	4,54 124.6E 1,24 124.0E	Pry 1	T4.5/4.5+/')1.0/23HR	Darnir		HPMK PGT w
31	142344	1.44 127.5F	Prvi	149374.347 71.072 444	DUSPIA		PGT
36	140551	1.7. 127.0E	PCM I		Dave se		PGTH
39 88	150521	1.4N 127.1E	Pry i	14.5/4.5-/91.0/24HR	0 M S D 2 7	SPLIT PACE	RPMX PGJ#
•1	141552	14.74 1/5.66	Pry 1		Dark se	3-11-444	PGT
42	151502	11.5" 124./E	Pry L		Dacn 14		PGT
43	141305	11.54 1/4.78	PCV 3	** ** * /-0 */3. Whi	Dece 1-		4004 FGT#
45	125513	11.94 127.5E	Pry	14.0/4.5 /e0.5/24HR9 7416-7/20 0.41-5/20	044631		RPMK
46	140503	12.00 123.0E	Pry 1	T4.0/4.0	Dazh 12	IN[1 385	RODY
47	140503	12.14 121.0E	Pry 3 Pry 5		0445 tr		PG1 a
49	141053	11.44 127.0F 12.74 122.4E	PCN 4		D=4511		PGT
50	141053	12.34 122.5E	PC4 /		005017		RODY
51	141053	12.44 122.55	Pry 3		Darbit		RP4R PGT#
52 53	141666	12.74 122.2E	PCN		0=5+15		ROUN
54	141444	12.7m 122.0E	PCY 1		OHEN 12		PGlw
55 56	144153	12.44 171.46	PCV 1	14-0/4-0 /50-0/2-HR			PG T at
51	142153 170050	12.9N 122.UE 12.4N 122.3E	Pru I	T4.5/4.5 /01.5/27HHG	Dachiv		ROUN
56	170326	11.20 122.7E	PCM I		Dach te		RPMK
59	171033	[1.44 172.36	PCH I		DWSP17		PG I M
60	171033	13.74 122.5E	PCH Z		Decriv		AODA
62	171426	17.94 127.4E	PCM 1		じゅぐち ナイ		PGIW
63	171508	14.14 122.4E	Pry I		Decn 12		ROD4
65	171608	17.74 122.3E 14,74 122.8E	Prys		D=<+11	N/A UJA TO TERMINATOR	PGTM
66	144032	14.5N 177.1E	PCH 3	14.5/3.5 /41.5/26HH	DAZASA		PGTW
67 68	140306	14.4N 127.7E	Pry 3	T3.0/4.0./41.5/30HR	Duchia		RPMK ROJN
69	141013	14.54 121.2E	PCH 3	13.0/4.0 /W1.5/26HR	045517		PGTW
70	141314	14.74 127.7E	PC4 5		DHED 14		RODY
71	101549	15.74 124.6E	PC4 5		Daza 14		RPHK RODN
72 73	100014	15.54 174.7E	Pre 3	13.5/3.5 /01.0/24HR			PGTW
74	1 90 24 9	17.1N 124.2E	Pry s	T3.0/7.0 /50.0/24HR	Dadhid		RPM
75 74	190249	17.24 125.76	PCM 6		D#25.11	C1 5A4e	PGT w
76 77	191531	17.7N 124.5E	Pru 6		044534	Ge de la	RODY
78	101531	14.3W 127.6E	Pry b		045045	****	PGTW
79 80	192357	21.14 120.0E	PC4 5	T2.5/2.5 T3.0/3.5 /W0.5/24HR	AF4PWG :	[NII J45	RODY PG1d
• i	500333	22.5N 172.0E	PCH 6	1 1/ 163 / WU - 3/ COME	044611	CI DOWA	PGTW
82	201538	31.4N 137.7E	PCN 5		AFGPMG		RPMK
83 84	2n1238 2n1313	27.9N 177.7E	Pry b		ひゃんちょう		PG I W
85	201313	21.74 134.5E	Pry		Dade 12		RODY
86	201513	22.9N 137.6E	PC4 6		004634	PROUSE:	PGTw
87	866242	34.4E PP.55	PON 7		Dadbar	EXPUSED ILC SYSTEM DISSTPATED	P61#

### ATRCHAFT FIXES

FIA	TIME	F11	FLT	70044			•sFC-								Eyê	EVE OHIEN-	FAE LEMB ICE	454
40.	(71	10517110	i VL	rlu t	MSLP	AFL	/ 186 /	# 4G	1114	/VEL	/ BKG /	- MAG	4AV	MF I	SH4PE	J144/TATION	OUT/ IN/ OP/SST	40.
i	102353	5.64 1 tu.75	700		1000	10	290	5	240	30	120	30		•			-11 -14 -11 -26	3
2	11414	7.14 137.0E	7 10 mm	3054	195		060	10	140	46	840	30	4	1	CERCIILAR	12	+14 +15 + B	
3	120528	4. 91. 1 14. DE	7nn∞n	3050	993	45	220	40	110	37	000	5.	A	٠,			.13 -11	5
•	120406	44 1 14.6F	7ngmm	CLUF	+95	•0	180	30	214		196	30	•	•			*14 *1* *12	5
- 3	1-2001	1.30 115.3E	7.10mm	1034	947	30	330	50		• •	ناوو	96	-	~	CINCILLAR	<b>♦</b> 0	·14 ·17 ·10	
•	140510	7.40 134.25	/nomm			50	90	5	170	35	800	30	4	,			-12 -15	7
,	1 30 30 4	7.40 137.ME	7 n g - m		74R	25	140	70	020	41	300	3^	,	•			·11 ·14 ·14	7
	176613	1.0. 131.ME	7 n g mm	2484	7114	- 0	130	20	107	78	020	24	5	4	CIRCILLAR	Su	·10 ·17 ·12	8
•	144560	4.64 1 10.3E	7.1044	2434	785	98	070	6	-	MB	074						-18 -11	9
10	140732	4 170.ME	Zogen			30	160	10	010	AH	تاوو	15	12	10	CIRCIILAR	50	·10 ·18 ·12	y
1.1	141932	3.1. 128.1E	7 n g mm						130	100	900	25					-15 -15	10
16	100197	1.04 127.4F	700=		965	100	>30	•	0.30	96	020	15		2	CIRCILAR	12	•11 •15 •11	10
1.4	しちいまうり	14.54 175.9E	7 n g mm	2400	466	90	150	8	040	90	360	14	7	3	CIRCULAR	20	01. 12. 41.	11
14	140950	17.44 172.4E	71040			50	0						5		CIRCIILAH	50		15
13	152153	17.40 177.18	7 n 0 mm						454	52	300	10	3	5	CINCILLAR	15	. 3 · 3	14
16	170344	14.29 122.35	7.00mm	2437	3R2	50	n90	10	1770	52	300	50	2	3	CINCHLAR	20	•13 <b>•</b> 12	14
17	111547	17.3× 122.4E	7 1 0 mm			50	490	8	040	50	320	24	,	2	CIRCILLAR		•11 •11	14
is	171340	10.1 + 172.FE	Ingun		776				3ልበ	50	946	10	,	-	CIRCIILAR	20	• M •10 •10	15
13	172045	14.2. 122.4E	7.048						2411	48	100	30	,	3			·1: ·10	15
24	1/2210	14.64 1/1.0E	7 1 0 40	2477		45	160	4	240	55	240	5	1	- 1	CIRCILLAR	10	• 7 •13 • B	15
21	10,747	15.2- 123.65	7ngun	3004		55	150	10	290	55	150	15	-	7			-18 -11	16
22	101355	14.4. 127.4E	7 opmis	2794	990	55	110	10	INA	Ab	110	50	4	5	CIRCULAR	30	·14 ·15 ·11	16
£ 5	1-1-10	14.5" 124.4E	70000						200	73	150	30	٩.	5			+15 + 9	17
69	106154	14.94 124.ME	7nome	1007	+89	35	240	50	300	64	244	30	5	•	CIRCULAR	25	•1# •15 • 9	17
25	190600	17.30 126.0E	70046	2994		90	040	15	2911	AG	180	15	4	4	CIRCILAR	•0	•15 • 7	18
26	130951	17.44 124.2E	7 n p wm	2404	986	75	120	25	260	70	120	24	5	R	CLRCILAR	40	413 +15 + 5	18
61	191458	27.11 107.45	7ngun	- •					080		350	10					•11 •11	19
28	194030	21.50 174.55	7-10 MM						256	80	160	· A	10	10	CIRCILAR	30	-10 -11 -11	19
24			7.044	1080	1004	50	>30	?5	260		100	50	- 5				·18 ·11 ·11	20

### DAJAU FIFES

Fia	fami:	÷11			FYF	EYF	3602=40144		HADAR	SIFF
NU.	(2)	205111	2+D42	<b>VCURA</b>	SHAPE	DIAM	ASMAN TOUFF	COMMENTS	POSTITON	WHO NO.
				•	J C		- ,,			
1	144500	11.1. 122.26	(4√0	POON	CIRCULAR	19		EvE	15.24 120.65	96327
۷	146530	11.44 121.76	LAVO	PAUM	CIRCULAR	19		SPIRAL RAND	15.24 120.68	98327
ز ز	146305	11.24 121.48	LAND	POUN	CIRCILAR	19		SPIRAL RAND	15.2W 129.6E	98327
•	しゃくりょう	14.4- 121.4F	(A·I)	PYON	CIRCHLAR	18		SPIRAL RAND	15.2₩ 120.6E	98327
•	170003	13.34 121.48	LAVO	マンつま	CIRCULAR	17		SPIRAL MAND	15.24 120.65	98327
b	していひろい	13.3~ 121.8E	(4.13	Gruu	CIRCHLAR	22		SPIHAL RAND	15.24 120.6E	98327
,	177455	11.34 122.1E	LAVD	GAUU	CIRCHLAR	13			15.2W 120.6E	98327
6	170530	11.50 127.18	L AHD	らっしい	CIRCHLAR	13		SPIRAL RAND	15.24 120.6E	98327
7	170503	11.54 122.7E	(A12)	についり	CIRCHLAR	1.			30.051 MS.61	98327
10	110530	11.46 1/2.25	LAND	ดายย	CIRCHLAR	14		SPIRAL HAND	15.24 120.6E	98327
11	170700	14.74 1774/E	LAND	らつりひ	CIRCHEA	15			15.2M 120.6E	98327
15	170730	17.44 177448	LAVO	6700	ELLIPTICAL			EAF WALE 50/12	15.2M 120.6E	98327
1 3	170905	13000 122036	( A v 7)	6700	CIRCILAR	1.6			15.2W 120.6E	98327
	170 +30	13.79 1/2.45	(A-13	FAIR	CIRCULAR	1.6			39.021 M2.6E	98 327
l o	1/1005	11.95 122.58	(A 10	6100	CIRCILAR	12			15.2m 120.6E	98327
16	174030	13.90 1/2.56	(A+t)	5100	CIRCILAR	12	101 11 23010		15.2N 120.6E	98327
	171100	11,74 177,65	1,4113				10413 73610		14.1× 123.0E	98446
10	171105	13.44 122.56	LAHO	6730	CIRCHLAR	15			15.2w 120.6E	98327
1 9	171130	11,30 122,48	LASS	FALH	CIRCILAR	,,	10004 44144	SPIRAL NVERLAY	15.24 120.66	98327
20	171500	13,74 122.78	(4.7				1860/ // //	4.184. AUE 6. 47	16.3M 120.6E	98371
21	171505	13.30 127.4F	LANS	FAIR	5 P 701 201 2	15		SPIRAL OVERLAY	15.2m 120.6E	98327 98327
53	171230	10.00 127.48	LAND	FAIR FAIR	CIRCULAR	15		SPIRA: NYERLAY SPIRA: NYERLAY	15.20 120.6E	98327
- 53	171330	14.24 127.38	LAND	FAIR	CIRCHEA	15		SPINAL NVENLAY	15.24 120.68	98327
6	171405	14.30 122.05	(4.0	POUR	CIRCULAR	14		SPIRAL OVERLAY	15.20 120.6E	98327
26	171930	14.34 122.45	(Av)	PODH	CIRCULAR	15		SPINAL OVERLAY	15.2m 120.6E	98327
21	17:500	14.35 1/2.35	(Au)	FAIH	CIRCILAR	1.5		Selda GACATA	15.24 128.68	98327
28	171232	14.3. 122.38	(A1/5	FALH	CIRCILAR	15			15.2m 120.6E	98327
24	171500	14.14 122.4E	AUD				1051/ ABIBS	EVE IND PENCENT CIRCILAR	16.3# 120.4E	98371
30	171500	14.00 122.0E	AND				10513 63614		14.1m 123.0E	98448
31	171502	14.30 122.38	LAND	PAJR	CIRCULAR			SPIRAL OVERLAT	15.2m 120.4E	98327
32	171535	10.0N 1/7.3E	LANT	POUM	CTRCHLAR			SPIRAL OVERLAT	15.2m 128.6E	98 127
23	171700	14.24 172.4E	LAND				1041/ 50304	EVF TO DEHCEN! CINCULAR	16.3m 120.6E	14680
34	171705	14.54 1/2.3E	LAND	●っり降	CIRCULAR			SPIRAL OVERLAY	15.2m 120.6E	98327
دو	171735	15,44 122.36	LAND	Page	CTRCHLAR			SULRAI NVERLAT	15.2M 120.6E	98327
j b	171400	14. 14 171.1E	( Aug		· ·		1144/ 50302	EVE ELLTHTECAL	16.3m 120.6E	98371
31	171 000	14,24 1/2,ME	LAUD				11025 40412	EVE ELLIPTICAL	14.14 123.06	98440
98	172000	14. 14 171.28	(AND				1174/ 30404	EVE TO DOT ELLIPTICAL	16.3W 128.6E	1 <f80< td=""></f80<>
34	112000	11,10 122.98	LAV)				//// 4041U		14.1m 123.0E	98448
**	172500	14,50 121.48	į A·+D				10472 50308	EVE AN PCT CINCULAR OPFW Se	16.3W 128.6E	98321
• 1	116600	14.84 127.8E	LAVO				11337 40517	EVF Zn-29NN DIAM 100 PCT ACCRY	14.1m 123.0E	96440
46	140000	13,44 1/7.48	1847				10475 40300	EVE ON PCT CINCULAR OPFN SU	16.3m 128.6E	146.80
• 1	1-0000	14,54 177,48	(ANO				woild trans	EVE BFCOMING LARGER	14.14 123.0E	98449
• •	140100	しきゅうし トノフェルモ					20411 43618		14.14 123.06	98448
4 >	100500	16,44 127.4E					21A1/ 6000U	EVE SO OCI ELLIPTICAL OPEN SU	30.051 mE.01	48 171
• 6	145500	14.44 177.3E					50443 V0317	EAL CINCINTUM CHEM	14.IM 123.0E	98440
47	100 100	14.44 123.25	(44.)				22444 50213		14.1m 123.0E	98440
4 8	1 40 300	14.74 177.5E					2141/ 50602		16.3N 120.6E	96321
4.9	141000	14,50 127.AE					204// ////	EVE SO PCT CINCULAR OPFN E	10.34 120.68	94371
50	141200	17.94 121.AE					22414 7361U	EAL ODEN EFFILLEF	14.14 123.06	98446
51	1-1400	15,44 1/1.48	1 4-17				25/// /////		16.34 170.66	48321

# TROPICAL STORM DOT

## SATELLITY FARES

FIA	TIME	FTX	_				
40.	(2)	20\$1110m	ACCRY	DAUSAK COUE	SATFILITE	CUMMENTS	SITE
	052235	4.04 147.7E	PCN 5	T0.0/0.0	DMEDEN	INII Jus	PSTW
• 5	041116	4.24 142.3E	PC4 5		DWZDSY		PGTW
3	715520	4.24 147.66	Pry 5	T0.0/0.0 /S0.0/24HRS			PGT#
,	0213B	5,50 139.0E	PCN 5	TU.0/0.0 /50.0/23HR	DWZDJY DWZDJY		PGT# PGT#
	092323	5.04 134.1E	Prys	11.0/1.0 /D1.0/25HRS			PGTW
7	090147	4.14 134.0E	Pry 5	12107120 7.7.207	DWED 15		PGTW
Ħ	090958	4.2N 137.4E	PC4 6		D45437		PGT
9	001500	7.24 134.2E	PC4 5		DMEDIA		PGT#
10	001458	7.4N 137.7E	PCN P		DRABSE		PGT#
11	092058 092305	7.3N 137.KE 7.94 131.7E	PCN 5		DW4634	NOT AVAIL EDGE OF DATA NOT AVAIL EDGE OF DATA	PGT# PGT#
13	100129	7.44 131.6E	PCN 5		045035	NUI AVAIL EDRE OF DATA	PATH
• 14	100310	9.1N 130.0E	PCN 5	11.5/1.5	Duspas	INII Jas	RPMK
Ē	100938	8.5N 129.8E	PC4 0		DUSPET	• • • •	PGTW
16	in1146	9.94 129.1E	PCN 0		DWGD 34		PGT
17	101410	9.9N   ?A.7E	P(N >		Dreco se		PGTd
1 11	101411	H. 94 127-6E	PCN D		Dade se		RODM
19 20	104519	9. 3N 126.1E	PCN	-3	Traped:	N/A OVER LAND	PGTW
21	110029	9.9N 125.7E	PCN 5	12.5/2.5-/D1.0/19HRs	DAZASA	N/A UVER LAND	RPMK PGT#
22	110252	4.4N 125.5E	PCN 3		CHENSA	N/A UFER LAND	PGTH
23	110525	4.5N 125.5E	PCN 3		DUSURS	The state of the s	RPMK
24	111057	9.94 127.6E	Pry 6		DUSPIT		RPMK
25	111100	10.04 172.0E	PCM 6		045937		RODN
26	111310	9.9N 127.9E	PC4 6		Dadnsv		RPMK
27	111533	10.1N 122.ME	PCH 5		046534		RPMK
5A 5R	111534	9.74 122.1E	Pry 5		Dusp 35 Dusp 37	N/A UJE TO TERMINATOR	ROUN PGTW
* 30	112159	10.64 127.4E	PCN 5	11.5/2.5./V1.0/24HR		AND USE TO THE THE TOTAL	RPHK
31	120011	10.7N 121.5E	PCN 5	71.5/1.5	Dachie		PGTW
• 32	120234	10.94 121.2E	PCH 5		DACRAC		PGTd
• 33	121039	11.5N 119.2E	PC4 6		びゃくわるる		PGTW
34	1>1040	10.54 120.4E	PCV		DACES		RODN
35 36	121252	10.74 120.18	PCN 5		ひゃくちょく		PGTW
37	121515	11.74   19.6E	PCN 5		DAZBIT		PGT# ROD4
36	122139	12.14 119.4E	PCN 5		DACHSV	N/A DJE TO TERMINATOR	PGTW
39	122139	17.14 119.7E	PCN 5		DUCUIT	-	RPMK
40	122353	12.04 119.8E	PCN 5	T3-9/3-0+	DUSPIK		RODY
41	122353	12-14 119-68	PCN >	12-0/2.0 /D0.5/24MR	DWGDJY		PGTW
42	140215	12.24 119.9E	Pcy 3 Pcy 3		Dada 12		RODN
43	110215	12.34 114.8E	PCW 3 PCW +		DUCU IN	CI UP BANDING FYE	PGT# PGT#
45	171020	13.14 119.5E	PCV		DMSP 17	C. D. BED MILLE	SPAK
46	141535	17.14 114.6E	PCN L		Dachar	CI UP MARGED FYF	PGTW
47	131457	13.5N 119.5E	PCN 3		Dace 12	EYE MAJGEU	PGT#
48	111457	15.30 110.3E	Pru 3		Dec 12		RPMK
49 50	132300	13.7N 120.1E	PCN 3	-3	D44017		SPMK
51	140117	14.20 120.1E	Pry 3	12.5/3.0-/WN.5/24HR	DAZESA		RODN
52	140117	14.0v 120.3E	Prys	T1.5/1.5.	Dachte	INII JOS	RPMK
53	140339	13.94 120.JE	Pry 5		045035	- · · ·	ROUN
54	143337	13.9N 120.3E	PCN >		こまれた まよ		RPMK
55	141000	14.1% 120.6E	Pry +		044651		PGTW
56	141000	14.00 120.6E	Pry 6		344937		RPMK
57 58	141217	14.04 121.15	Pry 5		Dadeste Dadeste	PSHL SECONDARY 14.0N 119.7E	RODN
5+	141617	14.7v 121.0E	BC# 2		044617	SECUMDARY AT 14.5N 141.0E	PGT# PGT#
60	141439	13.94 121.0E	Pry 5		Dachia		RPMK
61	142240	15.24 122.5E	Pry n	TU.0/1.0-/=1.5/23HR	Ducezi		RPHK
62	142541	15.14 122.3E	Prwh	T1.0/2.0 /41.5/24HRS	0w5037		RODM
63	150059	15.30 122.08	Pry		Drien te		RODN
64	150320	15.2N 122.7E	Pru >	*1 0/1 2./80 2/3/55	044014 044015		RODY
66	151121	14.24 127.98	Pru 3	T1.0/1.5+/#0.5/264HC	Dadaii		RPMK
67	151159	14.74 127.9E	Pry		DMSP3A		PGTW
. 68	151159	15.64 127.HE	PCN		DUSP IA		RODN
69	151420	14.64 174.5E	PCV 0		Ducuse		PGT#
• 70	125550	14.9N 174.1E	PCN N	T1.1/1.0	DWSP37	INII JUS	PGTW
71	140941	14.94 124.4E	PCNS	T1.0/1.0 /50.0/24MR	AF 42WD		ROUN

### ATACHAFI FIXES

	T T M S (7)	€14 205111 M	F∟T 1 <b>V</b> L		DRS MSLP										EYE SH476			HIEN- ATION			EMP (C) / JP/55T	40.
• 2	130503	11.24 120.5E	700MH	11105					240	30	150	50	1	7					. 4	•15	•10	•
		13.5N 120.0E	7n0MM 7n0MM			15	340	30	020 110						ELLIPTICAL	31	20	360	.15	•15	+10	6
		13.4N 120.5E							750 210						ELLIPTICAL	3 n	>0	360	. 4		+15	6 8
1	1-6535	17.4H 125.5E	7 n 0 MH	3127	1004	25	140	<b>\$0</b>	160	28	240	30	1 n	H					-11	+11	• 9	6

### PAJAH FITES

F14	118E (7)	F14 205111:00-	FAUAR	aCc4Y	EYF SHAPE	EYF DIAM	MAININ-COUE	COMMENTS	RADER Postfiow	SITE WWO WO.
i	136533	13.74 120.1F	CIAAJ	POUR	CIRCULAR	21		PSHL CENTER	15.2N 120.6E	98327
2	132303	13.44 120.1E	LAND	POUK	CTRCHLAR	20			15.2N 120.6E	98327
3	134330	11.4N 120.1E	LAND	POR	CIRCULAR	20			15.2N 120.6E	98327
	140033	13.44 120.2E	LAHO	FAIH	CIRCILAR	20			15.24 120.6E	98327
2	140105	13.9N 120.2E	LA IO	FAIR	CIRCULAR	25		CHIR STHRY SINCE LAST REPORT	15.2M 120.6E	98327
5	140135	13.44 124.3E	LAHO	FAIR	CIRCULAR	25		- <del>-</del>	15.24 120.6E	98327
- 7	140205	13. AN 120.2E	EAHO	FAIR	CIRCULAR	25			15.2₩ 120.6E	98327
- 5	140235	13.94 120.3E	LAND	FAIR	CTRCULAR	25			15.2≈ 120.6€	98327
4	140305	13. 3N 129.3E	LAND	FAIH	CTRCHLAR	25			15.24 120.6E	98327
Lυ	140410	13.9N 170.6E	LAND	ცემმ	CIRCULAR	25			15.2W 120.6E	98327
11	144432	14.0M 120.7E	LAND	5200	CIRCULAR	25			15.2N 120.6E	98327
15	142346	14.5M 121.8E	CVAJ	POUR	CTRCULAR			EYE DIAM UNK	15.24 120.6E	98327

### SYNDOTIC FIXES

FIA NO.	T 1:45 (7)	F14 20511100	INTENSITY ESTIMATE	VF4REST Data (NM)	COMMENIS
1	141500	20.04 129.0E	25	120	
2	170000	22.34 131.0E	25	50	
و	171200	27. NN 140.5E	25	60	

### TROPICAL DEPRESSION 05

# SATELLITE FEXES

FIX NU.	TTME (7)	POSITION FIX	ACCRY	DVDRAK CODE	SATFII TTE	COMMENTS	SITE
1	210311	19.3v 114.2E	PCN 5	71.5/1.5	DMSP35	INIT Des	RPMK
ž	220035	21.44 118.0E	PCN 3	71.0/1.0	DMSP36	INIT DES	PGTW
3	220253	21.4N 11A.3E	PCN 3	T1.5/1.5 /50.0/24HRS	DMSP35		RPMK
•	2>0253	22.14 119.5E	PC4 3	11.5/1.5	DMSP35	INIT JOS	RODN
ف	230018	28.0N 124.8E	PCN 3	12.5/2.5-/01.5/24HR	DMSP36		PGTW
5	220235	22.24 125.3E	PCN 4	, == 3,,, • 5	DMSP35		PGTW
ĭ	230235	22.0M 125.5E	PCN 3	T2.5/2.5 /01.0/24HR	DMSP35		RODN
	231022	27.5M 124.0E	PCN 3		DMSP37		PGT₩
ÿ	231022	30.451 WT.55	PCN 3		DMSP 17		RKSO
10	211259	30.05 NP.55	PCN 3		DMSP76	PSN BASED ON CR BANDS	PGTW
ii	211516	22.94 129.7E	PCN 5		Daspas		RODN
12	231516	23.24 129.8E	PCN 5		DMSP37		PGTW
وز	232121	24.1N 132.0E	PCN 5	T1.5/2.5 /#1.0/21HR	CF42HQ =		PGTW
14	232121	24.4N 137.5E	PCN 5	T2.0/2.0	DMSP37	INIT DESCUPR IVL	RPMK
15	240000	24.94 132.7E	PCN 5		DMCDJA		PGTW
16	240216	25.4M 137.1E	PCN J		DMSP35		PGTW
17	240216	25. IN 133.8E	PCN 3	Tl-n/1.0	DUSPRS	INI 345	RKSO
10	241000	27.7N 136.0E	PCN 5	*	DMCP37		PGTW
19	241002	29.04 135.7E	PCN >		DWSP37		RODN
20	241005	27.1N 136.0E	PCN 5		DMC037		RKSO

### RAJAR FIXES

FIX NO.	T 4E ( ·)	FTX POSTTTON	PADAR	ACCHY	EYF SHAPE	EYF Diam	RAHING-CODE ASMAR TOUFF	COMMENTS	MADAR Postitom	SITE
3 4 5 6 7 8 7	210200 210600 210600 210500 210500 210500 210500 210700 210800	72.24 125.1E 72.24 175.1E 72.34 175.7E 72.34 125.7E 72.44 126.0E 72.44 126.0E 72.44 126.0E 72.45 126.0E 72.46 126.0E 72.56 126.0E	LAND LAND LAND LAND LAND LAND LAND LAND				21822 50511 10823 50716 21812 50914 20042 50812 10872 50816 35/41 50819 22012 50814 20781 50911 24842 50822 24811 50816 3/// 40522		24,8M 125.3E 24,8M 125.3E	67927 47918 47927 47918 47927 47927 47927 47927

### SYNDOTIC FIRES

FIX	T+ME	502111041	INTENSITY	NEAREST	COMMENIS
NO.	(7)	E1A	ESTIMATE	DATA (NM)	
		19.00 114.0E 20.00 115.0E	15 15	60 60	

### TYPHOON ELLIS

### SATELL ITE FIXES

_							
FIX	TIME	FTX		242-14 -000	54TF1111E	CJAMENTS	SITE
w.	(7)	POSTTION	ACCRY	DADSWK CODE	361711116	C 3 - MP - 4   3	3,10
1	240010	5. PN 130.3E	PC4 5	10-0/0-0	DMSP 3A	INI 1 JOS	PGTW
5	241119	9.04 141.7E	PCN 5		DMCD34		PG Tur
3	241441	A.94 139.0E	PCM 6		DMCD34	POSSIBLE SECONDARY 19.8N 139.4E	PGTW
•	270001	9.04 140.4E	PCN 6	TU-0/0.0 /50.0/24HR4	Duspis	LOSSING SECTIONAL LABOR 124145	PGTW
5	270200 270 <b>84</b> 7	A.74 140.3E A.64 139.5E	PCN 5		DHSP37		PGT
7	271102	8.7N 139.4E	PCN 6		DHSP3A		PGT#
è	272128	11.3N 13R.9E	PCN 6		Dach 11		PGTW
9	272343	11.44 13A.7E	PCN 5		DACRIV		PGTd
10	141025	11.44 13A.6E	PCN 5		Ducest		PGT# PGT#
11	SW1008	12.IN 13A.4E	PC4 6		Duspar		PGT
12	241525	12.94 13R.6E	PCN 6		Duceah		PGTW
14	245352	12.54 134.0E	PCN >	TU.0/0.0 /50.0/24HRS			PGT
15	291508	12.9N 137.6E	PCN 6	1210/1100	DMCH3W		PGT#
16	292307	11.74 135.2E	PCN 5	T0.0/0.0 /50.0/24HKS	Decnse		PGTW
17	3n1150	13.74 132.6E			DACHAY		PGTd
18	3n1346	13.9v 13>.3E	PC4 6		DMSP 45		PGT#
19	302208	13.74 132.7E	PCN 5	11.0/1.0 /D1.0/23HRC	ひゃくりょく		PGTd
50	010031	13.54 137.48	Pru b		Duspas		PGTW
55	010227	13.2N 131.5E	PCN 5	T2.0/2.0	Duspas	INII DAS	RPMK
23	011050	13.7N 131.0E	Pru 5		DMSP37	CI UP	PGT#
24	011050	13.8N 130.9E	PCN 6		Duspit	UPR LVG NUTFI NO	RODY
25	011313	13.94 130.7E	PCN 6		Dade sv		PGTW
56	011313	13.7N 130.7E	PCN 6		DMSPRA		ROD4 PGT#
27	011509	17.94 130.2E	Pry 6		045634 045634	UPR LVL ANTI/RANDING	RPMK
29 28	012148	17.6W 130.1E	Prw 5		Duspay	Or A TAR BUILTING INC	RPMK
30	050013	14.5N 12A.4E	PCN 5	T3.0/3.0 /02.0/25HRS			PGTW
31	050137	16.4N 125.0E	PCN I	14.5/4.5 /00.5/24HRS			900N
35	020155	14.14 12A.3E	Pru 5		Owebia		RPMK
33	020508	14.54 12R.1E	Pry 3		Drebie		PGTW
34	020203	14.54 128.5E	PCN 5	_	045634	1911 345	RODN
35	0>0203	14.4W 128.1E	Pry 3	T4.0/4.0+	045P35 045P37	INII JOS CI UP	PGTW
36 37	021029	19.00 127.1E 15.10 126.6E	Prw + Prw 6		DWSPRA	C1 Or	PSTW
38	021450	15.1N 124.6E	PCV 5		DMSP35		RPHK
39	021451	15.3N 176.4E	PCN 5		Desp 15		PGTW
40	0>2128	14.44 174.0E	PCM 5		OMSP37		RPHK
41	022129	15.94 175.3E	PC4 5	T4.0/4.0 /91.0/21HRS			PGT#
42	022356	16.0W 124.0E	Pry 5	-5	DMCP3A DEGPAG		PGT# RPMK
43	030137	14.2M 124.8E	PCN B	15.0/5.0 /DZ.0/ZAHRS	Duspar		PGT
44	021537 600150	17.44 127.4E	PCW 6		DMZHJV		PGTW
46	031432	19.14 122.6E	PCN 6		DAZES		PGTM
47	031432	14.1H 123.1E	Prv 6		DMCDJS		RPMK
48	032549	19.5N 119.5E	PCN 3	T4.5/3.5 /WI.O/SIMPS	DHEPTT		ROUN
49	016549	14.74 121.5E	PC4 5	T3.0/4.0./w2.0/21HR9	CERSON		RPMK RPMK
50	040300	14.3m 120.6E	Pru 5		OMEDIA	EXPUSED ILCC	RODN
51 52	040314	19.5N 120.4E	Prw 4		DMSP14 DMSP17	ENTOUGH ILLE	RODN
53	041555	20.1N 110.0E	PCN 3		Despan		RPMK
54	041555	20.74 11R.1E	PCN 3		DMCPAH	EXPUSED FLCC NF OF DENSE CONV	RODN
55	042230	20.14 114.3E	PCH 5	73.5/3.5 /D0.5/24HR			RPMK
56	050101	30.00 114.0E	PCN 3		DMCB34		RPMK
57	050255	20.14 115.HE	5C# 1		Duch se		RPMK
58	040556	20.24 115.9E	PC4 3	T4.5/4.5-/W1.0/24HR	045945 045937		RODN RODN
59	051110	20.4N 114.3E	Prw 3		Ducp 17	EXPUSED ILCC	RPMK
61 60	051110	20.64 114.5E 20.64 117.7E	PCV 4		0=5935	WELL JEFTNED ITCC	RODN
95	051537	20.74 113.7E	PCN 3		DMSP35		RPMK
63	042210	21.74 111.AE	PC4 5		045417	N/A UJE TO TERMINATOR	PGTW
64	0 4 2 5 1 0	21.54 111.7E	Prw 5		DHSP37		RPMK
65	060045	71.5" 111.4E	PCV 5	12.5/2.5-/42.4/82HR	AFGPMQ :		RODN
66	165040	21.6% lln.0E	PCN 5		D#46 17		MK 30

### ATRCHAFT FIRES

	] tmf (7)	ETX POSTTION	FLT I VL		1 085 MSLP				014/						EYE Smape			H164-			EMP (	454	
	3.4003	11.36 1 12.45	7 n 0 m/m	1084	1000				150		040	30	_	12									
ز		11-34 112-35	70040		1000	40	270		140										•14	-15	+10	3	
		11.9N 1/9.1E	70046		984	,,,			140													•	
		14.10 124.15	70046		981	76			250						CIRCULAR						• 9	•	
					461											•			*			5	
•	020539	14.20 1/7./E	7n0M6	フロラフ					100												+12		
ь	りつりきょう	14.74 127.3F	7n04h	285a	974	50	120	>0	040	62	310	45	-	5	ELLIPTICAL	35	>5	160	-11	•17	+15	5	
,	021344	15.74 175.6E	70046	2739	971				210	74	140	60	4	×						.15	+10	6	
		15.74 175.3E	TOOMH		955	100	130	28	230	42	130	20	5	H	ELLIPTICAL	30	>0	090	-14	+17	-10	6	
		14.34 174.1E	7 n D M M		146				114									-	-		+14	7	
															F							i	
10	0 PU 546	17.34 1/1.4E	7 n 0 M H	>731	956										ELLIPTICAL	90	-0	010			-14		
11	044952	10.50 110.4E	7 n g M H	2479	984	70	100	5	200	50	100	50	2	- 1					-1-	•17		9	
		34 35	7.0.44			• • •			146		240		•	•					414	413		10	

### 04 340 FIEFS

FIX NU.	T1ME (7)	FTX POSTTION	HADAR	ACCRY	EYF SHAPE	DI 44	SENSE TOUFF	COMMENTS	MADAR Position	#40 <b>40.</b>
123 + 56 7 8 9 10 11 12 13 14	0=1330	14. W 127. ME 17.0N 124.0E 17.9N 127. TE 17.9N 127. TE 14.6N 127. TE 14.0N 127. TE 14.0N 127. TE 14.0N 127. TE 14.5N 110. TE 21.7N 115. TE 21.7N 117. TE 21.2N 117. TE	LAND LAND LAND LAND LAND LAND LAND LAND				4/// //// 41401 5/// 41411 529// 45411 52920 45411 52720 45411 52720 1001/ //// 65/// 2810 650// ////	PROBARIF LYE SPIRAL OVERLAY EVF 74 OFNCENT CIHCULAN EVE FIXEN CINCULAR DOFN NO	16.1# 123.0E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 16.3# 120.6E 22.3# 110.2E 22.3# 110.2E 22.3# 110.2E	98321 98321 98221 98221 98231 983321 983321 98365 45005

### SYMPOTTE FIXES

F1X NU.	[TME (7)	FTX POSTTIUN	INTENSTIV ESTIMATE	NEAREST TATA (NM)	COMMENIS
1	250000	7.00 141.0E	15	150	
Š	241200	7.0N 140.0E	15	120	
ۇ	270500	4.4N 134.3E	20	100	
•	200000	12.00 135.0E	15	60	BROAD F-W THOUGH
,	291500	17.04 134.5E	20	100	BROAD F-W THOUGH
6	300000	11.5H 133.5E	25	180	RRna) F-W THOUGH
1	300500	14.04 132.0E	25	150	BROAD F-W THOUGH

### TROPICAL STORM FAYE

### SATELL ITF FIXES

FLA	Tras.	FTX					
NO.	(7)	20517100	ACCRY	DAUSTR CODE	SATFILITE	COMMENTS	SITE
		• • • • • • • • • • • • • • • • • • • •					
	292307	2.0N 152.3E	PCN 5	TO 0.00	DHEBSK	INI 1 Jes	PGT#
1	301346	3.6N 151.7E	PCN 6	TU-0/0.0	DMSP35	1411 202	PGIM
2	302249	5.64 151.1E	PCN 5	T1.0/1.0 /01.0/24HRS			PGT
•	014908	5.74 150.2E	PCNO	11.0/1.0 /01.0/2404	DMSP 17	CI SAME	PGTW
ś	011132	4.1N 150.0E	PCN 6		DMZP34	· • • • • • • • • • • • • • • • • • • •	PGIM
6	011132	6.44 149.7E	PCN 6		0m5P35		PGTW
7	012007	6.34 147.3E	PCN 6		DMSP37		PGTW
έ.	012007		PON 5	-3			PGI
	020209	7.44 146.2E		12.0/2.0 /01.0/27HR	DMSP37	CI SAME	PGT
		7.8% 145.0E	PCN 6			CI SMAP	
Ιú	021114	7. AN 144. ME	PC4 5		DMSP3A		PGT# PGT#
11	021309	9.0N 144.5E	PCN 6		045035	**** ***	
15	022128	9.04 143.6E	PCN 5	T3.0/3.0	DHSP37	INII JdS	RPMK
13	0>2129	9.24 142.4E	PCV P		045037		PGTW
1+	052356	9.44 147.5E	PCN 5		Dwensy	fra. 116 - 4 = 4	PGTu
15	0.1003	9.3N 140.7E	PCN 6		DMSP37	EUGL UF NATA	PGTW
16	031055	9.74 140.3E	Prvo		DMCD34	EDGL JF NATA	PGTW
17	0.41435	10.00 130.6E	PON 6		DMSP35		PGTW
16	041435	10.00 140.1E	PCN P		DWCDJA		RPMK
19	015109	10.44 139.3E	PC4 5	T3.0/3.0 /50.0/24HRS			PGTW
50	074338	10.3N 139.3E	PCM 5		DMSP35		PGT
51	040118	10.9v 139.4E		74.0/4.0 /01.0/28HR9			RPMK
55	040132	10.5N 139.SE	PCN 3		DHEBST	EXPUSED I LCC	PGTW
23	040132	14.4N 140.SE	PCV 4	13.0/3.0	DMEBAL	INII -DOS	RODY
54	040949	10.4M 13A.7E	Pry 6		UMCD 53		PG i#
52	041519	10.64 13A.1E	PCN +		Owehdy		PG t 🙀
56	041413	10.7N 137.1E	PCH 6		045935		PGTW
21	041414	10.5N 13A.7E	PC4 >		Dades		RODN
26	04204B	10.9N 136.8E	Pry 6		DMebil	UPR LVL CHTR 10.5N 135.05	PGTW
29	042320	10.54 136.5E	PCN 5		DMebsy		PGTW
30	050114	10.34 135.9E	PCN 3	73.0/7.0 /50.0/28HRS			PGTW
31	050114	10.14 136.1E	PCN 3	T3.0/3.0 /50.0/24HRS			RODN
32	054928	11.44 135.6E	Prw 4		DM46 17	FXPOPEN I LCC	PGTW
33	051201	11.94 135.4E	Prw 4		AF4PMO	EXPUSED ILCC	PGTW
34	051355	11.9. 135.ZE	PCN A		DMSP75		RPMK
35	051355	12.04 134.9E	PCN J		DHEPTS	EXPUSED ILCC	PGTW
36	051355	12.34 L35.0E	PC4 3		DMERSE		RODN
37	052210	12.74 137.8E	PCN 3	T2.9/3.0 /W1.0/21HRS	DMSP77		PGTW
34	0=5305	13.14 133.7E	PCN 3		DMCDSY		PGTW
39	060237	13.74 133.4E	PON 3		DMSP 15		PGTW
40	165040	13.4N 137.3E	PC4 3	T2.9/3.0-/W1.0/25HR9			ROUM
+1	040709	15.0N 132.4E	PCV 6		DUSPIT		PGTw
42	051144	15,24 132.0E	Prw 4		DMCP3A		PGTw
43	041518	15.64 131.5E	Pcv +		DW46 14		PGTW
44	041517	15.6N 131.3E	PCN 3		DWSP35		RODA
45	070026	17.34 129.0E	PCN 3	TU.0/1.0 /WZ.0/26HR9	DMADSE		PGTW
46	971308	17.74 127.7E	PCN 6		DMZBJK	CI UP	PGTW
47	090008	19.64 124.4E	PCN 5	TU.0/0.0 /50.0/24HRS			PGTW
48	041250	30.2H 124.3E	PCN 5		DMCDJY		PGTw

### ATROMAFT FIXES

FIA NO.	T14E (7)	FTX POSITION	FLT LVL	70043 HGT	08S MSLP				441- 019/						EYÉ Shape	EYE ORIEN- DIAM/TATION	UNITY THE DRIVER	45N F 40.
1	012300	5.1N 146.5E	1500F1		1008													1
2	020652	7.54 145.5E	1500F1		1004	20	320	45	288	20	140	30	2	5				2
3	020945	7.5N 145.3E	ISOBE		1004	25	200	50	286	25	200	ion	-	5			+22 +23 +23 1	) 2
	021303	4.94 147.6E	700MH	3094			-		080	36	360	60		м				3
	022050	9.9H 143.8E	15ngf1	1	1001	4.0	270	15	250		270			۶			+24 +25 +25 2	7 3
6	010910	9.5N 141.6E	700MH	1084	998		270		160	55	270	40	5	7			+12 +15 + 6	•
7	014014	10.14 140.6E	70046	3065	998		170		140	46	0+0	70	- 5	4			-14 -15 -12	5
	040804	10.54 138.5E	700M8	3097	1001		180		110	55	050	50	5	5			·10 ·15 · 5	6
9	221240	10.24 135.8E	7ngmH	3033	991		170					120		3	ELLIPTICAL	5 13 090	+14 +17 + 4	7
10		11.3N 135.4E	1500F1		994		240		230		140			5			+5+ 45+ 65+	8
• 11	051925	11.4M 137.6E	700MH	3100	,,,	,,			220		150	60		5			+11 +11	9
· íż	052200	12.6W 132.3E	1500F	7.00	1004	10	180	140	230			440		10			26	9
وز	060717	13.9N 132.7E	1500FT		1001					•				-			-	11
	070534	16.0N 127.5E	700MH	1117		10	090	70	170	50	040	70		5			.34 + 6	iż

### SYMBATTE FIXES

FIA NO.	TTAE (7)	F14 P051110H	INTENSTIV ESTIMATE	NEAREST DATA (NM)	COMMENTS
1	241200	3.04 155.0E	15	150	EQUATORIAL DOUBLE-VONTICE INTERACTION
S	290000	2.5N 154.0E	į5	80	EGHATOPTAL DOUBLE-VONTICE INTERACTION
•	291200	3.04 153.5E	15	130	EST 4SIP INDBAU
	300000	3.54 153.0E	15	90	EST 4SIP 100848
5	301200	4.04 152.0E	15	150	SFC TROF N4-SE

### TROPICAL DEPRESSION 08

### CATELLITY FEXES

	(7)	POSTTION	4CCRY	DAUSTR CUDE	SATFLE TTE	COMMENTS		SITE		
• 1	202339	5.9N 134.4E		10.0/0.0	Duspak	INIT DUS CI SAME/HPR LVI		PST#		
• 2	511550	0.3N 135.5E	PCN 5		AFG2MQ AFG2MQ	Ct 3mag/med (at		PSTW		
• 3	521505	13.5× 139.8E	PCN 6	-1	OMED34	INIT JUS/LLCC 235N	14075	PETU		
•	225305	14.9M 139.6E	PCN 5	11.0/1.0	Dusp37	1411 00316501 1224		PSTU		
,	Sible	20.2N 139.4E	PCN 6		DMSP36			PSTW		
6	21144	20.3N 13R.9E	Pru 6		Duspag			PSTW		
7	2-1303	20.54 139.7E	PCN 5		DMSP35			PETW		
. 9	231328	20.54 13R.6E	PCN 5	T1.0/1.0 /50.0				PSTW		
	212245	22.6N 137.0E 22.4N 136.6E	PCH 5	1110/110 /2000	DHSP3A			PGTW		
• 10 • 11	240145	23.2N 135.1E	PCN 5		DM2b36			PSTW		
- 12	540503	23.4N 134.5E	PCN 5	T1.0/1.0	Duspas	INIT 285		RPMK		
• 13	240210	27.74 134.8E	PCN 5	1.40/100	DHEPRE			PSTM		
	240951	24.9N 134.0E	PCN 5		Duspa7			PGTW		
• 14 • 15	241244	24.9N 133.6E	PCN 6		DHEDAG			PGTW		
• 16	241307	24.9N 137.5E	PCN 6		DMSP3A			PGTW		
• 17	241451	25.2M 132.9E	PCN 5		D#46 32			PGTW		
• 18	241451	25.04 133.0E	Pru 5		DHSP15	INII 44GHTIMF NAS		ROOM		
• 19	250008	25.4N 130.9E	PCN 5	T0.0/1.0 /W1.	AFGENG PAHTS L	POSSIBLE SECONDARY	27,0m 13n.38	PGTW		
• 20	250126	26.2N 130.4E	PCN 5		Dec 6 se			PGTU		
• 21	240151	24.5N 130.1E	PCN 5		ひゃくりょく			PGTW		
• 22	240151	38. PSI NP. 25	PCN 5	T1.0/1.0	Prusma	INII D#S		RODN		
23	251226	30.7m 177.6E	PCN 5		DMCDJG			PGTM		
24	251250	30.74 127.5E	PON 5		DMZb 14			PGTW		
25	251433	30.4N 127.4E	PCN 5		045975			PGTW		
26	252350	31.5N 125.7E	PCN 5	T4+0/4+0	DMC6 14	INIT DUS		AKSO PGT <del>u</del>		
21	252350	31.94 175.5E	PON 5	12.0/2.0-/02.				PGTM		
28	240133	32.4N 125.4E	PCN 5		DMSP35			RKSO		
29	240314	32.4N 125.3E	PC4 3		Duspas			MKJU		
					AIRCRAFT (	INES				
	T = .45		FLT	70043 DBS M	AX+SFC-#40 MAX	-FLT-LVE-4ND ACCRY	EvE	EVE ORIEN-	RYF TEMP (C)	458
	TYME (7)	FTX POSTT[ON	i VL		EL/RRG/RYG OTH	VEL/BUG/HAR NAV/MFT	SHAPE (	MOITAT/WATE	OUT/ IN/ OP/SST	40.
40.	177	-05/11///	(**							
1	241016	23.1N 133.5E	700MB	7127 1004	15 110 120 150	15 000 ln 2 10			•10 • <b>3</b> • 5	1
					ZAMUSTIC EL	#E8				
F1x 40.	TTME (7)	FIX POSITION	INTENS ESTINA			COMMENTS				

# SUPER TYPHOON HOPE

	FIA		FTH					
	40.	(7)	205111(m)	*CC84	DAJSAK COUE	SATELLIE	CJMHFNTS	SITE
	ı	250151	10.5w 145.2E	Prw				
		240435	10.40 141.46	Pry	,	Dusp15	INII Jas	PGT#
	• 3	241108				AFUPPO		PGTd PGTu
	: ;	241433				Deckad		PGTW
	6	252350	11.44 Jan.HE			DMSP35 AFGPMG :		PGTW
	,	540101	11.44 140.55	PCN :	,	Decado		₽ĠĨ₩
	8	240133 240133				DHSP35		9614
	λú	540915				045435	INII Jus	PGT d RODN
	11	241501	17.04 JAN. DE			Dusp37		P574
	15	541535	17.04 130.4E	Pry e	•	044544		PGT#
	13	241414				Duspan		PGTW
	15	274048	11.30 tan.4E	PCN 5		D45632	INTO MIGHTIME OHS	PGT# RPMK
	16	270114	17.44 140.5E	PCN		Pethan Series		PGTW
	17	270114	13.4" 140.AE	Pry 1	11.0/1.0 /W1.0/24HRC	DAZES		RODN
	18	274951 272314	14.74 140.3E	Pru .		044037	EXPUSEU ILCC	PGT# PGT#
	żó	240237	14.3N 13H.OE 17.2N 137.7E	PCN 3				PGT 4
	. 51	241012	14.2M 134.5E	POND		Duspas Duspa7	B45. B	PGT#
	55	241013	17.74 137.5E	PCV 5		Dusp 17	BASED ON HOR I VE	RPHK
	• 23	241310	19.00 137-0E	Pru 6		DHENSA		PETH
	• 25	241337	36.AE1 NF.PE	PC4 5		ロミカカナ		PGTW RPMK
	26	205115	17.1N 134.2E	PCN 7		Director		PGTW
	2/	165545	14.94 135.7E	Privis		D45P37 D#5P3K		PGT
	54	240151	15.44 115.4E	PCN 5		PFSPMO	INIT Des	PGT#
	30	500513 500513	14.1N 136.7E	PCN 5		DMSP35		RPMK PGTw
	31	291138	14.54 135.18	POND	T3.0/3.0	DMSP35	INI 1 385	RODN
	35	555165	14.7× 134.9E	PCN 5		Duch se	CL UP,	PGTw
	33 34	201500	16.94 134.7E	Pru b		DMSP35		PGTW
	37	291500 3nu014	14.74 134.7E	PCN 6		DMSP35		PGTW RODW
	36	300020	16.74 137.4E	PCN 5	74.0/4.0 /NZ.0/21HRS	DHSP36		RODA
	37	361132	14.54 137.4E	PCN 3	T4.0/4.0-/01.0/24HRS	DMSP3A		PGTW
	30 30	300133	14.7H 131.3E	PCN 3		Duspag		RPMK
	46	300501	14.94 137.3E	PCN 1	14-5/4-5 /01-5/24HR4	DHSP35		PGTW RODM
	41	300932	17.0N 132.1E	Pon 2 Pon 3		D#46744 D#4677		PGT
	42	3~1233	17.74 131.6E	PCN 3		DHSP39		PGTW
	43	301301	17.4M 132.0E	PCH 3		Duspag		RODN
	43	301441	17.74 131.7E	PCN 4 PCN 1		DHSPRA		PGT# PGT#
	46	301442	17.74 131.4E	PCH 1		DMSP35		PETU
	47	304513	14.54 120.7E	PCN 1	15.5/5.5 /01.5/21HR4	DUSPRE		RKSO
	48	314005	14.5M 129.5E	PCV 3	15.0/5.0 /01.0/27HRS	DMSP37		RPHC
	50	310114	19.4N 129.3E 19.9N 129.9E	PCN 1		DMEDAY		PGTu PGTu
	5i	311153	17.3N 174.6E	PON 2		DMSP39		PGTW
		311544	19.74 125.9E	PCN 1		DMSP36		PSTY
	5.1 50	311355 311355	14.7N 125.9E	PC4 S		DMSP39		<b>P61</b> 4
	55	311423	19.7N 125.6E 19.80 125.5E	PCN 1 PCN 1		DMEBSO		RPMK ROOM
	56	311424	19,44 125.7E	PCN 1		Duspas		POTE
		312153	20.5N 127.7E	PCH 1	16.5/6.5-/01.5/24HRS	DMSP15		RODM
		312153 312153	20.54 123.7E	PCN 1	T0.5/6.5-/01.0/24HRS	DMSP37		PGTu
		312344	20.54 127.7E 20.64 127.3E	PCH I	16.5/6.5	DMSP37	INII 005	RODA
	61	010236	20.74 127.6E	PCN I		Duspak Duspag		PSTH
		010236	20.5N 122.4E	PCN 1		DESP39		RPMK
		011033 011336	21.3N 12n.6E	PCN 2		DMSP17		RODN Pala
		011336	21,44 119.5E	PCN 1 PCN 1		Duchio		Patu
	66	011335	21.54 119.5E	PCN I		Duchid Duchid		RPHK
		011408 011547	21.54   19.5E	PCN 1		DHERTA		RODN
		011547 012314	21,7H ]]R.6E 27,0N ]]7.1E	Pry 1		DHEPTE		RPMK ROOM
		070217	27.44 115.7E	PON 1 PON 1	75-5/6-5-/W1-0/24HRC	Dusp 17		RPHK
	71	7450c0	27.14 115.3E	PCN 1	T5.0/5.5-/#1.5/ZAHRS	DMEPRE		PSTH
	72 (	ロフロとキア	22.34 115.3E	PCN 1	15.0/6.0-/W1.5/29HRR	044634		PGTU
		021155 021155	27.54 117.4E	PCN 4		DHSP17		RODN RPMK
			22.74 117.1E 22.74 110.8E	PCH 4		D4SP37		ROON
	76 (	171528	27.7N 107.9E	PCH 6		Duspas Duspas		PETU
		12524	21.50 109.4E	PCN 5	T3.5/4.5-/W1.5/20HRS	Dugpar		RPHK
•	78 (	12524	27.64 10A.8E	PCN 5	12.0/2.0		INI Jes	RODN
							· · · -	mn 3-0

### ATREMATE PINES

FIX NO.	[ TME (7)	F1X POSITION	FLT I VL	70643 HGT	285 432H			\ <b>8 46</b> - # 40				- 4 MU			EYE Smape			PRIEN-		YF 1				454 40.
1	250728	10.44 144.5E	1500F1		1005	25	110	1 20	820	38	310	120	4	10						+21	,	. 3	23	
2	525113	11.20 147.4E	1540F 1	1085	1000	25	950	50	160	58	0/0	40	*	30							• • •			ż
3	244609	11.44 141.7E	7 n g m H	1081	1000			90	160	31	050	96	3	25							•			- 7
•	EIFUAS	11.90 141.3E	7ngmb	1091	1002	15	130	100	140	17	130	120	•	25					-10	• 11				ĭ
>	241430	12.34 139.8E	700mb	3090		-			230	50	300	34												- 4
•	244025	12.50 140.0E	1500F1			10	080	50	330	30	510	30	10	10							5 . 5			
7	272307	14.14 137.9E	72846	3094	999		120	15	140		140			•					412	•11			28	•
8	281933	14.74 135.7E	TORME	3052					110	41	070	120		5							•			Ä
7	242052	14.7N 135.7E	70040	3047	995	40	100	30	340		210	20	•	>					-11	• 1				
10	290715	16.6N 135.5E	700MH	2865			140	20	050		310	30	4	•					•••		• • i			,
11	290328	14.64 134.2E	7 n 0 mH	2864	972	70	130	20	130		940	30	,	1	CIRCILAR	R			.10	.11				7
15	291508	16.7 × 134.1E	71044	2/7A	965				220		110	1.0		i							• • •			
13	296031	14.4N 133.8E	70041	2745	961	90	360	30	080		360	20		ĩ	ELLIPTICAL	5	3	340	-14	-11				- 4
1.	300515	17.14 132.7E	7 1 0 MH	2556		45	090	15	170		040	15		•		•	-		•••		• • •			ü
15	300925	17.14 132.4E	700MB	2509	934		170	iż	230		170	12	•	1	ELLIPTICAL		6	160	. 12	•15				é
16	301939	14.24 130.2E	71044				>20	50	010		300	25	,	- 5	ELLIPTICAL		ě	140	• • • •		• • •			10
17	306555	14.4M 129.7E	7n0#H	2447	926	95	140	5	170	110		15	4	>	ELLIPTICAL		ě	140		.15				10
18	310649	19.34 127.6E	708MH	2327	515	95	360	50	048			15	- 5		CIRCULAR	15	•		•••		, .;			iĭ
19	310+10	19.44 124.4E	7 n c MH	>205	498	100	360	iō		147		10	-	Ś	CIRCILAR	ii			.12	.21				íi
20	312149	21.3N 127.7E	710MH	7237	902	140	110	>0	160	134	110	Žo		•	CIRCILLAR	Zn				. 20				12
51	010745	31.04 121.1E	700MH	2364	917		060	30		150		50	-		CIRCULAR	ÌA				+15				13
22	010906	21.20 120.05	7nome	>38)	970		160	20	350		240	50	4	3	CINCILLAR	16				.17				13

	TIME	FIX		04	EYF	EYF	BADOH-CODE		MADAR	41 TF
NO.	(7)	P051110N	HAUAR	ACCRY	SHAPE	DIAM	ASWAR TOUFF	COMMENTS	POSTTON	W40 40.
1	010000	20.54 123.08	LAND				315/1 ////		14.2N 122.7E	96231
5	010100	20.7N 127.9E				5			25.1m 121.6E	46496
3	010150	20.7N 122.5E	LAND				11411 53023		14,2N 122.7E	17580
4	010300	20.5N 177.2E	LAND				30751 52716		14.2W 122.7E	98731
•	010350	20.74 122.0E	LAND				30711 52914		14.2m 122.7E	15580
6	010500	20.54 122.0E	LAND			5			72.6W 120.3E	46744
7	010500	20.54 121.0E					3551 52519		14.24 122.7E	15286
	010500	20.7W 127.0E				5			24.04 121.6E	46599
4	010550	29.54 121.5E	LA-ID			4			14.2N 122.7E	16580
10	010500	20.94 121.8E	LAHO			٩.			24.UM 121.6E	46649
11	010500	30.7N 121.AE	LAND			٩.			72.64 120.3E	46744
15	010500	31.04 121.0E	LAVO			5			25.1N 121.6E	46596
13	010550	20,7N 121.3E	LAVO				74411 52912		14.2M 122.7E	98271
1.4	014700	20.9N 121.5E	LAND			4			72.64 120.3E	46744
15	010700	21.1N 121.5E	CAND			5			74.0W 121.6E	46699
16	010700	27.5N 171.6E	LAND			5			25.IN 121.6E	46696
17	010940	51.5N 151.3E	LAND			5			34.UN 121.6E	46649
18	010530	20.44 120.HE	LAVO				7//// /////	SPIRAL OVERLAY IS DEGREES	16.3M 120.6E	98321
19	010900	21.2N 121.0E	LAND			5			74.0m 121.6E	46599
20	010700	21.1N 120.2E	LAND			5			22.68 120.3E	46744
51	010400	31.74 120.4E	LAND			5			25.1N 121.6E	46696
55	010930	20.9H 120.2E	LAND				41111 11111	SPIRAL OVERLAT IS DEGREES	16.3m 120.6E	98371
23	011000	21.24 12n.4E	LAND			5		· · · · · · · · · · · · · · · · · · ·	24.0m 121.6E	46699
2+	011000	21.3N 120.7E	しきゅう			5			72.64 128.3E	46744
25	011500	21.3N 120.1E	LAND			5			22.64 128.3E	46744
26	011300	21.4N 119.7E	LAND			5			72.6N 128.3E	46744
21	011400	21.4H 119.4E	LAND			5			72.4W 128.3E	46744
28	011500	21.44 119.0E	LAND			5			72.6m 120.3E	46744
24	011600	21.74 11A.7E	LAND			5			72.64 128.3E	46744
30	011700	21.74 119.4E	LAND			4			36.051 MO.55	46744
31	011900	21.7N 11A.1E	LAND			5			72.60 179.3E	46744
• 32	011440	21.16 119.1E	LAND						24.3m 128.6E	46770
33	011300	21.7N 117.9E	LAND			4			32.68 128.35	46744
34	012000	21.74 117.7E	LAND			5			36.051 Md.55	46744
35	012100	21.4N 117.4E	LAND			6			22.04 128.3E	46744
d t	012100	21.4N 117.5E	CAVO				10303 /////		35.411 WE.SS	45005
31	020180	37. 34 114.7E	LAND				11111 11111		22.3W 114.2E	45005
30	020100	37.5H 116.1E	(AND				25/// 53032		35.04 128.35	46744
34	020200	22.4N 115.7E					· · · · · ·		35.01 ME.SE	45005
40	020300	35.44 115.2E	LAND				11111 11111		35.41 ME.55	45005
-1	020300	22.4N 115.2E	LAND						35.41 46.25	45005
42	024400	22.5N 114.ME	LAND						35.011 NE.SE	45005
43	0 > 0 4 0 0	22.4N 114.HE							35-411 NE.SE	45085
44	024500	22.44 114.3E							35.01 ME. 25	45005
										40000

STHOSTIC FIRES

FIX INTENSITY WEAREST POSTITION FSTIMATE SATA (NM)

1 241200 10.5W 147.0E 15

### TROPICAL STORM GORDON

### SATELLITE FIRES

F LA	114E (2)	6021110M E   X	<b>VCLSA</b>	NAUSEK CUDE	SATELL LE	CJANFATS	SITE	
16 17 17 17 17 17 17 17 17 17 17 17 17 17	24125 241250 241433 242310 241107 241103 241133 241133 241332 271255	20.74   24.26 20.74   24.26 20.74   24.76 20.74   24.76 20.74   23.76 21.76   23.66 20.74   23.66 20.34   23.66 20.34   23.66 20.34   23.66 20.34   23.66 23.64   10.46 23.64   11.66 23.64   11.66 24.64   11.66 25.64   11.66 26.64   11.66 26.64	Prw 5 Prw 5 Prw 5 Prw 5 Prw 5 Prw 6 Prw 6 Prw 5 Prw 5 Prw 7 Prw 5 Prw 7	12-0/2-0 12-0/2-0 12-0/2-0 12-0/2-0 12-0/2-0 13-0/3-0 14-0/6-0 14-0/6-0 14-0/2-0 14-0/6-0 13-5/3-5 12-5/3-5 12-5/3-5 13-0/3-0 13-0/3-0 13-0/3-5/2-M	Despia   D	INII JUS  CI UP  BANDING TYPE FVE  CI SANE  INII JUS	Pole Pole Pole Pole Pole Pole Pole Pole	
		23.1N 114.1E	Prw 5		045014	CI DOWN	PGT	
					ATRCHAFT F	[xę>		
F14 40.	T1M5 (7)	61X 6021111111	FLT I VL			FLI-LVL-4MN ACCRY E VEL/HHD/MNG NAV/MFT SH	TAPE DIAUTATION	UNAN TAN DENEKT MUP
1 2 3 4 5 7 6	242036 242152 270810 270948 271336 272152	19.3% 120.7E 20.0% 127.2E 20.5% 126.5E 20.5% 126.0E 20.7% 124.0E 21.1% 122.0E 21.1% 122.0E 21.1% 122.0E	700mm 1200F I 700mm 700mm	394 50 12 394 50 12 30 13 3003 391 60 02 2942 383	120 0 30 080 0 40 070 0 50 110 110 0 30 150		CILAR 5 PTICAL 40 25 010	*25 *25 *25 *29
					BAJAN FITE	s		
FIR NO.	11M€ (7)	F14 00517170	PAUAR (			-COUE TOUFF COMMEN	175	MADER SITE POSITION WHO NO.
14 10 17 18 14 21 22 23	241300 241300 241300 241300 241300 241300 241300 241300 241300 242000 24300 243000 243000 243000 243000 243000 243000 243000 243000	21,10   21,45 20,20   21,15 21,00   21,15 21,00   21,15 21,20   21,15 21,20   21,15 21,20   21,16 21,20   21,16 21,20   21,16 21,20   21,16 22,20   21,16 21,16   21,16 21,16	A		\1001 64\24 84124	6270v 73111 7301u 72813		25,1% 121.6E 46496 25,1% 121.6E 46496 25,1% 121.6E 46496 27,1% 120.3E 46496 27,1% 120.3E 46744 27,1% 120.3E

### TROPICAL DEPRESSION 11

### CATELLITY FIXES

FIA	TTME	FTX						
NO.	(7)	POST T [ 0N	<b>∌CCRY</b>	DAUSAK CODE	SATFILITE	CJAMENTS	SITE	
	021317	12.19 135.3E	Prn 6		Ducesa	INII VIGHTIME OHS	PGTW	
• ¿	855060	13.4W 131.2E	PCN 5	TU- ( *0.0	DMSP35	INII Jds	PGTW	
· 3	030953	13.9N 13n.4E	PON D	1016.4180	DMSP 37	1.11 0-3	PGTW	
•	010953	14.5M 131.0E	PCN 6		DMSP37		RPMK	
5	071150	14.24 130.2E	PCN 6		DMSP34		PGTw	
6	031258	14.4N 130.3E	PCY 5		Dmdb30		PGT⊯	
• 7	031510	13.3N 12R.9E	PCN 5		0~5035		RODN	
8	01510	14.9u 13n.3E	PCN 6		DWSP35		₽GT₩	
	040032	15.04 127.7E	PCN 5	T0.0/0.0 /50.0/22HR	AFGP#G 2		PGT⊯	
• 10		15.74 12A.1E	PCN >		0meb 3d		₽61#	
• 11	040510	15.2N 124.1E	Prn 5	TU.0/0.0	DMSP35	[MI ] JQS	RODN	
• 12		15.44 12A.1E	PC4 5		Duspas		PGTW	
• 13	040733	14.94 127.0E	PCN 6		DMCH37		PGTW	
. 14	665140	14.4N 124.3E	PCN 5		Dadbán		PGTw	
• 15	041314	14.54 124.3E	PCN 5		DMebsy		PGTW	
• 16	041451	16.5N 126.0E	PCN 5		044634		PGT⊯	
• 17	041451	14.2N 125.4E	PCN 5		044035		RPMK	
• 16	044214	17.94 126.2E	PON 5		D <b>≃</b> 5037		PG <u>T</u> w	
19	050014	17.74 127.8E	PCN >	12.0/2.0 /02.0/24HR			PGTW	
20	050120	17.74 IZA.0E	Prn 3		DMSP14		PGT⊯	
21	050151	17.4N 12A.DE	PON 3		Duspas		PGTw	
22	050151	18.0N 126.9E	PCN 5	T1.0/1.0+/01.0/24HR			RODN	
23	041556	19.94 124.2E	Prw 3		りゃくちょく	EXPUSED I LCC	₽GT₩	
24	051402	19.2N 125.2E	PCN 6		Dadbin		RODN	
25	051433	14.04 175.8E	PCN 3		Duspas		PGT⊯	
• 26	052153	14.9N 122.8E	PCN 5	12.0/2.0 /S0.0/22HH			PGTW	
27	052153	19.34 123.6E	PCN 5	71.0/1.0	DHSP77	INII Jøs	RPMK	
• 58	052356	18.50 122.9E	PEN 5		DMensy		PGTw	
59	040243	19. 7N 127.5E	PCN 5	11.0/1.0 /50.0/25HR			RODN	
30	040314	19.34 123.4E	PCV 5		DMense		RODN	
31	060314	19.3N 123.5E	PCN 5		045632		RPMK	
32	041034	21.14 122.0E	PCN 5	T0.0/0.0	DMSP37	INI DOS	RKSO	
33	061317	51.0M 110.6E	PON 5		Dadbin		RODN	
						_		
				,	ATRCHAFT FI	XES		
FIX	TIME	FTX	FLI	70043 OBS MAX-SEC	-W4D MAX-F	FI-FAF-WU VCLBA	EYE FYE ORIEN-	EYE TEMP (C) 45N
	(2)	POSTTION	ĹŸĹ	HGT MSLP VEL/ARG				DUTY TAN DENSET HO.
	0.74415	14 40 175 15	7.00	1099 1003 10 230	49 334	15 060 48 5 5		•11 • 9 >8 Z
1		14.0% 132.1E	700MB 700MB			12 340 10 4 4		.11 + 9 28 2 .15 + 15 + 8 28 2
		14.7N 129.9E				30 140 35 4 15		.25 +23 28 4

### SYMPOTIC FIXES

FIX	T1ME	FTE	INTENSITY	NEAREST	COMMENTS
NU.	(7)	POSITION	ESTIMATE	Data (NM)	
		12.00 136.0E	15	120	

TYPHOON IRVING

Flx Nu.	T ( 42 ( 7 )	6 1 X 20 5 7 1 1 104	ACCRY	DAJSAK CODE	SATFII TTE	COMMENTS	SITE
	•••			TO PARK COURT	.4171777.2		3116
ı	021550	14.14 137.5E	Pry 6		PEASAG		w faq
Š	000023	14.14 134.1E	PCN 4	TU-0/0.0	Dwensa	INII JOS	PGTW
,	0 6 2 3 0 3	14.53 137.9E	Pry 3 Pry 5	#1 0 / 1 0 / 1 0 / 2 3 HP 6	AFG2MO		PGTW
5	412000	17.90 175.9E	Prus	T1.0/1.0 /01.0/23HR	DMCD34		PGT# PGT#
6	££€0₽0	19.34 135.5E	Pcv +		OHCD47		PGT#
7	001100	14.30 134.3F 17.44 134.6E	E POP		Dadbar Dadbar		PGTW
ÿ	091500	17.7× 134.4E	PCN 3		Deces		PGTW RPMK
10	006160	17.74 1 14.ME	Pry 3		Decade		RODY
15	10025	14.9× 177.3E	Pru s	-1	TEGPMG AEGPMG		PGTW
13	100127	14.44 177.18	Pry 3	T1.0/1.0 /S0.0/25HR	DMCDir		PGT# PGT#
14	100127	14,54 133.1E	PCN 3	T1.0/1.0	Dadbin	INII JOS	RODN
15	£1€0n1 £1€0n1	14.3H 132.0E	Pru 6 Pru 6		DMSP37		PGTW
17	101555	14.34 131.4E	Prad		DMCD3/		RODN PGTW
16	101307	19.54 131.4E	Pry 6		AFRIND		PGTW
50 19	101442	14.14 1/0.8E	PCN 5		D#5P35 D#5P37		RPHK
51	101445	17.0% 130.1E	PCN 3		DMSP35		PGTW RODM
55	102154	17.0% 120.ME	Pry 5		DMSP37		PGTW
23	1n2154 110009	17.0% 120.8E	Pry 5	T1.0/1.0	Dusp 17	INII JOS	RP4K
52	1;0100	16.74 179.6E	PCN 5	12.0/2.0 /Ul.0/24HRS	DWGP3n DVGP3U		PGT# PGT#
26	110142	14.4N 120.4E	PCN 5		Ducp 15		PGTW
28	110142	14.7N 129.5E	PCN D		D45P35		RPHK
29	111250	17.10 129.26	PCN 5		UMCD11		PGT# PGT#
JU	1:1349	17.2N 120.2E	PC4 6		DHSP39		PGTW
35	111423	17.34 120.3F	Pry 5		045P75		PGTW
33	112134	17.54 124.1E	PCN 5	T2.5/2.5 /01.5/24HRS			RKSD RPMK
34	112134	17.34 17K.7E	PC4 >	1-11112	045937		PGTW
35 36	112351 120230	17.64 127.6E	Pry 3	T3.0/3.0 /D1.0/24HRS			PGTW
31	120530	17.5% 127.7E	PCN 5	T3+n/3+A	DMCD34	INII DAS	RODN RPMK
36	120305	17.5N 177.0E	Pcn 5		DHSP75		RODN
3 <i>y</i>	121015	14.74 127.0E	PCN 5		Dusp 37	CI UP	PGTW
•1	121330	14.84 174.3E	PCN 5		AFGPAG PFGPAG		PGTW RPMK
42	121330	11.90 124.0E	Pry 5		Duceso		PGTW
4.5	121537	14.9N 174.3E	PCV 5		044P35 044P37		ROOM
45	122333	20.00 127.1E	PCN 5	T4.5/4.5 /01.5/24HRS			PGT# PGT#
46	115011	20.04 124.9E	PC4 3	T4.0/4.0 /01.0/24HRS	Dach to		RODN
47	130211	20.44 127.0E	PCN 3	T4.0/4.0+/01.5/29HRS	Ondbar Ondbar		RPHK
49	110247	20.74 127.0E	PCN 3		045935		RODN PGTW
50	130354	21.59 124.4E	PCN *		DMCH37		RODN
51 52	120754	21.44 124.7E 22.18 125.9E	PCN 6		DMSP3A		PGTW
55	121311	22.3N 125.4E	POND		046536		PGTW PGTW
54	121256	77.44 175.4E	PC4 3		DUSPR		ROOM
55 56	171528 172234	27.7N 125.4E	PCN 5	TR 0:5 0 (0) 0:3:440	D#4P74 D#4P77		RPHK
57	112235	23.04 175.1E	PCWS	T2-0/5-0-/01-0/21HRS	Dusp17		RPMK RODN
58	140055	27. PM 124.0E	PC4 5		DMCP3A		RPMK
59 60	140152	23.3H 125.1E 21.5H 124.8E	PCN 1 PCN 3	T4+5/4.5 /00.5/24HRS	Dachid Dachid		ROOM
61	140152	21.74 125.16	Pru 3	T4.5/4.5	DMCD30	IN11 345	PGT# RKSO
62	140559	27.4H 174.9F	PCN I		Duspas		PGTW
64	140228	23.4N 175.0E	Pry 1 Pry 2		045P35		RKSO
65	141116	24.54 124.7E	PCN S		0MSP37		RPMK RODM
66	141525	24.74 124.4E	PC4 I		Ducpag		RPMK
68	141338	24.54 124.6E 24.54 124.5E	PCM 3		Dacbie		PETM
67	161510	24.44 124.5E	Pry 3		D#4035		RK\$0 PgT#
7 U	142214	24.44 124.8E	Pry 1	75.5/5.5 /DD.3/24HR4	045017		RPMK
72	146615	25.44 124.7E	PCH 1 PCH 3	14.0/4.0 /HO.5/27HRS	045037 045034		RODN RKSO
7 5	ICUDIA	25.44 124.4E	PC4 3	15.0/5.0 /00.3/23MRS	Ducp 19		RODM
74 75	140503	34.64 124.65	Prw 3	T5.0/5.0 /50.0/24HRS	DMCD34		PGTu
76	150210	24.14 124.7E	Pru 3 Pru 3		)44774 		PGT
77	150210	24.3H 124.3E	PCN 3		DHCD34		ROON RKSO
7 g 7 g	141055	27.24 123.8E	PCM I		044017	-c 044	RPHK
60	141233	27.50 123.7E	Pru 2 Pru 1		045P37 0#5P34	PSN 843EN ON FYF	ROOM Patu
91	151233	27.64 127.6E	PC4 I		DHCD10		RKSO
8 } 8 5	14131 <i>+</i> 141320	27.5% 123.7E	PC4 I		Duspas		RPMK
84	151950	27.54 12354E 24.14 124.0E	Pry I Pry 3		Duspik Duspis		PGTW PGTW
80	141451	27.90 121.ME	Pry 3		Ducesa		RKS0

4b 87 88 89 91 92 93 95 97 98 101 102 103 104 105 107 108 111 113 114 115	15c15e 15c155 16c020 16c0151 16c0151 16c0256 16c0256 16c1302 16c1302 16c1302 16c1302 17c1302 17c1035 17cc1035 17cc1	29.20 123.76 29.70 123.66 31.40 123.76 30.10 123.76 30.10 123.76 30.20 123.77 30.10 123.77 31.50 123.77 31.50 123.77	PCN	1 15-0/5.5 1 15-0/5.0 1 15-0/5.0 1 15-0/5.0 1 1 1 3 3 3 3 3 73-0/4.0-3 3 73-0/4.0-3 3 73-0/4.0-3 3 73-0/4.0-3	/YU.0/24HRC /WU.5/24HRC /WU.0/24HRC /YU.0/26HRC /WU.0/26HRC /WU.0/26HRC /WU.0/27HRC /WU.0/27HRC	OMED 47 OMED 47 OMED 47 OMED 47 OMED 71		PG T# RPMK PG T# PG T# PG T# PG T# PG T# PK 50 ROON RN 50 RPMK RK 50 RC 9 PG T# RPMK RK 50 ROON ROON ROON ROON ROON ROON ROON ROO	
150 113 118	171556 172114 172114	34.5N 131.1E 41.5N 137.1E 41.5N 137.9E	PCN S PCN S PCN S	5 T2.5/3.5 . 5 Tl.5/2.5 .	/w2.8/27HRc /w1.5/24HRc	0msp34 0msp34 0msp37 0msp37		RKSO RPMK RPMK RKSO	
121 122 123 124	172345 180114 180218 180218	41.9N 137.5E 43.5N 134.5E 42.9N 134.6E 44.DN 135.1E	PCN S	<b>,</b>		D#4634 D#4634 D#4634		RPMK RKSO RPMK RKSO	
					47:	ACHAFT FIXES		ar 30	
Fix No.	T1#5 (7)	FIX Posttion	FLT LVL	70043 OBS		AD WVK-EF19-FAF AB UIM/AEF1940	-WNN ACCRY EYE INNO NAVIMET SHAPE	EAE ONIEN- BAL LEND (	
1 2 3 4 5 6 7 8 4 9 0 1 1 1 3 4 5 6 7 8 4 9 0 1 1 1 3 4 5 1 1 5 6 7 1 8 9 0 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 2 3 4 5 6 7 8 9 0 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	040008 040928 040928 0402122 140716 140914 140914 14091 141991 14091 14091 14091 14091 14091 14091 14091 14091 14091 14091 14090 140950 14090 14090	17.44 136.0E 14.14 136.0E 17.44 134.6E 17.44 131.6E 14.44 131.6E 17.44 170.2E 16.44 170.2E 16.44 170.2E 17.54 120.2E 17.54 120.2E 17.54 120.2E 17.57 120.2E 17.57 120.2E 17.78 120.2E		1037 994 1 1077 998 1 1076 998 1 1066 994 1016 992 1018 992 1018 992 1099 985 1099 9	20 100 1 20 270 7 30 130 1 30 330 2 30 210 5 45 290 15 55 200 5 55 310 3 65 130 12 70 020 17 75 330 9	10	35 5 6 420 6 10 10 7 12 10 7 5 10 7 5 10 5 5 400 5 1 420 5 1 420 5 1	13 - 10 - 25	29 1 2 3 3 4 4 5 6 6 7 7 7 8 8 9 9 10 11 11 12 13 14 14 15
FIX	TYME	Fly				AU FIXES			
NO.	(7)	P051110A	PAUAN	EY ACCHY SHA		MONTH-COUE	COMMENTS	MAJAR Pristrov	<11F
23 95 7 9 10 11 12 13 14 15 16	171900 171700 171700 172000 172000 172030 172100 172100 172200 172200 172300 172300	23.0M 176.4E 25.3N 126.3E 23.0M 126.1E 23.0N 126.1E 23.2N 126.3E	LAND LAND LAND LAND LAND LAND LAND LAND	POUR POUR POUR POUR	4.0 4.0 4.0	6///2 1/// 6///2 33611 5///2 52816 5///2 5//// 6///4 5//// 6///4 53105 6///4 52808 6///4 52808 6///4 52808 6///4 53308 6///2 53308 6///2 53304	EVE MOVO 3115	24.3M 124.2E 26.4M 125.3E 27.4M 125.3E	47918 47907 47907 47907 47907 47918 47907 47918 47907 47907 47918 47907 47907 47907 47907 47907 47907 47907

A VINDER OF MICHAEL

**\$** 

1+	1.0000	21.44	125.0E	LAND	POUM	5.0		EVE MINU	6 J115	24,86 1	25.3E	47927
20	140000	27.44	125.DE	LAND			5///2 524//			24. Ju	24.2E	47918
21	1.0000	21,34	124.0E	LAND			2///4 50000			24 HM 1	25.3E	47327
22	140030	21,54	174.4F	LAND	PAUM	6.0		EVE MOVE	R 3220	24. MN )	25.3E	.7927
23	140100		124.46	LAND	Pyuk	40		EAL MUNI	6 28)5	24.8N 1	25.3E	47977
2.	140100	21,54	154. HE	LAND			7///4 53210			74.84 1	25, 3E	47927
25	140100			LAND			6///2 53100			74.3N 1	24.2E	47918
• 26	1 40 100	24, 74	125.5E				A5//3 05510			24,0M 1	21.6E	46849
* 21	140500	21,54	154 . HE	LAND	Phon	**		EVE STU	•	24.HN 1	25.38	679>7
24	140500	27,44		LAND			6///2 52511			74.3N 1	24.2E	47918
2 s 3 u	140200	21,10		LAND			4///4 52705			74.8W 1	25.3E	47927
31	140200	27,44	1 > 2 - 11 -	LAND			24443 42421			24.0N 1	30.15	46509
35	140300	21,50	124.9E	LAND LAND			6///4 50413 6///2 72903			24 . HW 1	29.38	47927
ود	140300	23 20	174.06	LAND						24.3M 1	20.26	47918
39	140400	23.94	124.1E	LAND			21944 50120 22974 50105			24,04 1	21.05	46509
33	140400	21.74	124.9E	LAND			A///2 50313			74.0M 1	21.06	46699 47918
36	140400	21.44	174.4E	LA·ID			6///4 50/08			24,84		47997
37	140500	24.24	124.4E	LAND			17/14 50208 17444 53420			24.0H 1	21.0F	46649
36	140500	24.04		LAND			6///3 53514			24 HW 1	25.36	47927
3+		21, 10	124.9E	LAND			5///2 53611			24.3N 1	24. ZE	47918
40	140500	24.34	174.4E	LAND			24444 5340/			24.0M 1	21.6E	46609
41	140500	24.14	125.08	LAND			5///3 50308			74.RM 1		47977
42	140500	24.14		LAND	ნემს	4.0		EAE MUAL	A 3335	24,64 1	25.3€	47927
4.3	140600		124.7F	LAND			6///2 73612			24.34 1	24.2E	47916
**	140700		124.76	CNAJ			20773 52714			24 . HW 1	>5.3E	479>7
• >	140700	Se • SM	124 . RE	LAND	5700	4.0		EAE MUAS	4 3205	24.6H 1	25.3E	47997
*6	140700	54. SM		LAND			10984 52407			24.00 1	21.6E	46649
47	1.0700		174.7E	LAND			4///2 73315			24.3H 1	24.ZE	47918
49	140900	24.14	174.75	LAND	a - 00		11/14 52105		_	24,04 1	5 J • PE	46649
50	140900	24 1 1	124.6E 124.7E	LAND	ดามบ	10	A///2 73305	EVE STU	•	24.84 1	23.3E	47927
51		24.14	13. 75	LAND						24,34 1	54. SF.	47918
52	140+00	24 3	124.9E				6//44 50000 6/60 ts/45			24.64 1	23.JE	47997
53	140700	24.34	144.4E	LAND			6///3 70604			24.84 1	23.3E	47997
5.	141000	24.40	124.75	LAND			20713 53114			24.3M 1	24.25	47918
55	1.1100	24.54		LAND			6///3 73507			74.34 (	27.JE	47997 47978
56	141100	24.5N		LAND			45/43 53000			24.84	24.66	47927
57	141100	34.54	124.5E	LAND	FalR	5.0		EVE MOVE	3228	24.8N 1	23. JE	A79P7
58	141200	24 5N	174.6E	CHAJ			12043 63006			24.0M 1	Pl.AF	46699
54	141200	24.54		LAND			6///3 50100			24,64 1	25. 1E	47997
60	141200	24.50	124.5E	LAND	FAIR	6.0		EYE MOVE	A 3220	24.64 1		47997
61	141200		124.8E	CAND	-		6///3 73407			24.34 1	24.2E	47918
65	141235		125.0E	CAND	Phofi					26.4N 1	27.8E	47991
. 65	141235	24.64	35.25	LAND	PAUR					26.44 1	27.68	47931
64	141300	24. 9N	124.5E	LAND	FAIR	30		EVE MOVE	3220	24.60 1	25.3E	47907
65	141300	24.9N	124.6E	LAND			77973 53608			24.0% 1	31.6E	46699
66	141300	24.74		CHAJ			A4/A3 53007			24.64 1	25.JE	47997
67	141300	24,54	124.7E	LAND			6///3 73005			24.34 i		47918
• 68	141310	24.5N	125.4E	LAND	POR					26.4N 1		47991
69 70	141400	24.90	124.5E	LAND	FalR	30		EAE MUA	A 3270	24.8N 1	25, 3E	47927
71	141400	27.9N		LAND			6///3 53605			24.84 1	25.3E	47927
72	144435		174.6E	LAND	0.40		6///3 73404			24.34 1	24.ZE	47918
73	141500	24 011	124.5E	LANG UMAJ	AJDR		6///3 73208			26.44	3/-36	47918
74	141500	24.94		CAND			4///3 53211			24.34 12 24.84 1	24.25	47997
75	141500	25.1N	124.36	CAND	FAIR	30	W///2 22611	EVE MOVE	2220	24.84 1		47927
76	141600	24.9N		LAND	2846	• • •	A///3 52705	EAE MAIN	, 3550	24.6N 1	27.35	
77	141600	25.0N	154.5E	CAND			21944 52720			24.0N	21.45	47977
78	141500	24.30	124.6E	LAND			6///3 73306			24.3h 1		47918
79	141500	25.2N	124.4E	LAND	FAIR	30		EVE MOVE	1610	24.8N	26. 15	47927
89	141700		124.3E	LAND			21943 53311		. 50.0	24.8M 1	25.3E	47997
81	141700	25.0N		LAND			6///2 73407			24.30 i		47958
85	141700	24.3N	124.3E	LAND	FAIR	30		EVE MOVE	3510	24.8H 1	25.3E	47997
83	141700	25. IN	124.4E	LAND						24,0H 1	21.6E	46649
84	141500	25.24	124.3E	CAND			55/43 53410			24.8H 12	25.3E	47927
85	141900	25. SN		LAND	- •-		A///2 73608			24,3N 1	24.2E	47918
86	141900		124.4E	LAND	FAIR	30		EVE MOVE	3010	24.8N 1	25.3E	47997
• 67	141510	25.14	124.4E	LAND	FAIR					56,4M 1		47931
	141900	24.5N	124.5E	OFAJ	POOR		10018 -43-4			26,4H 1	21.6E	47991
90	141900	25 34	124.38	LAND	w. 10		10915 50316	e Ma		24, 0W 1	SI.OE	46649
91	141900	25,3N 25,3N	124.25	LAND	Fair Fair	36 36		EYE STAR		24.8W 1	(3, JE	479P7 479P7
92	142000	25.3N		LAND		410	75/13 50000	C. A. S. MA	•	24 BH 1	23.36	47777
ÝÌ	144000	25.64		LAND			6///2 73507			24.8W 12	24_28	47997 47918
94	142010	25.14		CAND	POR		[ Jay	PREL CHI	r <del>a</del>	26,4H 1	27 85	47991
95	142100	25.5N	124.3E	LAND			21944 50509		• • •	24.5H 1	21.6F	46549
96	142100		124.4E	LAND			6///2 73207			24,3M 1	34.2E	47918
97	144100	25.4N	124.5E	LAND	FAIR	30		EVE MOVE	9 3610	24 MM 1	25.3E	47997
96	142100	25. 6N	124.3€	LAND	-		25/43 50508			24 BH 1	25.3E	47997
99	142135	25.54	124.2E		PODR			PRBL CHI	r <del>a</del>	26,4H 1	27.8E	47971
100	144500	25.54	124.4E	FAND			5//43 50607			24.8N 1	25. 3E	47927
	145500	25.44	124.4E				6///3 73303			24.3W 12	35.45	47918
105	145500						25/45			24,04 1	36.15	46649
103	145500	25.54	124.3E	LAND	PODR			EVE MOVE	3605	24 BN 1	25.3E	47927
104	145510			LAND	PIOR			PROL CHI		26.4H 1	27.8E	47971
105	142235	25.3N	124.4E	LAND	PADR		44449 -4443	PEBL CHI	TR .	26.4m 1		47971
	142300		174496	LAND			6///2 73403			24.3M 12	75.05	A7918
			124475	LAND	PODR		4//43 50311	C		24 AM 1	(), JL	47397
100	142300		174.3E	LAND	POUR			EVE MOVE		76.3M 1	23.55	47999
	150000		124.5E		PIOR			EVE MOVE		26.4M 1	C	47472
111	150000	25. 94	124.58	LAND			4///3 51415	# 4.F 14.184		24,88 1	36.35	47927
112	140000	25.4N	174.4E	LAND			6///2 70104			24.5H 1	24.25	47918
					<b>-</b> .							
111	140010	25,54	124.3E	LAND	POOR			PROL CHI	T <del>w</del>	26,4H 1		47931

114	150035	24.0N 125.3E	LAND	POUR		HEHE CHIM	26.4M 127.8E	47931
115	150100	24.9N 124.3E	LAND	POUR		FAE MUNE 3550	26.3¥ 125.8E	. 7 775
116	150135	24.2N 124.5E	LAVD	POUR		PSHL CNTH	26.4× 127.8E	47971
117	150200	24.4N 124.5E	LAND		6///3 53611	-	74.8N 125.3E	47927
118	150200	24.2W 174.3E	LAND	POUR		EVE MOVE 3620	26.3N 125.8E	47429
119	150235	24.4N 124.5E	LA vo	POUR		PSRL CHTH	26.4M 127.8E	47931
120	150300	25.5N 124.4E	LAND		6///4 53414	,	24.8M 125.3E	67927
121	1-0300	26.4N 124.3E	LAND	PADR		EYF MOVE 3620	26.3N 125.8E	47329
155	150310	24.74 124.7E	LAND	POUR		PSHL CHTH	26.4N 127.8E	47931
123	150500	23.4N 125.0E	LAND	GOUD	5p	EVE MOVE 3120	24. HN 125.3E	47927
124	150500	27.2N 123.9E	CHAL	(,,,,,,,	6///4 53226	EAL MINN 2150	24.HN 125.3E	7927
•125	150535	27.74 124.2E	LAND	POUN	M///4 33EEE	PSHL CNTH	26.4N 127.8E	47931
126	150700	27.2N 127.8E	LAND	FAIR	40	EVE MOVE 2920	76.3N 125.8E	7929
•127				POUR	40		26.4N 127.BE	7+11
	150710	27.9N 124.2E	LAND			PSBL CHTH		
•15B	150735	27.2N 125.0E	LAVO	POUR		PCHL CHTH	26.4M 127.8E	47931
129	150800	27.14 123.7E	LAND		K///3 729UY		24.8W 125.3E	47927
130	150300	27.2N 127.HE	LAND	FAIH	50	EYE STNA	26.3N 125.8E	47929
131	150900	27.1N 127.HE	( Au)		20473 50000		24.8N 125.3E	47927
132	150900	27.2N 123.9E	LAND	FAIH	50	EVF STUR	26.3N 125.BE	47929
133	1<1000	27.IN 127.HE	LAND		5//43 50000		24.HM 125.3E	47727
134	141100	77.34 123.4E	CMAJ		5//43 53609		74.84 125.3E	47927
135	151100	27.24 123.HE	LAND	FAIR	55	Evf Move 3210	26.3N 125.8E	47929
136	151100	23.4W 123.8E	LAND	FAIH	55	EVF MOVE 3210	26.2W 127.7E	47930
137	151200	27.5N 123.4E	LAND		6//44 50211		24.8M 125.3E	47727
135	151200	27.5N 123.7E	LAND	FAIR	55	EVE MOVE 3510	26.3N 125.8E	47929
137	151300	27.54 123.4E	LAND		6//14 50000		74.HN 125.3E	47927
140	1 < 1 300	27.5N 123.HE	LAND	FAIR	30	EYF MOVE 3610	26.3≈ 125.8€	47929
141	151400	27.54 123.4E	LAND		6///4 53506		24.HW 125.3E	47927
142	151400	27. 3N 124.0E	LAND	ცესს	55	EVE MOVG U215	26.34 125.8E	47929
143	151500	27.9N 124.0E	LAND	GNUU	60	EVE MOVE 0120	26.JM 125.BE	47929
144	154700	24.34 123.AE	LAND	6100	60	EVE MOVE 3620	26.3N 125.BE	47929
145	151900	24.54 121.8E	LAND	POUR		EVE MOVE 3620	26.3N 125.8E	47729
146	151730	28.3N 174.0E	ACFT			NAV ACCIHACY DNH		54435
147	156151	34.24 127.AE	ACFT			****		54875
148	152335		LAND	POR		PSHL CHTH	26.4N 127.8E	47931
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### SUPER TYPHOON JUDY

### SATELLITE FIXES

FIX	TTHE	FTX					
NO.	(7)	POSITION	ACCR.	SAJSWK COUE	SATFILITE	CJ4HFNTS	SITE
1	151310	13.7N 150.1E	Prn h		DMSP35		PGTw
2	152239	17.20 150.4E	PCNS	T0.0/0.0	DMCD3r	INII JOS	PGTW
	141120	17.54 145.48	PCV 5		DMEDIV		PGTW
4	142134	13.14 144.1E	PC4 5		045037	EUGE JE DATA	PGT
	170055	17.74 147.7E	Prw 5	T3.0/3.0 /03.0/27HR9	DMCD 14		PGTW
5	170132	13.94 147.4E	PCN 6		Dazbar		PG1#
- 1	170133	14.14 147.4E	PC4 5	T3.0/3.0	044644	INII JOS	RPMK
8	171015	17.94 LAD.HE	PCN 5		045937		PGTW
7	171155	14.44 140.3E	PCN 5		0-4634		PGTW
10	171414	14.4N 140.5E	PCN 5		044015		PGT₩
11	171414	14.94 140.4E	PCN 6		DWCD3H		ROOM
15	174114	15.44 138.7E	PCN b		DMSP37		PGT#
13	172345	15.44 138.0E	PCN 5	T4+0/4+0 /01+0/23HR9	DASP4A		PGT
1.	176345	15.6M 138.7E	Pry 3	T4.0/4.0	045634	SPC IINI	RODN
15	189036	15.40 139.5E	Pry 5		DHENJA		PGTW
15	140036	15.50 139.5E	PCN 5	T4+0/4+0+/01+0/23HRS	DMCh34		RPMK
17	140114	15.64 138.4E	PCN 5		Duspas		PGTW
18	140354	14.44 137.6E	PCN h		Dusp 37		PGTW
į,	141226	14.7N 137.1E	PCW 5		DAZES		PGTW
žó	181355	17.1"   37.0E	PCVS		Duspas		PGTW
SI	141355	14.54 137.2E	Pry 5		Dusp 15		RODN
22	141455	14.74 137.UE	PC4 5		Duspah		RPMK
23	144054	17.94 136.1E	PC4 L		0.5937		PGTW
24	192327	14.24 135.HE	PCN I	15.0/6.0 /DZ.0/24HRS	AFGPMO		PGTW
ēέ	190159	14.54 135.6E	PC v 1		Duspas		PGTW
5.0	100237	14.44 135.5E	Prv I	16.0/6.0 /01.5/26HRS			RPMK
21	100237	14.5" 135.5E	PCV 1		DWSD35		PGTW
28	190734	19.4x 134.9E	Pry ?		DMSP 17		PGTW
29	602161	19.74 134.0E	Prv L		DMCD34		PGT#
30	191258	1 3. Av. 134.7E	PCN I		DMSP34		PGTW
31	191337	20.0- 134.HE	PCV P		DMSP35		PGTW
32	101519	17.94 134.7E	Pi 1		DMSP35		RPMK
ۆز	191517	14.74 174.4E	Pr ( I		045435		RODN
34	192034	20.5V 134.4E	Pry 5		045837		PGTW
35	196309	21.34 137.HE	Prw 1	15.0/6.0 /41.0/24HRS			PGTW
36	200140	21.5N 133.0E	Prw L	17.0/7.0 /01.0/23HR			RPMK
37	200140	21.55 133.6E	Pry I	10.0/6.0	DHCH34	INII Jec IINI	RODY
٠.	2., 71 70				J 1- 1-		

38	enstra	21.70	137.68	PCW L		Duchit		ROON
34	500513	21.74	137.55	Prw L		044614		Púlw
40	200314		132.HE	PC4 2		Dren 11		PGTW
41	201055		132.4E	PC4 +		DACASI		HPMK
+2	201150		132.5E 132.1E	Pry 5		Dado 14		PGT#
**	201500		111.4E	Pry 2		044514		PGT# RPMK
45	201500		131.9E	PCN I		Duspis		RODN
46	201500		131.7E	Prv 1		Dusp 15		PGTW
47	242155	21.24	131.6E	PCN 3	12.0/4.0 \AS.0/50HK2	DUCPET		RPMK
48	202155	21.24	131-1E	Pru 3		046511		PGTW
50	210033		131.IE	Prw 3	T3.0/5.0 /+1.0/22HRs	OMENSA		RODY
51	510151		131.1E 130.9E	Pry 3	13.0/5.0 /SU.0/25HRS	Dadb3a Gadb34		PGT# ROJN
52	210121		130.98	Pry 3		DMSP34		RPMK
53	210121	21.50	34.98	Pry 3		DMCD 14		PG1 d
54	219200	23.5	130.BE	PCN 3		DMCDIN		PGI≓
55	211036		129.9E	Pry 5		Dusp 17		RODN
56	511550		129.7E 129.6F	Pry 5		Ducp 37		PGT#
58	211314		129.3E	Prys		DMSP35	C1 DOWN	PGT#
59	211441		120.25	Pry 2		DMSP 45		RPMK
60	211442	24.34	120.28	PCN 1		Duspah		ROUN
61	211442		129.0F	PCY 5		045632		PGI₩
65	212135		124.25	PCY I		DHSP 17		RODN
63	212135 212135		12A.1E	PCV 2	15.0/5.0 /50.0/24HRS	Duco 17		RPMK
65	220015		12A.1E 127.7E	PCN 3	74.5/6 A /UN. 2/24HDE	Duspit Duspit		PGTW
66	220015		127.7E	PCN 3	T4.5/5.0 /w0.5/24HRS T4.5/4.5 /w0.5/24HRS	Duspan		ROUN PGT#
67	220105		127.4E	Pry 3	***************************************	Dacosa		ROUN
68	220142		127.4E	PC4 3		DUSPIS		PGT
69	220243	24.0%	127.5E	Pru 3		Decase		RKSO
70	220243		127.4E	Pry 3		DMSP39		RODN
71	221016	24.54	124.HE	Pon 6		OMEDAS		ROUN
72 73	2>1256 2>1616		127.0E	PCN B		Dada se Dada 11		PGT# PGT#
74	221529		124.HE	Prvs		DHENJA		RODA
75	221343	24.44		Pry 4		Buspao		RPMK
76	271343		124.HE	PCN 5		DAZBAA		RK50
77	221343		154.HE	PCN		Duchia		ROUN
78 7÷	221123 222115		124.6E	Pry 5 Pry 3		045P35		PGT
80	222115	25.5N	154.15	PCW 3		DWSP37		₩T24 PCOR
01	222115		125.9E	PCN 2		045037		9244
82	222357		124.8E	Pry 5	15.0/5.0	DMCP 16	INI JOS	9K50
83	222357	24.44		PC4 5	15.0/5.0-/00.5/24HRC	PERSMO		PGTW
84	53055+	24.54		PCN I	T>.0/5.0 /50.0/29HR5	DMCD30		RP4K
85 86	230554		125.1E	PCW 1	12-075-0 100-5/25HK5	Decriso		ROUN
87	210305	24.5H	125.15	PCW 1		Dusp34 Dusp35		RKSO RODN
68	230955	27.2N		PC4 2		Dugual		<b>РРМК</b>
89	270955	27.5N		PCV 2		Duspar		RODN
90	270755	27.34		PCN I		DUSPRI		PGTW
91	231136	27.34		PCN 2		DMSP 17		RP4K
92	541538	27.60		Prw 1		DACHSW		PGTW
94	231334	27.24 27.50	127.6F	PCM 1 PCM 1		D#2514 D#2534		HODN RKSD
95	211324	27.54		PCN 1		Ducesa		#19e
96	211547	27.9N	123.38	Pry 3		Duspas		RKSO
97	211547	27.54	123.3E	PCH 1		DMSP35		RODY
98	212536	29.44		PCA 5		Duspar		<b>ЯРЧК</b>
100	212336 212338	29.74 24.54	123.08	PCN 1 PCN 1	** *** * ***	PERSHU PERSHU		HOUN
101	240150	54.30	122.15	Pru 3	14.0/5.0 /#1.0/24HR4	DUSPER		PGT# RPMK
102	240505	29.04		PCV 1		0msp 14		189
103	240205	29.04		PCN 1	T4.0/5.0-/W1.0/24HRS	PEUPMO		RPMK
104	244505	20.04		PCN I	T5.11/6.0-/01.0/26HRS	DHCD30		RK50
105	240246	29.14		PCN I		DMSP35		RKSO
106	240247 241117	29.1N 29.8N	177.15	PCN 3	15+0/6-0-/D1-9/24HRS	DMSD35 DMSD37		ROON
108	241117	29.74		PCN		DMCD11		ЯК <b>5</b> 0 Ярмк
103	241305	34.14		PC4 3		OMERSA		PGT
110	241401	30.34		PCN 3		DMCH34		RPMK
111	241525	30.24	122.58	PCN 3		044634		RK50
112	241528	30.14	122.56	PC4 3		DMense		RODN
113	242516		122.9E	Pry 3	13.0/4.0 /W1.0/20HRs	044637		RPMK
115	242516	37.44		PCH 3	74.0/5.0-/42.0/23HRS	DMZ637		RODN
116	250146	31.04	121.2F	PCN	13.0/4.0 /W1.0/25HRS	Dazhio		RKSD PGT#
117	544558	31.00		Pry 3		DMCD35		RK50
115	240558		127.48	PCN 3	T4+0/5.0-/=2.0/24HR9	DMCD34		RODA
119	251056	31 - 5N	124 - 3E	PCN 3		DMCD31		RP4K
120 121	251246 251246		124.0E	PCN 5		Dwen 30		HOUN
155	241546	32.9N 31.7N		PCN 5		Dadh 1d Dadh 1d		RKSO PGTW
123	241344		124.4E	Prn 3		DMCD34		ROME
12+	251310	31.34	124.AE	PCN 5		Duchie		PGTW
125	241210	31.54	124.5E	Pry 3		DHEPTH		RODN
126	251510	32.14		Pry 5		045935		RKSO
127 126	252155 252156	32.54		E W19	12.0/3.0-/W1.0/24HHC	D=4011 D=4017		HP4K
124	240042	32.44		Pry 3		DMSP3A		RODN RP4K
130	240127		124.2E	Pra 5	12.1/1.0 /wl.n/24HRs	Dadasa		w159
131	240510	37.41	326.HE	Pry 3	12.0/7.0-/#2.0/24HRC	OMED 14		9004
132	540510	31.74	124.58	Pry 5		ORED 12		PGTW
133	549510		124.75	Prv J	FC+0/7.0-/W2+0/25HR5	Duspay		RK\$0
134 611	541036 541036	34.44		Pry 4 Pry 3		044531		RODY
	0 30	3 1 <b>, 2</b> 4				0=45+1		RPMK

136	241227	34.65 124.55	Pry 3	Decade	RKSO
137	541551	34.44 12H.7E	Pry J	Dweban	PGI#
130	241325	14.3M 120.2E	Pru 5	Dreshar	RPMK
134	241451	34.50 129.0E	PCN 5	DMSP34	RKSO
		34. 2., 120.0F		Dugoza	RODN

### ATRCHAFT PIXES

FIX	FIME	5 T X	FLT	70043	385	M & X -	-SFC-	- w v0	MAX	-FL T	LVL	-480	AC	PY	EYE	EVE ORIEN-	EYE TEMP (C)	45N
NO.	(7)	40111264	ίΫL	461	MSLP	VEL	/4RG/	PYG	01W	/VFL	/HH6	/HNG	NAV	ME T	SHAPE	DIAW/TATION	DUTY THE OPING	NO.
																	-	
1	152341	11.9% 147.5E	7 n 0 mH	3068	<b>398</b>	35	110	70	n Q n	54	0 2 0	15	4	5			·1# ·12 ·12	2
2	170303	14.NN [47.7E	7 n 0 MM	2043	795	35	360	15	060	46	350	90	3	10			•11 •11	2
٤	170505	14.24 142.2E	7 n 0 mm	3025	994	40	090	16	180	46	040	14	5	10			+16 +11 +10	2
•	174048	15.34 139.5€	7 n n MH	2492	987	70	090	15	170	61	040	10	5	7	CIRCIILAR	10	+11 +12 +14 >6	3
>	140554	14.34 13R.ZE	7 n 0 mm	2/07	956	55	270	10	636	84	500	5	1	3	CIRCULAR	6	·15 ·11	•
6	140945	14.54 1.17. ME	7 n 0 MH	2717	956	65	350	5	350	96	330	5	2	2	CINCHLAR	5	·13 ·18 ·10	•
7	1×1932	17.7N 146.3E	7 n 0 mm	2411	922				360	93	580	5	•	2			+19 +17	5
Ħ	192149	17. AN 134.2E	7 n 0 mH	>336	714	55	260	12	120	90	260	7	1	- 1	CIRCULAR	5	+14 +23 +18	5
ý	191036	19.5M 134.HE	71048	7295	909				280	92	170	15		3	CINCILLAR	7	+1h +15	6
10	191921	20.7N 1 14.3E	7 n g 4 H	2121	889				270	108	100	Ξ,	5	5			+34 +1B	7
1.1	192145	30.05 1 74.05	700MB	2091	987	70	060	15	360	110	270	5	5	2	CINCHLAR	5	·14 ·24 ·15	7
15	200500	22.18 1 13.1E	710MH	2241	90A	130	030	3	120	136	030	4	2	7			.18 -18	8
13	240943	27.54 177.0F	7004H	23#n	919	50	280	4.0	160	110	270	10	,	2	CIRCILLAR	7	·1# ·17 ·15	8
14	292259	23.34 1 31.2E	700MH	7379	940	100	050	30	020	84	120	14	5	5	CIRCULAR	10	+17 +18 +12	9
Ĺo	210300	23.5N 130.ME	710MH	2611	945		010	10	070		010		5	10	CIRCULAR	25	+19 +19 +14	9
16	2,0503	34.74 130.5E	700MH	2613	945	100	350	10	250	75	1/0	40	10	5			+20 +15	10
17	214842	24.24 130.2E	700MB	2614	944	100	160	10	340	76	210	30	- 5	2	CIRCULAR	30	+14 +18 +15	10
18	516506	24.24 128.2E	71048	267A	952		140	>0	110			154	4	2			+10 +15 +16	ii
19	220117	24.34: 127.HE	7 n 0 m t3	2679			350	15	140		260			خ			+18 +16	ii
20	220247	24.3M 127.6E	700MB	2684	951	95	0.30	15	120	78	030	120	4	2			+18 +19 +17	11
21	220550	24.24 127.3E	700MH	267R	953				120	78		143	5	3			+16 +15	12
2.5	220958	24.3N 127.2E	700MB	2004	949	75	300	15	290		550		4	Š	CIRCULAR	35	·14 ·15 ·15	iē
23	2>1932	25.24 124.2E	70048	2634	946			• -	140		050		2	A			+18 +15	13
24	5>5500	25.54 125.4E	700411	2667	946	55	120	150	180		120		3	10	CIRCULAR	20	+13 +18 +16	13
25	230500	26.9M 124.3E	TODMH	2669	952		080		120		080		5	2			+15 +15	14
26	230818	27.1N 124.2E	700MH		950				210		140		5	5	CIRCULAR	15	·10 ·15 ·15	14

### PAJAH FIKES

FIX NO.	FTME (7)	F19 P0511[0N	RADAR	ACCRY	EYE SHAPE	EYF DIAM	RADON-CODE	COMMENTS	HADAR Posttion	411k
1	141535	13.1N 145.1E	LAND	FAIR				NFG WALL CLD	13,6N 144.9E	91218
2	141710	13.24 144.9E	LAND	FAIH	ELLIPTICAL			AXIS IN/5	13,6W 144.9E	91218
و	161935	17.54 144.5E	LAND						13.6N 144.9E	91218
•	144010	13.5M 144.2E	LAND	FAIR	CTRCIILAR	35		CHIR OPEN SH-N	13.6N 164.9E	91518
>	144135	17. RN 147. ME	CAHD	FAIR	CIRCULAR	30		NFG WALL CLD OPEN SW AND WE	13.6N 144.9E	91518
6	210500	23.4N 13n.3E	LAND				309/4 4////		26.1M 127.7E	47937
	210700	24.0N 130.4E	LAND				30842 53022		26.IN 127.7E	47937
В	210400	34.0N 130.2E	LAND				35/// 52709		26.14 127.76	47937
9	210900	54.5H 130.5E	LAND	GnDD		4.0			26.14 127.7E	47977
10	510300	54.14 130.JE	LAND				35/// 53010		26.IN 127.7E	47937
11	210900	24.1M 130.1E	LAND	GnJU		¥.0			26.1N 127.7E	47937
12	211000	54.1M 159.HE	LAND	Gา0D		36		EAE MUAU 5850	26.1% 127.7E	47937
13	2,1100	24.00 120.HE	LAND				35//0 52412		26.1M 127.7E	47937
1 4	211100	24.1N 124.7E	LAND	FAIR		4.0		EAE MUNG 5150	26.IN 127.7E	47937
l o	511500	24.04 129.4E	(AN)				5///2 72611		26.1m 127.7E	47937
16	511500	24.14 129.5E	LAND	FAIR		40		EAE MUNU 5150	26.1M 127.7E	47937
17	211300	34.9N 129.3E	LAND				5///1 72710		26.1M 127.7E	47997
18	211300	54.14 150.4E	LAND	6100		40		EVE MOVE 2720	26.1M 127.7E	47937
19	211400	34.14 129.2E	LAND				5///2 72707		26.1W 127.7E	47937
20	211400	24.14 120.2E	LAND	ცისი		4.0		EVE MONE 5750	26.14 127.75	47937
51	211500	24.14 129.1E	LAND	00			5///2 72806		26.1N 127.7E	47937
55	211500	24.1N 120.1E	LAND	POOR				EVE MOVA 2720	26.1M 127.7E	47937
53	211500	54.54 150.SE	LAND				5///2 70408		26. IN 127.7E	47937
24 25	211500	34.14 128.4E	LAMD	POUR				EVE MOVE 2720	26.1N 127.7E	47937
	211700	24.34 128.9E	LAHO				5///3 73107	Walla	26. IN 127.7E	47937
56	211700	24.24 12R.7E	LAND	POOR				EVE MOVE 2720	26.1M 127.7E	47937
21	211800	74.74 124.9E	LAND	0-00			15//3 7330/	55 Mayo 2326	26.IN 127.7E	47997
29	211900	24.24 128.5E	LAND	POUR				EAE MUNE 5150	26.IN 127.7E	47977
30	511300	24.34 128.7E	LAHD				25//3 72909		26.14 127.7E	47917
31	211710	24.24 124.5E	LAND	POOR				EVE STUR	26.14 127.7E	47997
35	515000	24.3N 124.6E	LAND				6///1 72706		26.1m 127.7E	47937
33	512000	24. 44 128.5E	LAND	6700		4.0			26.1W 127.7E	47937
34	512100	24.34 128.3E	LAND	POR			4///1 72611	EVE MOVE 2715	26.1W 127.7E	47937
35	512500	24.4N 124.3E	LAND	PIJUN			5///1 72609	EAC MILAN SATO	26.1N 127.7E 26.1N 127.7E	47937 47937
36	514500	24.34 120.38	( A4)	PADR			7///1 /2007	EYE MOVE 2715	26.1M 127.7E	7937
37	212300	24.34 174.0E	LAND	PAUR				EVE MOVE 2715	26.14 127.7E	47937
38	220000	74.3N 127.9E	LAND	P-104			5///3 72808	EAC MUAN \$113	26.1M 127.7E	47937
34	520000	24.3N 127.9F	LAND	POOR			7///3 /2000	EVE MOVG 2720		
40	\$20000	24. 1N 127.7E	LAND	POR				EVE MOVA 2730	26.1N 127.7E	47937
41	520500	27.04 127.5E	LAND	- JOH			3///2 72719	EAC WIAM CLAA	26.1% 127.7E	47977 47977
	220200	24.24 127.5E	LAND				3///2 72507		76.1# 127.7E	47937
	220300	24.34 127.2E	LAND	POOR			/ / E / E JU!	EVE MOUR 2320	76.1W 127.7E	47937
44	250300	24.10 127.2E	LAND	F 10K			22704 5////	ELE MILLIO EREA	24.8M 125.3E	47927
45	220400	24. IN 127.3E	LAND				3///1 72511		26.14 127.7E	
46	220500	24.15 127.16	LAND				A//// 50000		24.3N 124.2E	47937
47	220500	24.24 127.2E	LAND				22R14 53306		74.4N 125.3E	47918 47927
46	220200						5///1 72405		26.1W 127.7E	47977
	2,0300	C-* IN 17 1-1935					//1 /2-05			41441

49 50	270500 270600		127.3E		はしてい	711			Ev€	Move	0920	76.1	4 127.7	E 47+37
51	220600	24.34	127.35	LAND	<b>ც</b> იას	70	6////	51204	FUF	STNR		24.3	" 124.2	1741R
52 53	220600 220700		127.26	LAHO				72500				26.1	127.7	E 47937
54	220700	24.14	127.1E 127.0E	L AHD	POUH		6////	71804	546	Move	24.10	24.3	4 124.2	E 4741H
55 58	270800	74.3N	127.28	LAMD				73404	CTE	7117914	2430	26.1	4 127.7 4 127.7	E 47947
57	220800 220800	24.00	127.28	L AND				71502				24,8	4 125.3	IE 47727
58	220500	24.14	127.0E	LAND	POUR		.,,,,	11302	EVE	STWR		24. <i>5</i> * 26. 11	124.2	E 47977
59 60	220835 220300	24.14	127.2E	LAND	POUH POUH							76.4	4 127.8	E 47431
61	220300	24.34	127.2E	LAND	7 /511		50A74	53607	EAF	STUP		26.14 26.41	127.7	E 47971
62	224700 224710		127.2E	CAND	POUR		21A73	73605				26.19	4 127.7	E 47997
64	271000	24.4N	127.ZE	LAMD			27045	53005				/6.4/ 24 H	8.151 Y	E 47771
65 66	221035 221100	24.3N	127.0E	LAND	PAUR							26.44	1 127.8	E 47971
67	221100	24.44	127.06	LAND	PAUH		>1473	52/11	Fvŧ	MOVE	2420	26.M	123.3	E 47927
68 69	221110 221110	24.4N	127.3E	LAND	POUR		3///3	7340+	-			/b, i*	* 121.1	£ 67477
70	271135	24.44	127.0€	LAND	POUR							76.4	i 127.8	F 47391
71	551500 551500			LAND	POUR				٤٧f	MUAU	3525	26.11	127.8	E 47971
73	551500	24.44	174.9E	LAND			2///5	72908 53414				76.11	1 127.7	E 47937
74 75	221510 221535	24.4N	127.0F	LAND	POOR							76.41	125.3	E 47931
76	221300	24.7N	176.7E	LAND LAND	PYÜN		22712	52814				25.44	127.8	E #793]
77 78	221300 221300		126.7E 126.8E	LAND	6000	45		-	EYF	MUAR	3020	26,34	125.3	E 47437
79	271310	24.74	126.6E	LAND	POUR		2///6	73011				76.11	127.7	E 47997
R) R0	221335 221400	24.5N	154.HE	LAND	POUR							76.4	127.8	E 47931
82	2>1400	24.7N	126.5E	LAND				//// 52906				74.54	154.5	E 47918
83	2>1400 2>1400	24.7N	126.4E	LAND	6700	45			EYF	Move	3020	26.14	125.3	E 47927 E 47937
85	221410	24.7N		CHAJ	POUN		5///3	73111				70.14	127.7	E 47937
86 87	221435	24, AN	176.6E	LAND	POUR							26.44	127.81	E 47971 E 47973
88	2>1500 2>1500	24.7N	124.4E	LAND	6n0D	45	5///1	73010	EVE	MUAU	2710	26.1%	127.75	E 67997
89 90	2>1500 2>1500	24.4N		LAHD			21713	52911				74 . HS	125.36	E 47927
91	. >1510	24.7N	124.7E	LAND	PODH		6////	00000				24.34	124.25	E 47+18
92	2>1535 2>1600	24.79	124.7E	LAND	FAIR GOOD							26.44	127.86	E 47771
94	221600	24.84	124.3E	_AND	g., <b></b>	•5	21713	53107	EAF	Munc	3220	76.14	127.76	E 47937
95 96				LAND	FAIR		6////	533ju				24.34	124.26	47918
97	221635	25.NN	126.65	LAHD	FAIH							26.4N	127.88	47971
98 99	2>1700 2>1700	24.74	35.451	LAND	GUUD	44		130	EYE	MOVG .	3520	26.1N	127.76	47317
100	221700	24. 3N	124.3E	LAND			4///3					74.3N 26.1N	124.26	67918 67937
102	221700 221710	25.64		LAND	POUR		21413	53406				24.KN	125.38	67927
103	221735	25.24	124.7E	CLAJ	FATR							70.4N 76.4N	127.85	47+31 47+31
104		24.94	124.2E	LAND			21414 5///3					24.HN	125.38	47927
106	221500	25.UN	126+1E	LAND	ดาบย	45			EYF	HOVA .	3510	76.1m	127.75	47+17 47917
108		24.00	124.7E 124.7E	LAND			6////					M. 45	124.25	47918
109	521300	5c. UN	174.35	しるいり		_	5//12					76.\N	124.26	47918
111	521300	25.14	126.DE	LAND	たつひし	45	21674	501u8	£ 4 F	HOVE :	3510	26.1#	127.75	67937
112	221910 221935	25.1n	124.2E	LAND	POUR POUR							26.00	125.3E	47997 4793]
114	222000	25. 34	174.1E	LAND	Phon		1///3	7341a				26.4%	127,88	47971
115			126 • 3E				6////	73516				74.3N	127.7E	47918
117	525010	25.64	174•2E 174•1F	LAND	POUN		22513	53512				74.84	185.36	47927
	525100	79.54	125.9E	LAND			3///2	73415				26.1≪	127.88	47937
120	222100	24.30	124.28	CHAJ			6////					74.HM	125,35	47927
155	252110 252135	24.4×	124+1E 124+1E	(Av)	POUR POUR							76.4N	127.85	67971
123	222500	25.14	174.DE		- 104		3/1/2	73415				76.4N	127.8E	67931
	525500 525500	25.5V	124.0F 124.9E	しまべり			6/1//	73308				74.3N	126.25	47918
120	222235	24.04	174.1E	LAND	Falk		5/1/3	23514				74,8H 24.4M	125.3E	47927
	222300 222300	26.54 26.54	125.7E 125.9E	LAND			4/1/3					76.1M	127.76	47977
124	222300	74.34	175.48	しゅつ			5///3					74.3N 74.4N	124.25	47918
131	252310 252335	74. Iu	174.1F :	CHA:	FAIN							76,4N	127.8E	47931
132	210000	24.14	175.4E	447			5///4	53030					127.85	
134	210000 21000	24.14	114.1F	(A+iO (A+iO	FALH		5///4	73325				76.1N	127.7E	47977
135	211035	74.74	IZA.IF	(Art)	FAIR							76.4N	127.8E	47971
137	210100	24.64 24.34	1 - C. 4F	(#4) (#4)			4///4					74, HN	125.38	47427
136	230110	24.34	26.0F	A40	4738							76.1M 76.4M	127.7E	47937 47931
1 • u		74.64 ! 74.64	75.75	AND AND	Ph JH		20514	52816				26.4N	38.551	47971
141	5 1057D 5 10500	24.74	175.45	A+3	0.2.14		5///5					76.1N	125.3E	47927 47937
143	540532	2 M . 6 W	1/5.4F	A++)	#1JH #1JH							76.4N	38.151 38.151	47971
144	210100 210100	24.54 1 24.44	24.0F	A7			20224					24.HN	38.35	47427
146	210310	A	126.4E 1	<b>4</b> →7	Phon		5///5	. 3112					127.7E	47937 47931
f	239335	24.14	175.2F	(A*-)	HILLE							76.4M	127.8E	4797

148	234600	24.1N 124.6E	. Aug		
149	5.44.400	24.441 174.AE	LAND POUR	5///5 73115 EVE MOVA 3330	26.1M 127.7E 47977 26.8M 125.3E 47927
151	230410	24.40 124.7E	LAND LAND POUR	>>6 46 53122	24.MM 125.3E 47927
152	240435	24.44 124.4E	LAND FAIR		26.4N 127.8E 47931 26.4N 127.8E 47931
153 154	230500 230500	27.04 124.5E 21.14 124.6E	LAND	1//6 73020	26.1m 127.7E 47977
155	270500	24.44 124.5E	LAND POUR	77679 53008 EVF HAVA 2720	74.88 125.3E 47927 76.38 125.8E 47929
156	210510 さをいすら	24.4% 174.6E 26.4% 174.6E	LAND FAIR LAND FAIR	En and English	26.4# 127.8E 47931
158	231500	26.4N 126.4F	IA-in aniik	EVF MOUR 3320	26.4W 127.8E 47971
159	230700	24. JU 124.4E	LAND FALK 3	n EVF STWR	76.3M 125.8E 47979 76.3M 125.8E 47979
	240700	27.24 124.2F	LAID LAND POJH	30415 72896	24.8N 125.3E 47077
162	270300	74. JN 124.1E	LAND	EYF MNVA 3320 22515 53012	26.3M 125.8E 47029 24.8M 125.3E 47027
163	230300 230300	27.04 124.0F	LÁND POUR	21775 53UOB	24.4M 125.3E 47997
100	211000	27.1× 124.05	LAND PODH	EVE MOVG 1810 EVE MOVG 3320	76.3M 125.8E 47979
166	901162	27.24 123.7E	LAND	11875 52404	26.3# 125.8E 47929 24.8# 125.3E 47927
168	211200	27.24 123.HE	LAND POUR	EYŁ MNYG 3220 Eył Stnr	26.3M 125.8E 47979
169	5 11500	27.2N 123.7E 27.3N 123.7E 27.4N 123.6E	LAHO	11815 53408	26.3M 126.8E 47429 24.4M 125.3E 47927
170	511300	27.44 123.6E	LAND POON	EVE MNVG 3220	26.3M 125.8E 479P9
172	211400	27.5% 123.6E 27.5% 123.5E 27.5% 123.5E 27.7% 123.3E 27.4% 123.3E 24.4% 123.2E	LAND POR	677/5 53312 EVE MOVE 3205	24.8M 125.3E 47927
173	541200	27.54 123.5E	LAND POOR	EVE MOVE 3205	26.3M 126.8E 47999 26.3M 125.8E 47929
175	211700	27.44 123.3E	LAND PODR LAND PODR	EVE MOVE 3430	26.3H 126.8E 47979
176	211400	24.0N 121.2E	LAND GODD .		26.3H 126.8E 47929 26.3H 126.8E 47929
1//	211300	24.14 127.0E	LAND GOUD	5 EVE MOVE 3120	26.3H 126.8E 47999
Fiv	Tr#5	ETY		DOTTO FIRES	
	{7}	-057710P-	INTENSITY NEAREST ESTIMATE DATA (NM)	COMMENTS	
1 2	1=0000 1=1200	9.00 154.0E 11.50 150.0F	015 250 029 250		
			TROP	ICAL DEPRESSION 14	
			•	ATELLITE FIXES	
	118E (7)	FTX P051T[0*6	SCCAA DADSWK CODE	SATFILITE COMMENTS	\$1TE
• 2	141435 170552	12.74 140.2E	PCN h	DMSP35 PSN BSU ON MK IN. CONV ACTIVITY	KGMC
ر ٠	170921	14.74 168.3E 15.30 167.3E	PCN 6 PCN 6	Dw\$p37 Ow\$p36	PHIK Phik
•	171233	14.54 154.7E	PCN 5	DMSP35	PGTW
• 5	172333	17.4N 166.5E	PCN 4 TU-5/0-5 /50-0/24HRs	DMC 11N1 AFG	PGTW
• 1	144513	14.3N 167.0E	Prn 6	D#4p47	KGMC Potu
. 4	191044 191214	14.44 165.9E 14.24 165.9E	PCN 4	DMSD36	PGTW
10	41514	14.9N 165.5E	PCN A PCN B	Duspis	PGTW KGWC
11	141912	19.44 167.6E	PCN 6	DMSP37	KONC
12	141713	15.6N 165.2E 15.8N 164.8E	PCN 3 T1.0/1.0 /50.0/21HR4	DMSP37 DMSP36	PGTW
1+	182536	15.40 164.7E	PCN 6	Decase	PGTw Phik
• 15 16	1#2314 1qu753	14.9N 164.7E 17.7N 163.7E	PCN 6 T1.0/1.0 /00.5/24HRe	DMEPRE	KB#C
• 17	190753	19.14 167.6E	PCN 6	DM4937 DM4937	PGTW KBWC
		14.24 157.6E	PCN 6	Омерал	PSTM
• 20	191117	19.9N 163.8E 29.4N 162.4E	PCN 6 PCN 6	Duspas Duspas	PGTW
21	192127	22.0N 161.1E	PCN 5 T0.0/0.0 /41.0/26HRe	DMEDJY	KGMC PGTM
53	2n0037	22.3M 160.7E	PCN 5	Омер 3 Ф Омер 3 Ф	PGTW PGTW
		<del></del>		- <del></del>	70.4

ATROPART FIXES

FIX NO.	TTHE (7)	FTX POSITION	FLT LVL	70047 HGT	OBS MSLP	44X-SFC-#4D VEL/ARG/R4G	MAX-FLT-LVL-RND ACCRY DTP/VEL/BRG/RNG NAV/MFT	EYE SHAPE	ETE ORIEN- DIAW/TATION	BYF TEMP: (C)	#5N
2	190539	13.5N 104.6E 17.0N 163.9E 19.7N 160.5E	ISOUFT	1165	1007		140 25 060 120 4 10 210 15 110 35 5 5 180 15 230 10 5 60			.25 *24 30 8c *5+ *5+	1 3

SYMPOTTO FIRES

NO.	(7)	POSITION	ESTIMATE	NEAREST DATA (NM)	COMMENTS
. 1	1 A 0 0 0 0 1 7 0 0 0 0	12.0N 168.0E 13.0N 160.0E	15 15	300 300	

### TROPICAL STORM KEN

### CATELLITY FIRES

FIK NU.	₹1ME (7)	F1x +0511100	*Cu34	UV774K CON	F	547611 178	CJanr	NTS		\$116		
• 1	312136	25.74 ] 19.06	. hc# 2			005011	[N]   JdS			PGI#		
ے ہ	010115	27.44 1 11.46	Pry 7	T1.0/1.0		Dadota				PGI#		
3	010500	24.04 193.9F	Pry 5	11.1/1.0		ひゅんちょうひゅんしょう	1411 345			PG1#		
,	011016	24.34 132.6F	Prun	1		D450 17	1411 205			PGT#		
b	011016	74.34 [13.7E	Pr4 4			DRZh 11				ROOM		
	411514	25.14 1 17.5E	Pry 4			Ordhin				PGT		
9	011320	24.24 132.7E	Pry 7			DMCD IV				Pale		
ن ا	012115	27.44 1 17.2E	Prv	T1.0/1.0 /5	0.4/2048					PG1d PG1d		
11	020020	24.74 131.7E	Pry 3		440760.00	DWED IN				PGTd		
15	リクノリラう	27.44 1 11.4E	Pry 1			0448 14				P61 #		
13		24.0v 132.1F	Pry 3			Bech 12				P61#		
15	020142	24. 24 132.2E	Pry 7	71.0/1.0 /5	0.0/24##	Dachit Dachit				#004 #189		
16	021305	27.70 1 11.1F	PCHT			045-16				PG1#		
17	021461	24.04 131.7E	Prv 5			C=<0 12				PG1		
		24.44 130.ME		11.5/1.5		Juer 17	[N] ( 365			RPMK		
14	024055	21,54 110,7E	Pry B	16.5/2.5-/0		044011				9614		
• 21	0.0124	24.24 120.55	Pru i	10.3/2.5-/0	1 . 3/C/NR	GAKA 12				PG Tar		
25	030123	21.24 120.HE	Pry 7			044614				Pola		
53	115060	21.1- 179.46	Pry 5	13.0/7.0-/0	2.0/2.HH					#00 t		
• 24	0.40511	- 73.930   30.0 [E	Prys	13.073.0		Om . n 10	[4]1 )05			RKS()		
25 26	020435 020436		Pry n Pry n			Duchi:				#00 4		
• 27	031117		Pry			044511				PC I W RODY		
28	445110	31.60 131.0E				DWSDIA				P61#		
	031317	31.79 131.9E	Pr4 s			0115034				RPMK		
ن (ز ا د	531316		PCY			Unch				PGTW		
	031404	37.0N 131.5E 31.7N 131.2E	Pru 3 Pru 5			DAKE 14				PASO Palm		
دُدُ	031405	31.4N 111.3F	Prv n			000015				ROUM		
34	031546	32.14 131.36	Fru n			Dade 17				ROUN		
35	031546	32.5N 131.7E	Pry 7			0440 14				RKSO		
36 32	012035					OHED 17				RODN		
36	032035	37.0% 192.7E 37.1% 192.3E	Prv 4			044011				PGTW		
	072344	33,4N 133.4E	Pru i	12.5/2.5-/0	A / 2 9 M P 4	OMEDIA				AK SO RPMK		
40	072344	37.94 137.1E		11.0/2.0 /w	. S/ZAHAS	Despin				9614		
*1	040155	34.34   34.45	PC4 .			044014	FINALEH n	n į		PGTW		
						13CH4F1 +1	xe 5					
FIX NO.	TIME (7)	FIX POSITION	۶ ( ۱ ۱ <b>۷</b> (	70043 385 4)2# 10h	MAX-SFC. VEL/4RG/	BAG UINT	.   1 -   AP - 4AU	ACCRY NAV/MFT	E T È SMAPE	PATTAL/METO	EYF FEMP	(C) 45A PVRKT NO.
1	012105	25.44 132.1E	15:0F	998	40 n30	10 120	13 040 45				.25 •25	, ,
2	0>2132 0>2132	27.04 131.0E 24.34 130.4E	PADAN PADAN		50 700 15 030	50 220 50 130	36 050 12n	5 20 2 5	CINCILLAR	50	-10 -10 -10	
	020725	30.34 130.HE	70044	2484 488	50 090		65 110 41				5 - 5[+ 11+	
5	010713	30.74 130.78	7.10MB		50 180	10 210	55 140 40	2 14			114 -12 - 2	9
					0	A JAN FTRES	i.					
Fix Nu.	TYME (7)	F11 P051T10N	RADAS A	EYF Crit Shafe	EYE		COUE		COMMENTS		HADAR POSTTION	417F
	012000	24.0N 130.5E	LAND			65///	50114				28,4m 127,5E	47909
2	020700	24.7N 131.2E	LAND			44//1	11111				28.48 127.5E	47909
ś	00200	35.161 NF.05	しかりり			48					28.4N 129.5E	47909
•	020900	27.1N 131.1E 27.3N 130.9E	LAND			A5//L A5/// A5/// A5///	53413				28.4M 129.5E	47909
,	021000	27.3N 130.9E	ניויא. האאו			45///	53113				28.4N 129.5E	47909
ĭ	021500	27.24 130.08	CHAJ			45///	25911				78.4N 129.5E	479ng
8	0 > 1 300	24.94 130.6E	LAND			65///	5180s				78.4H 129.5E	2969
, 4	021400	30.0F1 W1.75	LAND								28.4M 127.5E	A7909
	021500	27.2N 130.5F	LAND			65///	53411				28.44 129.56	47969
12	021500	27.44 130.4E	CAND CAND			65/// 65///	53511				78.4M 129.5E	47909
13	021700	37 20 130 ht	1 4			48///	2011V				28.4M 129.5E	47909 47909
14	021700	27.94 130.5E	LAND			45///	53608				28,44 )29,5E	*1000
io	022100	34.0E1 PC.PC	LAND			45/// 45/// 45/// 45/// 45///	30211				28.4H 129.5E	47909
	025500	24.44 130.7E	LAVO			69///	50113				28.4H 129.5E	47909
17	024300 02000	24.4N 130.0F	LAND			65///	53308				28.4N 129.5E	47909
		24.44 130.4E	LAND			A5///	53319 63212				78.4H 129.5E	2000
žó	D-0100										cu 124.3E	47909
	0-0100 040200	37.24 130.28	CVAJ			65///	53513				28.4M 122.4F	
	n 10200 n 10300	27.24 137.2E	ドサペン ドサペン			65///	53513 50210				28.44 129.5E 28.44 129.5E 26.44 129.5E	47909
22	0.0200 0.300 0.400 0.400	27.24 130.2E 21.44 130.3E 21.44 110.4E	じゅうり しゃくり しゃんり			65/// 65/// 6///3	53513 50210 5///				28.4M 129.5E	67909 67909 67909
23	710200 710300 710400 710500	27.24 130.2E 21.44 130.3E 21.44 110.4E	じゅうり しゃくり しゃんり			65/// 67// 6///3 65///	53513 50210 5/// 50122				28.4% 129.5E 30.6% 131.0E 28.4% 129.5E	47909 47909 47909 47909
22	0.40200 0.40300 0.40400 0.40500 0.40500	27.24 137.2E	LAV9 LAV9 LAV9 LAV9 LAV9			65/// 65/// 65/// 65/// 67//3 65/// 67//4	53513 50210 5/// 50122 50216				28.4M 129.5E	67909 67909 67909

	0.51400	31. IN 111.5E		POUH		32.14 131.55	47454
21	0.41400	33.44 131.3E			55/41 50316	33.44 130.3E	47486
28	0 11455	30.11 PO.ºc£		PYUH		32.1m 131.5E	47954
54	006160	32.0v 171.5E			44//1 5////	34.3K   132.6E	47792
30	071500	31. 34   31.5E	LAND		55/11 50319	33.4W 130.3E	47406
31	071500	32.14 131.NE	CPAJ		K5//1 50211	34.5k 1 Mt. 4F	47792
32	011500	32.14 131./E	LAND		55/41 50319	33,4H 130.3E	47486
وو	011502	32.34 131.6E	LAND	PJUH		32.1m 131.5E	47454
34	031700	12.34 131.7E	LAND		55/// 5////	13.2H 131.2E	47409
35	031700	32.34 131.7E	LAND		21601 50316	74. #N 132.6E	47792
36	031700	32.44 131.4E	LAND		20401 50222	33,4W 130.3E	47406
37	D31701	32.44 131.7E		POOR		32.1N 131.5E	47954
3 8	011755	32.7N 132.0E	LA-10	FAIR		12.14 131.5E	47454
39	UUELFO	32.4N 131.9E	IAND		45//1 50416	34.5m +32.6E	50114
40	031900	32,44 132.0E			55/// 50424	33.2N 136.2E	47909
+1	0.0615.0	32.44 131.9E			20541 50111	13.4W 130.3E	47406
42	648160	32.4N 132.2E		FAIR	****** J	73.7N 131.0E	47440
4.3	031300	32.90 132.1E			/1371 50322	14_3m 132.6E	47792
44	011700	32.9N 132.1E			55/// 50319	33.2M 134.2E	17409
40	031355	37.24 132.3E		POUN	44/1/ 40271	33,7M 131.0E	47440
46	0.45000	33.14 132.4E		P-10N	55//1 50516		
47	032000	33.14 132.2E			55/// 50316	34,34 132,68	•7792
						33.24 134.2E	7999
+ 6	0.44100	31.34 132.4E			24411 50316	34.3M 132.6E	47792
44	035100	17.24 137.4E			55/// 50411	33.2N 136.2E	47999
50	0.35500	37.4N 172.HE			2/4/1 50516	34.3N 132.6E	47792
51	035500	31.3v 132./E			55/// 50619	33.2N 134.2E	47499
52	0.32300	31.7N 137.7E			55/52 5052/	34.34 132.6€	47792
53	0 15 300	31.44 137.1E			44/// 5052/	33.2H 134.2E	47499
54	012300	33.74   37.1E			44/01 ////	34,6≈ 135.6£	47773
55	044000	37. IN 137.4E			55/50 50522	34.6N 135.6E	47773
56	0.40000	33.94   33.5E			54//2 50616	34.3N 132.0E	47792
57	044000	31,4N 137.6E			65/// 50532	73.2m 134,2E	47499
58	040500	34.7N 133.4E			6/1/2 5////	34,3N 132.6E	47792
59	040900	34.5N 174.2F			2294/ 50722	35,3M 138,7E	47439
60	040300	34.2N 135.1E			224112 40415	36,2N 136,1E	47705
61	040300	35. ON 135.5E			7291/ 70422	35.JN 138.7E	67639
65	041000	34.14 135.7E	( A-ID		229H/ 70519	35.34 139.7E	47539
63	041000	74.14 135.6E	(A+i)		11772 50515	36.2€ 135.15	47705
64	041000	36.14 135.6E	LAND		45841 5042U	35,2N 137.0E	47536
65	041100	34.44 1 14.2E	LAND		A5AA/ 50525	35.2M 137.0E	47536
66	041100	36.24 1 14.0E	LAND		35/0/	37.7H 135.8E	47572
61	044100	34.24 136.1E			11712 50720	36.2M 135.1E	47705
68	001100	36.64 136.6E			A584/ 50527	35.2M 137.0E	47436
69	005140	30.54 136.0E			21A46 5003U	36.2N 135.1E	47705
70	041200	34.44 134.7E			ANN 31 50637	37./W 139.8E	47572
71	041300	34.94 137.2E			3581/ 50625	37.7m 139.8E	47572
72	041300	36.4N 117.2E			51742 50638	36.4M 135.1E	47705
73		35.50 174.HE			127// 50330	35.3N 133.7E	47539
•		,			30330	35,34 1351.1	4

### TYPHOON LOLA

### SATELLITE FIXES

Flx	FTME	FIX					
NU.	(7)	20511100	#CC44	DAJSWK COUE	SATFIFTE	CJAMENTS	SITE
1	021120	21.94 151.3E	Pry 5		DHEPAN		PGTW
2	021545	22.14 151.0F	Pry 5		DMCD35		PGT⊯
3	022055	22.91 150.9E	PCN 5	T1-n/1-0	DMSP37	INIT JdS	RPMK
4	U22056	27.40 151.1E	Pru 6		Dusp 17		₽GT⊯
•	025551	22.54 151.3E	PCM 6		D45034		PGT#
6	030036	22.34 151.1E	Prv b	15.0/5.0	Dwdb sa	INII 348	PGTW
1	E510F0	22.94 151.3E	PCN 5	Ti-0/1.0	DMCPIS	INIL Sec 11NI	RODY
8	020123	21.04 150.7F	Prw 5	T2.0/2.0	0~4634	1N11 3d5	RKSO
*	070123	22.54 151.1E	Pry b		0meb 12		PGTW
10	010336	22.74 150.7E	Prv 5		Duebas		PGTW
11	071103	23.04 150.7E	Pru 5		DMEDIA		PGT⊯
15	071136	30.001 WI.FS	Pry 5		Dadh 10		PGT⊯
13	N 71405	22.5% 150.5E	P(4 7		Dweb 1e		RKSO
1+	031405	21.3v 120.4E	Pry 5		Dadb 12		PGTal
10	にものろにり	21.5H 144.0E	Prw		DMSP37		RODY
16	972035	21.24 144.5F	Pry 6	T3.0/3.0 /01.0/20HR	c Duchil		PGT w
17	072503	21.34 160.1E	PC4 4		AFRPWO	BEGINAING OF FYF	PGTW
18	044017	21.44 14A.RE	Pr.N. 3		Dechia		PGT₩
1.4	044104	23.44 140.05	Prw 5	**************************************	C D#5P35		RODN
20	040105	23.74 164.8F	Pry 3	73.5/7.5 /N1.5/2.HR	C DHEPTE		RK50
21	040105	23.44 148.ME	Pry +		D#2632		PST∎
22	040 +16	24.14 147.HE	PCN 3		045037		PGT#
23	041117	24.34 147.7E	PC4 5		Dwdb 44		PGT₩
24	041226	24.4N 147.5E	Pry 3		DMSP3A		PGTW
25	041346	24.54 147.4E	Pry 3		0446174		PGTW
26	041346	24.74 147.5E	PCN .		Dech te		RKSO
21	041346	24.74 147.0E	Pry 3		045035		RODY
28	044015	74. 3" 166.7E	PCN L		DHCH 17		RODN
24	044015	74.3" 144.7E	Prv i	15.0/5.0 /02.0/24HR	s Bachil		PGTW
30	042327	25.14 144.7E	Pry I		DMCD34		PGTW
16	046358	25.54 146.4F	Prv 2	15.0/5.0 /112.0/23HH	C Duchia		RODN
35	04235B	27.24 146.5E	PCN 1		Dach in		PGT
33	050045	25. 14 144.5E	PCY 1		045035		RODY
34	050046	25. 24 166. BE	PCN L	T4.5/4.5 /01.6/24HR	C D45015		RK50
ct	050046	24.34 144.5E	Prv I		D=40 14		PGTW
36	050956	24.00 144.4E	Pry I		Ducu 7		PGTw

37	041208	25. IN 146.5E	PCN I		DHEPIA		PST
3#	051540	26.3N 146.6E	PCH 1		Duspaq		PGTU
39	051328	26.5N 146.4E	PCN 1		Duspis		PGTW
40	051328	26.2N 144.3E	PCN 2		Duspis		RODN
41	051955	27.04 146.3E	PCN 2		DMSP17		PETW
42	052309	27.3N 146.6E	PCN 1	15.0/5.0-/50.0/21HR<	DWSPRA		PGTW
43	850040	27.5N 146.6E	PCN 1		DUSPIS		PGT#
• •	060121	27.54 146.6E	PCN 1		Duceio		PSTW
45	151040	27.5N 144.5E	PCN 1	14.5/4.5	Duchid	INII DOS	RPHK
46	060835	27.7M 146.2E	PCN 4		DUSPRE		PGTw
47	061150	24.34 144.0E	PCN 1		DHEPIN		PGTu
48	155190	24.84 144.2E	PCN I		045039		RODN
49	041551	28.74 146.2E	PCN I		Duspay		PGTW
50	061309	30.44 NF. NS	PC4 1		DRZ5 52		PGTW
51	041935	29.54 144.0E	PC4 2		Dusp 17		PGTH
52	070007	29.74 146.2E	Prn 2		044634		PSTU
53	070101	30.14 146.4E	PCY I	T4.5/4.5-	DUSPRY		RODN
54	079102	30.04 146.4E	PCH 3	T3.5/4.5 /W1.5/26HRS	Dechia		PGTu
55	070957	30.7N 146.5E	PCN 1		D45P 17		PGTw
56	071137	30.9N 146.4E	PC4 1		Diadh Jy		PGTW
57	071202	31.74 149.2E	PC4 5		Dade sa		RODN
58	071202	31.74 147.0E	PC4 5		ひゃんりょう		PGTw
59	071432	32.04 147.1E	PC4 3		DMENJE		PGTW
60	072056	33.7N 14A.2E	PCN 3	T2.0/3.0 /W1.5/20HRS	DUSURT		PGTW
61	072233	34.04 148.6E	Prn 3		Dazh sv		PGTW
62	040043	34.24 14A.9E	PCN 3	12.5/3.5 /WZ.0/24HRG	DMZGSA		RODN
63	0.00043	34.74 149.HE			Dadasa		PGTW

### ATRCHAFT FIRES

	TTHE (7)	FTX POSITION	FLT I,VL	70043 461	OBS MSLP			\3 46 -=40	MAX-						EYE Shape	EVE ORIEN	M OUTY TAY DEVEST	40.
1	031932	23.50 109.7E	70046	3044					0.40	45	270	15	H	4			+16 +13	•
Ž	036046	23.5N 149.4E	7 n 0 мH	3001	990	45	090	20	170	49	080	40		2	ELLIPTICAL	25 20 170	+11 +15 +13	4
3	040909	24.9H 14#.1E	7 n u m m	2717	978	65	120	15	360	71	320	30	2	4	CINCILAR	15	-04 -12	5
•	041913	24.4N 147.0E	700MH	2911		35	270	èο	290	50	200		5	- 5			.17 + 6	6
ŝ	044118	25.14 1.6.ME	74046	2/51	965	75	₹50	15	020	68	330		•	10	CINCHLAR	30	•11 •15 • B	•
	050504	25.74 146.6E	70044	2743		90	300	10	310	A7	230	10	3	5	CINCHLAR		-19 +10	7
,	050948	24.44 146.5F	70040	2/51	959		210	50	250	46	100	10	2	4	CINCHLAR	24	+12 +13 +12	1
8	051743	27.04 146.4E	7 n 0 ч н	2065		45	250	50	340	45	300	Š٨		4	ELLIPTICAL	15 12	• 23	8
ÿ	052120	27.14 146.5E	7 i) 0 mm	2056		75	070		070	45	300	30		4	ELLIPTICAL	17 12 030	·14 ·17	8
10	040610	27.9N 146.5E	TOUMH	2683	953		280		949	71	240	50	2	4			•1 <del>3</del> •13	9
11	040850	24.1N 146.4E	7 2 0 MH	2744	460	50	480	50	ING	72	940	94	2	5	CIRCULAR	20	+17 +17 +15	4
īž	061943	24.74 146.3E	70040	2869		75	080	5	050	60	330	30	5	0	CINCHLAR		-14 +12	10
ĨĴ	044137	29.74 146.2E	70000	2840	984	75	080	5	230	60	1/0	30	5	10	CIRCILLAR	3n	+11 +15 +14	10
14	070537	10. IN 146.4E	7 7 0 MH	2907		50	260	50	020	51	910	30	4	Ð			-15 +12	- 11
is	070929	31.24 146. RE	70048	2426	974	70	040	10	A 19 11	77	1/0	65	,	4			. 4 .15 .15	11
16	071995	31.24 147.9E	70048	2442			120		230	57	120	3 n	4	,			•19 •12	12
		33.54 140.1E	70048						170	49	060	154	4	~			-14 -17 -12	15

### TYPHOON MAC

### SATELLITE FULES

FIX NO.	TIME (7)	FTR POSTTION	ACCRY	DAUSTR COUE	SATFII ITE	COMMENTS	SITE
1	140008	11.4w 134.5E	Pru 5	10.0/0.0	Dadhav	Sec (INI	PGTW
5	140030	11.9N 13A.5E	PCN 5		Ducasa		PGTW
,	140917	11.5N 134.9E	PCN 5		DWSP36		PGT# PGT#
;	141250	11.9N 134.7E 17.0N 134.2E	PCN 5		045935		PGT
6	142157	12.?N 133.6E	PC4 5	TU-0/0.0	DMSP37	INI OUS	RPMK
7	142350	17.74 133.0E	PCH 5	71.0/1.0 /01.0/24HR	AFGPMO		PGT
*	151037 151232	12.9N 131.6E	PCN 6		D#4P37		RPMK PGT#
• 10	151252	12.5N 130.0E	PCN 5		Dechido		PGT
11	151346	12.24 131.9E	PCN h		Duspas		ROOM
12	151527	12.2N 131.0E	PCN 5	TU.5/0.5 /00.5/24HRS	045P35 045P37		RODN RPMK
14	162137	13.04 129.6E	PCN 5	10.5/0.5 //0.5/24/10.5	Duspar		PGTH
15	142332	13.3N 179.0E	PCN 5	T1.0/1.0 /50.0/24HRS	AFRPUO		PGT
16	140133	13.5M 128.8E	PCM 5		DMCD34		PGIU
17 18	160227	13.4N 129.7E	PON 5		DMSP17		PGT #
19	141017	13.9N 127.0E	PC4 6		DMSP37		RPMK
• 20	141514	13.3M 124.3E	PCW 5		DMGP3A DMGP37		PGTW PGTW
55 51	162117 170114	14.14 125.2E 13.64 125.4E	PCN 6 PCN 5	12.5/2.5 /01.5/26HRG			PGT
23	170114	13.6W 125.8E	PC4 5	12.0/2.0 /01.5/24HRS	Duchia		RPHK
24 25	170757	13.94 125.3E	PON 5		D44037 D44039		PGTW
26	171355 171356	13.3N 125.0E	PCN 5		D=<534		RODN
27	172238	13.94 174.4E	PCN 6		D45037		RPMK
26	LAU03B	17.54 127.8E	PC4 5	T3.5/3.5-/01.0/23HRS	DMCD3A		PGT
29 29	190237	13.74 127.5E 13.44 127.4E	PCN 3	T3.5/3.5 /N1.5/24HRS	December 19	INIT Das	RPMK RODN
31	141118	13.9N 122.3E	PCN 4	130373.	DMSD37	•	RPMK
32	191118	13.34 172.7E	Pru 6		DHSP37		RODN
33 34	141320 Pal336	13.24 122.2E	PCN 5		Ducase		PGT d RPMK
35	141337	13.34 172.2E	Pru 5		Dadosa		PGT#
36 37	145518	13.74 121.5E	Pry 6		045P37		RPMK PGTW
38	144518	13.54 121.4E	PCN 6	12.5/3.5+/W1.0/24HR			PGTW
39	190218	13.9N 120.7E	PCN 5	12.5/3.0 /W1.0/24HRS	DMCP39		RPMK
• 41	100518	38.051 NS.FI	PCH 5	T2.5/3.5 /wl.0/24HR9	PF92MQ :	PSUL 240 CHTH AT 153N 12U6E	ROD4 RPMK
45	191058	13.74 120.6E	PCN 6 PCN 5		Duce 27	Lage Can Call at 1224 15085	ROUN
• 43	101305	17.5N 11A.8E	PCN 5		DHED 14		PGTW
• 44 • 45	191313	17.74 119.6E	PCN 5		0mcb3a 0mcb3a		RODN RPMK
• 46	191318	13.54 11A.AE	PCN 5		DMCB34		PG [#
• 47	192157	14.5v 119.4E	PCN 5		045937		PGTW
• 46	192157 192157	14.7N 117.8E	PCN 5		DMGP37 DMGP37		RODY
50	200144	16.5N 118.8E	Prw 5	T1.0/2.0 /W1.5/24HR			ROUN
51	200159	14.8W 118.9E	PCN 3	72.0/2.0 /W0.5/24MR9	PEASES :		RPMK PGTd
52 53	2n0159 2n1038	16.9N 11A.RE 17.5N 11A.5E	PCN 3 PCN 5	T1.5/2.5 /w1.g/24HR4	D#5937		PGTW
54	201244	17.50 137.7E	PC4 5		DMSP3A		PGTW
55 56	201439	17.74 117.5E	PCN 6		Dweb 34 Dweo 34		RPMK RODN
57	2n1440 2n2137	17.44 11A.3E	PCN 5		DMSP37		PGTM
58	202319	18.44 117.7E	PCN 5		Dagp 17		ROUN
59	510114	14.94 117.3E	PCN 5	T1.0/1.0 /50.0/24HRS	PF92MG :		RODN
60 61	210126	18.7N 117.7E 19.9N 117.2E	PCN 5	T1.0/2.0 /W1.0/24HR			PGT#
• 65	210321	19.84 114.8E	PCN 5		DHSP79		RODY
63 64	211018	19.44 117.4E	PCN 5		Duspa7 Duspa9		PGTW
65	124115	19.4N 117.1E	PCN 5		DMCD30		RODA
. 66	212258	19.64 114.6E	PCN 5	12.0/2.0-/01.0/24HR			RPMK
67 68	2:2258 2:0108	20.4W 114.4E	PCM 5		DMSP37 DMSP34		RODN RPMK
69	520305	20.9N 114.4E	PCN 5	13.0/3.0 /02.0/25HR			RODY
70	220305	20.94 114.1E	PCN 5	= · · ·	Decbio		RPMK
71 72	551405	20.3N 114.8E 20.4N 114.9E	PCN 5		045P37 045P39	PON BOU ON EXTRAP OF CLO LINFS	RODY
73	521405	21.34 116.ZE	PCN 5		DMCP39		RPHK
74 75	272538 210050	21.4N 114.7E	PC4 5	12.0/2.0 /50.0/24HR9	DMEPRT DMEPRE		RPMK ROJN
76	210050	21.4N 114.5E 21.5N 114.5E	PCN 5	T2.5/3.0 /WU.5/23MM	AFGPMQ :	INIE 205	PGTH
77	210243	21.5% 114.1E	PCN 3		044540	-	RODY
78 79	210243	21.9N 117.9E	PCN 5		044474 04447		SPRK SPRK
#0	541116	22.2N 117.4E	PCN 6		Dusp 17		9004
81	241342	39.FII W1.55	PCN 5		Duspag		RPHK
88	211343 211343	27.4N 117.3E	PCH 6		Dweb30		900M PG 1 W
84	212218	27.5N 117.8E			Duspay		9KS0
85	240031	22.54 112.9E	PCN 5	91.5/9 8 /U1.6/24HP6	Decade		RPMK RODM

### ATROMAFT PIXES

F14 NO.	) 1ME (7)	FFX POSTITION	デレ7 ( V(	70042 HGT	28S MSLP				44 X-						EYE SHAPE	PAE OHIEM-	175 TEMP (C)	uSN un
1 2 3 5 5 6 7 10 11 12 13	141436 142042 140929 244009 244904 241433 242151 214619 214404	17.94   118.18   14.14   114.18   14.14   118.08   14.25   117.58	7.0 MH 7.0 MH 15.0 F1	3054 3056 3056 3057 3067 3067 3067 3067 3067	995 984 994 1005 1000 997 998	50 +0 50 50 +0	050 110 360 360 310 350 070	75 75 70 70	170 160 160 160 330 330 040 130 150 150	58 52 65 45 27 28 31 60 24 20	300	40 30 50 20 50 20 42 60 45	4 4 7 7 7 7 4 4 7 4 4 10	5 4 10			*19 *15 *11  *13 *11  *10 *14 * 8  *11 *15 * 9  *11 *11  *10 *11 *11  *11 * 13 * 8  *12 *16  *18 *15 * 9  *25 *26 *28	2 4 6 7 7 9 10 12 14 15 15
14	212100	21.04 116.IE	1500F					A yAs	FIXE	s								10

F14	T1ME (2)	F11 P051110n	PAGAN	ACCHY	EYE SHAPE	EYF DIAM	BANNS-CODE	COMMENTS	MADAR POSTTION	411F
1	171959	13.7m 1/4.3E	ACFT							54495
ż	172300	13.84 123.9E	LAM')				10210 ////		14. IN 123.0E	98448
ī	172300	14.54 123.5E					4/11/ ////		16.3W 120.6E	98321
	1 40 900	11.34 122.VE	CHAJ				202// 52110		14.1m 123.0E	98448
>	141030	17.74 172.46	CAND				25/// /////		22.34 114.2E	45005
ь	1=1100	19,44 127,88					1044/ ////		16.3m 120.6E	96321
7	101100	11.7m 122.9E					25/// /////		16.3M 128.6E	9832[ 9832]
	141200	13.54 122./8	CHAIL				1/54/ ////		16.3M 120.6E	98371
10	1#1500	11.64 177.7E					1056/ ////		16.3M 120.6E	98371
11	191530	11.50 172.38	LAVO				302// 727//		14.IN 123.0E	96440
įž	INLOUG	11.44 172.5E	A-10				1173/ 52709		16.3m 120.6E	98371
13	102145	13.44 171.0E	LAND	FAIH	CIRCULAR	15			15.2N 120.6E	98377
1 .	106530	11,44 171.5E	LAND	FAIR	CIRCULAR	15			15.2M 120.6E	98327
15	14555	13.44 181.4E	LAND	FAIR	CIRCULAR	15			15.20 120.46	98327
16	101505	15.14 120.55		Paúñ Paúñ	CIRCULAR	•			15.20 120.6E	98327 98327
10	101300	16.24 120.4E 14.76 120.2E		PHON	CIRCULAR	7	41111 11111		16.3m 120.66	98371
14	191335	15.3% 120.0E	CAND.	POJH		5	4,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		15.20 120.6E	98327
20	191400	15.04 120 DE					4//// /////		16.3N 120.6E	98321
51	142200	14.04 119.4E					104// 104//		16.30 120.6E	98371
55	200000	14. 3v 110.0E	CHAID				105// /////		16.3M 129.6E	98371
23	200040	14.90 119.5E	CHAI				1266/ 52912		16.34 120.6E	98371
2+	200100	14.4H 114.ME	FWN				1051/ 53218		16.3m 120.6E	96371
<b>45</b>	200100	17,5% 119.5E	FWD CMAD				106// 5///		16.3M 120.6E	48371 48371
26	540300 540130	14.74 119.7E	LAVD				1051/ 630//		16.3m 120.6E	96371
58	200500	17.04 114.0E	LAND				11119 19901		16.3N 120.6E	96321
29	200.00	17.24 114.5E					11172 5////		36.3M 120.6E	96371
30	200500	17. TV 118.7E	LAND				1068/ 5////		30.051 ME. 81	98371
31	200900	17.30 114.7E	CAND				1061/ 5////		16.34 129.6E	<b>96371</b>
32	201200	17.44 118.4E					4561/ 6////		16.30 120.66	98321
33	220200	20.44 115.HE					41112 11111		22.3m 114.2E 22.3m 114.2E	450R4 450R4
3+ da	2>0200	20.50 315.4E	LAND				65/1/ ////		22.3M 114.2E	45004
36	220900	20.94 115.9E	LAVID				A0/// /////		35-411 ME.SS	45884
37	2>1200	20.94 115.5E					60/// /////		22.3M 114.2E	45004
38	2>1300	20.94 115.5E	CHAJ				50913 5//00		72.3M 114.2E	45884
34	2>1400	20.94 115.5E	LAND				40913 54400		22.3M 114.2E	45644
40	5><100	21.24 114.7E					40523 53100		35.94 114.SE	45004
41	525300	21.44 114.0E					40523 53007		25.34 114.25	45004
+2	230000	21.40 1)4.5E					40573 53061		25.34 114.2E	45084
4.3	230200	21.4N 114.3E					5///2 52906		35.411 06.55	45004
45	230500	21.74 113.8E					5///2 52996		35.34 114.55	45004
4.5	210700	21.74 117.7E					5///2 52903		22.34 114.2E	45004
•7	231500	21.9m 117.9E					MIII2 11111		22.3N (14.2E)	45004
4.0	211500	22.24 113.0E	LAND				11111 11111		25.34 114.5E	45884
4.9	211400	22.3w 113.3E					A//// /////		22.34 114.25	45084
54	535000	55'3M 113'9E					40415 ////		22.34 114.2E	450N4 450N4
51	212100	22.3M 113.0E					\$1111 11111 \$1111 11111		25.34 114.26	45004
52 53	540000	27.34 117.0E 27.34 112.7E					31111 11111		72.3m 114.2E	45004
54	240100	27.34 117.6E					3/1// ////		22.3m 114.2E	45004
55		27. 34 117.6E					6/1// /////		35.411 ME.SS	45685
•							•		-	

### TROPICAL STORM NAMCY

### SATELLITY FERES

100216   18.70   112.0E	FIX NO.	TTME (7)	FTX POSITION	ACCRY	UVTRAK	CODE	SATFII ITE	COMMENTS	SITE
1   1   1   1   1   1   1   1   1   1		102218	10 20 111 95	9au 4			Ovenal		9974
3 100218 1 18.4m 111.2E PCN 5 73.0/3.0 DMCR34 4 100218 1 18.4m 111.0E PCN 5 73.0/3.0 DMCR37 5 101058 1 18.4m 111.0E PCN 5 73.0/3.0 DMCR37 6 101058 1 18.4m 111.0E PCN 3 DMCR37 7 101058 1 18.2m 110.7E PCN 3 DMCR37 8 101059 1 14.5m 110.5E PCN 4 DMCR37 8 101059 1 14.5m 110.5E PCN 4 DMCR37 8 101059 1 14.5m 110.5E PCN 4 DMCR37 8 101059 1 14.5m 110.6E PCN 7 3.0/3.0 /PC.0/21NRC DMCR37 8 101059 1 14.5m 110.0E PCN 6 PCN 7 3.0/3.0 /PC.0/21NRC DMCR37 8 11 201144 1 14.0m 104.E PCN 7 3.0/3.0 /PC.0/21NRC DMCR37 8 12 200340 1 10.4m 104.EE PCN 7 3.0/3.0 /PC.0/21NRC DMCR37 8 PCN 7 3.0/3.0 /PC.0/24NRC DMCR37 8 PCN 9 P									
100216   18.70   112.0E					*1.641.6			THIT DAG	RPHK
\$ 101058 18.4% 110.1E PCN 4 6 101058 18.4% 110.7E PCN 3 7 104859 14.5% 110.7E PCN 3 8 101059 14.5% 110.5E PCN 4 9 104338 18.6% 100.5E PCN 4 10 102339 18.6% 100.5E PCN 6 10 102339 18.6% 100.5E PCN 7 11 201146 18.6% 100.5E PCN 7 12 201040 10.6% 100.6E PCN 7 13 201219 18.7% 100.2E PCN 8 15 201040 18.6% 100.6E PCN 9 16 201040 18.6% 100.6E PCN 9 17 201040 18.6% 100.6E PCN 9 18 202319 18.5% 100.6E PCN 9 18 202319 18.6% 100.6E PCN 9 18 202319 18.6% 100.6E PCN 9 20 210126 18.6% 107.6E PCN 9 20 210126 18.2% 100.2E PCN 9 20 210126 18.2% 100.2									
	- 5				1307300	,		1411 043	RPMK
7 101459 10-14 11n-6E PCN 3 8 101499 14-59 11n-5E PCN 4 9 102338 18-64 100-5E PCN 6 10 102339 18-64 100-5E PCN 6 11 20140 110-6E PCN 9 73-0/3-0/02-0/21MRC 12 200340 10-64 100-6E PCN 9 73-0/3-0/02-0/21MRC 12 200340 10-64 100-6E PCN 3 PCN 9 13 201219 18-7-1 100-2E PCN 9 15 201349 11-64 100-6E PCN 9 16 201400 18-64 100-6E PCN 9 17 202319 17-54 100-3E PCN 9 18 202319 18-24 100-6E PCN 9 19 20108 17-64 107-6E PCN 9 20 210126 18-24 100-2E PCN 9 21 210321 17-75 100-3E PCN 9 22 210321 17-75 100-3E PCN 9 23 21139 14-14 100-1E PCN 9 24 211421 17-94 107-6E PCN 3 25 211421 17-94 107-6E PCN 3 26 212258 17-64 107-6E PCN 3 27 212258 17-64 107-6E PCN 3 28 200302 17-54 107-6E PCN 3 28 200302 17-55 100-6F PCN 3 28 200302 17-55 100-6F PCN 3 30 201339 16-64 100-6F PCN 3 31 201339 16-64 100-6F PCN 3 31 201339 16-64 100-6F PCN 5 32 20102 17-55 100-6F PCN 5 31 201339 16-64 100-6F PCN 5 32 20102 100-6F PCN 5 31 201339 16-64 100-6F PCN 5 32 20102 100-6F PCN 5 33 20102 100-6F								FYF BANDING POSSIBLE	RODN
								CIC CONTINUE CONTINUE	RPHK
102338   18.6 \( \) 100.6 \(									KG#C
10 102339 10.0N 110.0E PCN 9 73.0/3.0 /70.0/21MRC DMCD34 RDD 12 200340 10.4N 109.8E PCN 9 DMCD34 DMCD34 RDD 13 201219 18.7N 109.2E PCN 9 DMCD37 RDM 13 201219 18.7N 109.2E PCN 9 DMCD37 RDM 15 201439 14.6N 108.6E PCN 9 DMCD37 RDM 16 201439 17.5N 109.3E PCN 9 DMCD39 RDM 17 202319 17.5N 109.3E PCN 9 DMCD37 RDM 18 202319 14.2N 109.6E PCN 9 T2.5/3.0 /w0.5/24MRC DMCD37 RDM 19 210108 17.6N 107.0E PCN 9 T2.5/3.0 /w0.5/24MRC DMCD37 RDM 21 210221 17.7N 107.0E PCN 9 T2.5/3.0 /w0.5/24MRC DMCD37 RDM 22 210321 17.7N 107.0E PCN 9 T4.5N 108.2E PCN 9 DMCD34 RDM 22 210321 17.7N 107.0E PCN 9 DMCD34 RDM 23 21139 14.1N 108.1E PCN 9 DMCD37 RDM 24 21021 17.9N 107.4E PCN 9 DMCD37 RDM 25 21421 17.9N 107.4E PCN 9 DMCD37 RDM 26 212258 17.3N 107.3E PCN 9 DMCD37 RDM 27 212258 17.3N 107.3E PCN 9 PCN 3 DMCD37 RDM 28 200302 17.3N 107.2E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 28 200302 17.3N 107.2E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 29 200302 17.5N 107.2E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 29 200302 17.5N 107.2E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 29 200302 17.5N 107.2E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 29 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 29 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDM 20 200302 17.5N 107.4E PCN 9 T1.5/2.5 /w1.0/24MRC DMCD37 RDMCD37 RDMCD37 RDMCD37 RDMCD37 RDMCD									KGUĆ
12 200304   14.04   104.6E   PCN 3   104.0E   PCN 3   12.0139   14.24   104.0E   PCN 3   104.0E   PCN 4   104.0E   PCN 5   104.0E   PCN 5   104.0E   PCN 5   104.0E   PCN 6   PCN 7   PCN 8   PCN 7   PCN 8   PCN 9   PCN					73-0/3-0	/02.0/21MR			RPMK
2 20300   10.64   109.8E   PCN 3   Description   RPM     3 21219   18.74   109.2E   PCN 4   Description   RPM     4 201219   18.74   109.2E   PCN 4   Description   RPM     5 201439   18.64   106.6E   PCN 4   Description   RPM     6 201439   18.64   106.6E   PCN 5   Description   RPM     7 202319   17.54   108.3E   PCN 5   PCN 5   PCN 5   PCN 5     8 202319   18.64   106.6E   PCN 5   PCN 5   PCN 5     9 210108   17.64   107.0E   PCN 5   PCN 5     10 210216   18.74   107.0E   PCN 5   PCN 5     20 21021   17.74   107.9E   PCN 3   T0.04.0-/01.0/264RC   Description   RPM     21 210321   17.74   107.4E   PCN 5   Description   RPM     22 210221   18.14   108.1E   PCN 5   Description   RPM     23 21139   18.14   108.1E   PCN 5   Description   RPM     24 21121   17.94   107.4E   PCN 5   PCN 3   Description   RPM     25 211421   17.94   107.4E   PCN 5   PCN 3   Description   RPM     26 212258   17.34   107.3E   PCN 5   PCN 5   Description   RPM     28 200302   17.34   107.2E   PCN 5   T1.57/2.5   M1.0/24HRC   Description   RPM     29 201302   17.34   107.2E   PCN 5   T1.57/2.5   M1.0/24HRC   Description   RPM     30 21139   16.64   106.6E   PCN 5   Description   RPM     31 21139   16.64   106.6E   PCN 5   Description   RPM     32 21139   16.44   106.6E   PCN 5   Description   RPM     33 221139   16.44   106.6E   PCN 5   Description   RPM     34 22100   16.44   106.6E   PCN 5   Description   RPM     35 22100   16.44   106.6E   PCN 5   Description   RPM     36 22100   16.44   106.6E   PCN 5   Description   RPM     37 22100   16.44   106.6E   PCN 5   Description   RPM     38 22100   16.44   106.6E   PCN 5   Description   RPM     39 22100   16.44   106.6E   PCN 5   Description   RPM     30 22100   16.44   106.6E   PCN 5   Description   RPM     30 22100   16.44   106.6E   PCN 5   Description   RP									ROOM
13 201219 1 13.71 100.2E PCN 4  20 1219 1 14.91 101.0E PCN 4  15 201499 1 14.641 100.4E PCN 4  16 201490 1 14.641 100.4E PCN 3  17 202319 17.541 100.4E PCN 5  18 202319 17.541 100.4E PCN 5  20 210126 1 14.241 100.6E PCN 5  20 210126 1 14.241 100.2E PCN 5  21 210121 17.77 107.9E PCN 5  22 210121 17.79 107.4E PCN 5  23 211139 1 14.141 100.1E PCN 5  23 211139 1 14.141 100.1E PCN 5  24 211421 17.941 107.4E PCN 3  25 21421 17.79 107.5E PCN 3  26 212259 17.79 107.9E PCN 3  27 212259 17.79 107.9E PCN 5  28 2201302 17.59 107.4F PCN 3  29 2201302 17.59 107.4F PCN 3  20 21139 1 14.141 107.2E PCN 5  21 21139 1 14.141 107.2E PCN 5  22 21139 1 14.141 107.2E PCN 5  23 21139 1 14.141 107.2E PCN 5  24 210121 17.94 107.5E PCN 5  25 212259 17.79 107.2E PCN 5  26 212259 17.79 107.2E PCN 5  27 212259 17.59 107.4F PCN 3  28 2201302 17.59 107.4F PCN 3  29 201302 17.59 107.4F PCN 3  20 201303 17.59 107.4F PCN 5  20				PCN 3					RPHK
14 201219 14.34 104.6E PCN 4									RPMK
10	14		19.34 189.6E	PCN 4			DMSP37		KGWC
17 202319 17.5% 100.3E PCN 5 18 202319 19.2% 100.6E PCN 5 72.5/7.0 /w0.5/24MRC 19 210108 17.6% 107.0E PCN 5 DMC077 RPM 19 210108 17.6% 107.0E PCN 5 DMC077 RPM 20 210126 14.2% 100.2E PCN 5 DMC074 RPM 21 210321 17.7% 107.0E PCN 3 22 210321 11.1% 100.1E PCN 5 23 211039 14.1% 100.1E PCN 5 24 211031 17.9% 107.4E PCN 3 DMC077 RPM 25 211031 17.9% 107.4E PCN 3 DMC079 26 211031 17.9% 107.4E PCN 3 DMC079 27 21228 17.3% 107.3E PCN 5 27 21228 17.3% 107.3E PCN 5 27 21228 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 28 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 28 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 28 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 29 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 20 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 20 220302 17.3% 107.2E PCN 3 T**0/4.0~/50.0/24MRC DMC077 RPM 21 221339 14.4% 104.6E PCN 5 DMC077 RPM 22 22102 14.4% 104.6E PCN 5 DMC077 RPM 23 22102 14.4% 104.6E PCN 5 DMC077 RPM 24 220302 17.3% 107.2E PCN 5 DMC077 RPM 25 200.2 10.4% 104.6E PCN 5 DMC077 RPM 26 200.2 10.4% 104.6E PCN 5 DMC077 RPM 27 200.2 10.4% 104.6E PCN 5 DMC077 RPM 28 200.2 10.4% 104.6E PCN 5 DMC077 RPM 29 200.2 10.4% 104.6E PCN 5 DMC077 RPM 20 200.2 10.4% 104.6E PCN 5 DMC077 RPM 20 200.2 10.4% 104.6E PCN 5 DMC077 RPM 20 200.2 10.4% 104.6E PCN 5 DMC077 RPM	15	201439	14.44 10A.7E	PCN 4			DREDIN		RPHK
17 20/2319 17.5% 100.3E PCN 5 18 20/2319 10.2% 100.6E PCN 5 18 20/2319 10.2% 100.6E PCN 5 21 210108 17.6% 107.0E PCN 5 22 210108 17.6% 107.0E PCN 5 23 211021 17.7% 107.0E PCN 5 24 210/221 17.7% 107.0E PCN 5 25 2110/21 17.9% 107.6E PCN 5 26 2110/21 17.9% 107.6E PCN 5 27 21/221 17.9% 107.6E PCN 3 28 2110/21 17.9% 107.6E PCN 3 29 210/21 17.9% 107.6E PCN 3 20 210/21 17.9% 107.6E PCN 5 21 21/228 17.5% 107.9E PCN 5 22 21/238 17.5% 107.9E PCN 5 23 2110/21 17.9% 107.2E PCN 5 24 22/20/21 17.5% 107.6E PCN 5 25 2110/21 17.9% 107.2E PCN 5 26 21/258 17.5% 107.6E PCN 5 27 21/258 17.5% 107.6E PCN 5 28 20/302 17.5% 107.6E PCN 5 29 20/302 17.5% 107.6E PCN 5 20 20	16	201440	19.6M 108.4E	PCN 3			DHED39		RODN
19 210108 17.5u 107.0E PCN 5 20 210126 14.2u 107.0E PCN 5 21 210321 17.7u 107.0E PCN 3 22 210321 17.7u 107.0E PCN 3 23 21139 14.1u 104.1E PCN 5 23 21139 14.1u 104.1E PCN 6 24 211421 17.9u 107.4E PCN 3 25 211421 17.9u 107.4E PCN 3 26 212258 17.3u 107.3E PCN 5 27 21228 17.3u 107.3E PCN 5 27 21228 17.3u 107.3E PCN 5 27 21228 17.3u 107.3E PCN 5 28 200302 17.3u 107.2E PCN 3 29 200302 17.3u 107.2E PCN 3 29 21139 14.9u 104.6E PCN 5 30 21139 14.9u 104.6E PCN 5 31 221139 14.9u 104.6E PCN 5 31 221139 14.9u 104.6E PCN 5 31 221139 14.9u 104.6E PCN 5 32 221002 16.9u 104.6E PCN 5 33 221002 16.9u 104.6E PCN 5 34 221002 16.9u 104.6E PCN 5 35 2002 17.9u 107.2E PCN 3 36 2007 17.9u 107.2E PCN 3 37 2007 17.9u 107.2E PCN 3 38 2007 17.9u 107.2E PCN 3 39 2007 17.9u 107.2E PCN 3 30 2007 17.	17		17.54 10A.3E	PCN 5			Dugp 17		RODN
20 210126 1 1-2x 100.2E Prn 5 21 210321 17.7x 107.0E Prn 3 74.0/4.0-/N1.0/24HRC Decord ROD 22 210321 17.7x 107.0E Prn 3 74.0/4.0-/N1.0/24HRC Decord ROD 23 211021 11.3x 107.0E Prn 3 Decord ROD 24 210321 17.3x 107.0E Prn 3 Decord ROD 25 211021 17.3x 107.0E Prn 3 Decord ROD 26 212258 17.3x 107.3E Prn 5 27 21221 17.3x 107.3E Prn 5 28 20002 17.5x 107.4E Prn 3 T**0/4.0-/S0.0/24HRC Decord ROD 27 20002 17.5x 107.4F Prn 3 Decord ROD 29 20002 17.5x 107.4F Prn 3 Decord ROD 30 20133 16.4x 107.6E Prn 5 31 201133 16.4x 107.6E Prn 5 32 20102 16.4x 107.6E Prn 5 34 20103 16.4x 107.6E Prn 5 35 20103 16.4x 107.6E Prn 5 36 20103 16.4x 107.6E Prn 5 37 20103 16.4x 107.6E Prn 5 38 20103 1	16	202319	19.2N 108.6E	PON 5	12.5/1.0	/WU.5/24HR4	DMC037		RPMK
21 210321 17.7 107.0 PC 97 3 74.0/4.0-/01.0/24HR4 Duscriu 22 210321 14.1 104.1 PC 9C 5 Duscriu 23 211159 14.1 104.1 PC 9C 4 Duscriu 24 21121 17.9 107.4 PC 9C 3 Duscriu 25 21121 17.9 107.4 PC 9C 3 Duscriu 26 212258 17.3 107.3 PC 9C 5 27 212258 17.3 107.3 PC 9C 5 27 212258 17.3 107.2 PC 9C 9 71.5/2.5 /w1.0/24HR4 28 200302 17.3 107.2 PC 9C 9 71.5/2.5 /w1.0/24HR4 28 200302 17.3 107.2 PC 9C 9 71.5/2.5 /w1.0/24HR4 29 200302 17.3 107.2 PC 9C 9 71.5/2.5 /w1.0/24HR4 30 201339 14.4 104.6 PC 9C 9 74.0/4.0-/50.0/24HR4 31 201339 14.4 104.6 PC 9C 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19	210108	17.64 107.0E	PC4 5	-		DMCDSY		RPMK
22 210321 14-14 104-1E PCN 5  23 211039 14-14 104-1E PCN 4  24 211039 14-14 104-1E PCN 4  25 211039 14-14 104-1E PCN 4  26 211031 17-04 107-0E PCN 3  27 211031 17-04 107-0E PCN 3  28 22032 17-34 107-0E PCN 5  28 220302 17-34 107-0E PCN 5  29 220302 17-35 106-0E PCN 3  30 221139 16-04 106-0E PCN 3  31 221139 16-04 106-0E PCN 5  31 221139 16-04 106-0E PCN 6  32 221002 16-04 106-0E PCN 6  32 221002 16-04 106-0E PCN 6  33 221002 16-04 106-0E PCN 6  34 221002 16-04 106-0E PCN 6  35 221002 16-04 106-0E PCN 6  36 PCN 7  37 PCN 7  38 PCN 7  88 PCN	20	210126	14.24 10A.2E	PCN 5			DMCH34		RPMK
23 211159 14,14 104,1E PCN 4 24 211421 17,34 107,4E PCN 3 25 211421 17,34 107,5E PCN 3 26 212258 17,34 107,3E PCN 5 27 212258 17,34 107,3E PCN 5 27 212258 17,34 107,2E PCN 5 27 212258 17,34 107,2E PCN 5 27 212308 17,34 107,2E PCN 5 28 204302 17,34 107,2E PCN 5 29 204302 17,34 107,2E PCN 3 30 221139 14,44 104,6E PCN 3 30 221139 14,44 104,6E PCN 3 31 221139 14,44 104,6E PCN 5 32 22100 14,44 104,6E PCN 6 33 20400 14,44 104,6E PCN 7 34 20400 14,44 104,6E PCN 7 35 20400 14,44 104,6E PCN 7 36 20400 14,44 104,6E PCN 7 37 8888	21	210321	17.74 107.9E	PCN 3	T4.0/4.0	-/91.0/24HR4	PERPHG :		RODN
26 211621 17.34 107.6E PCN 3 25 211621 17.34 107.6E PCN 3 26 212258 17.34 107.3E PCN 5 27 212258 17.34 107.3E PCN 5 28 220302 17.34 107.4E PCN 5 71.5/2.5 /w1.0/24HKC DWCP7 RPM 28 220302 17.34 107.4E PCN 3 74.0/4.0-/50.0/24HRC DWCP7 29 20302 17.35 106.4E PCN 3 30 23139 16.44 106.6E PCN 5 31 23139 16.44 106.6E PCN 5 32 23102 16.44 106.6E PCN 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22	210321	14.14 104.1E	PCN 5			DMCD39		RPHK
25 211421 17.34 107.0E Pri 3 Ougura RPM 26 212258 17.34 107.3E Pri 5 Pri 5 Ougura Pri 7 RPM 27 212258 17.34 107.2E Pri 3 To-0/4.0-/50-0/24HR Dequa ROD 28 220302 17.34 107.2E Pri 3 To-0/4.0-/50-0/24HR Dequa ROD 29 220302 17.34 107.2E Pri 3 To-0/4.0-/50-0/24HR Dequa ROD 30 221139 14.64 104.6E Pri 3 Ougura RPM 30 221139 14.64 104.6E Pri 5 Ougura RPM 31 221139 14.64 104.6E Pri 5 Ougura RPM 32 221402 14.64 104.5E Pri 5 Ougura RPM 33 221402 14.64 104.5E Pri 5 Ougura RPM	53	211159	14.14 104.1E	PCN 4			DMSP37		RPMK
26 212259 17.3w 107.3E PCN 5 27 212258 17.3w 107.3E PCN 5 27 212258 17.3w 107.2E PCN 3 T1.5/2.5 /w1.0/24HKC DwGw77 RPM 28 220302 17.3w 107.2E PCN 3 T**0/4.0~/50.0/24HKC DwGw77 ROD 29 220302 17.3w 107.2E PCN 3 DwGw74 RDM 30 231139 14.4w 104.6E PCN 5 31 231139 14.4w 104.6E PCN 5 32 23102 14.4w 104.6E PCN 5 0wGw77 RPM 31 231139 14.4w 104.6E PCN 5 0wGw77 RPM ARM	24	124115	17.94 107.4E	PCN 3			Drech sa		RODN
27 212258 17.44 107.46 PCN > 11.5/2.5 /M1.0/24HRC DMGP7 28 220302 17.34 107.26 PCN 3 T4.0/4.0-/50.0/24HRC DMGP34 RDD 29 220302 17.55 104.46 PCN 3 DMGP34 RPM 30 221139 14.64 104.66 PCN 3 DMGP37 RDD 31 221139 14.64 104.66 PCN 0 DMGP37 RPM 32 221402 14.64 104.56 PCN 0 DMGP37 RPM 32 221402 14.64 104.56 PCN 0 DMGP37 RPM RDD	25	124115	17.94 107.9E	PCN 3			Dech sa		RPHK
28 22/302 17.3% 107.2E PCN 3 74.0/4.0-/50.0/24HRC 0			17.34 197.3E	PCN 5			DMSP 37		RODN
29 220302 17,5% 104,45 PCN 3 DMSPRU 30 221139 14,64 164,65 PCN 3 DMSPRT RDD 31 221139 14,64 164,65 PCN 6 DMSPRT RPM 32 221402 14,64 164,55 PCN 6 DMSPRT RDD 32 221402 14,64 164,55 PCN 6 DMSPRT RDD	21	212258	17.64 107.9E	PC4 >	11.5/2.5	/W1.0/24HR	Duguar		RPHK
30 221139 14.64 174.66 PCN 3 04477 ROD 31 221139 14.44 174.66 PCN 0 04477 RPM 32 221402 14.64 174.56 PCN 5 04479 ROD					T4.0/4.0	-/50.0/24HR			RODH
31 221137 16.4W 104.6E PCN 0 DMSP37 RPM 32 221602 16.6W 106.5E PCN 5 DMSP39 ROD									RPMK
32 271602 IA.6N INA.5E PON 5 DASPING ROD									RODM
			16.9N 104.6E						RPMK
33 221402 14.64 195.1E PCN 5 DMSP4W RPM			16.44 106.5E	PCN 5			Dadhsa		RODY
	33	521405	14.4H 195.1E	PCN 5			Daznja		RPHK

### SYMMOTTE FIXES

FIA	TIME	FTY	INTENSTIV	NEAREST	
NU.	(7)	205111NH	ESTIMATE	DATA (NM)	COMMENTS
1	171200	15.0v 113.0E	15	150	
حَ	190000	17.50 111.5E	is	90	
3	101200	19.0% 111.5E	is	60	
	100000	14.00 111.2E	20	120	
Ġ	191500	14.3v 110.7E	25	120	
6	200000	14.54 149.5E	ē۶	50	
- 1	501500	14.14 109.58	10	50	
8	210000	17.24 10K.9E	راخ	70	
+	6021.5	17.04 100.0E	5	20	
10	224000	17.0M 107.0E	5	70	
11	220500	16.5V 10R. OF	25	150	
12	221500	17.00 107.0E	5	120	
13	210000	14.3v 104.05	16	120	
1.	240000	15.0H 104.0E	17	150	
15	250000	15.74 142.5E	10	60	

### TYPHOON OWEN

### SATELL LIFE FIXES

FIA	TIME	ETX					
NO.	171	POS1110M	ACCAA	DAJSEK CONE	SATFILITE	CJMHFNTS	SITE
• 1	210140	12.74 130.96	204 b	T1.0/1.0	044634	INII Jas	PG1#
• 3	212117	11.94 130.4E	PCN 5		DH2511		PGI
	214326	11.34 136.0E	PCN 5	72.0/2.0 /01.0/23HRS			PGT# PGT#
٠ 5	220120	11.04 134.7E	PCN 5	1-117660 77710775 31111	CERPAN		P194
* b	220357	11.54 137.2E	PCN 5		DMCH 17		PGTW
• 7	521550 52150#	11.54 134.4E	PCN 5		DMZB34		PGT#
. ,	221550	35.4E1 VF.11	PCN 5		DMCD34		PGT# RODN
• 10	222057	17.04 135.9E	Prv 5		DWSP37		PGTu
• 11	272308 270102	12.0M 136.7E	PCN 5		DMCDAY		PGT#
13	210105	11.90 135.4E 12.40 136.5E	PCN 5	TU.0/0.0 TZ.0/2.U /SD.0/ZAHRS	Dachia	INII 738	RPMK
14	270937	17.64 135.6E	PCV 6	12.077.0 730.072300-	0mgp37		#124 #124
1 >	102112	14.74 134.2E	PCV 5		DWeb 14		PGTW
16	535036	14.50 135.5E	Pry 5	-3	DMSP37		PGI⊯
16	240031 240032	15054 134-7E 16074 145-4E	Pry 5	12.0/2.0 /02.0/23HRs	DMCDSY		RPMK
17	240042	14. 24 135.0E	Prv 3	T3.0/7.0 /01.1/24HRS			PGT# PGT#
20	240043	16.94 134.7F	Pry 3	0.F\0.ET	DWebsa	INI Jas	RODN
55	240917 240917	14.24 137.7E	PCN 5		759240		PGTW
53	241313	19.40 133.56	Pru 3		AFGSMU		ROON RPMK
24	241314	19.34 132.7E	Pry 5		DMEDAN		PGI
<>	241324	11.24 132.7E	Prv 5		DWCD3A		PGTW
26 27	242157	14.1% 137.1E 20.94 131.2E	Pry 5	T4.074.0 /02.0/22HRS	Ducp 19 Ducp 17		RODN
ŽÜ	242158	24.74 130.9E	Prv 3	1441174.0 7115.0722HR	045277		RPMK Pgid
24	242158	20.44 130.4E	Pry 3		Ducu 47		RODY
31 30	250014	31.00 130.HE	Pc v 3	14.5/4.5 /D1.5/24HRS	Dechar		PGTW
35	250205 250205	21.3 : 130.6E 21.2:: 130.5E	PCN 3	14.5/4.5 /01.5/25HRS	Dachsa		PGTW
5 5	251038	21.94 129.7E	PCN L	17877865 7111657671105	045037		RODN Polw
	521039	21.30 120.7E	Prv 1		DUCUTI		RODA
35 36	251255 251304	22.04 129.4E 24.44 129.4E	PCV 2		DHEH34		PGT#
36	251305	53.00 150.1E	PCH I		DMCD34		APMK Rodn
38	252137	33.10 120.2E	Prv 1		OMSP37		PGTW
34	252137	22.94 124.2E	PCV 1	15.5/5.5 /01.5/24HRS	D446431		RPMK
40	240145 240146	21.36 129.9E	PCN I	** * * * * * * * * * * * * * * * * * *	DMCD3A		RPMK
42	240145	27. TN 120.0E	Prv	16.0/6.0 /01.5/24HRS		•	RODN Pgtw
43	241018	21. At 120.2E	Pru 1	, , , , , , , , , , , , , , , , , , , ,	D44077		PGTW
44	241018	23.44 129.2E	Pry 1		TEUPHU		RODN
46	24123H 24123H	24.00 129.3E 23.70 129.3E	PON 1		DMChair		PGT# RODN
4/	241246	21.9N 170.1E	PCN I		DHEDIA		RPMK
48	541546	23.34 120.3E	Prw 3		Dach sa	EYE NOT USHE	PGT#
4 ¥	24124b 242117	24.0% 120.2E	Prw 3 Prw 1		Decasion		RKS1 PGT#
51	246117	24. 14 129.5E	PCN I		D46643		400M
52	242339	24.74 129.55	PCN L	T5.0/4.0 /W1.0/22HRS	DAZASK		PGTW
53 54	242338 270127	24.44 120.4E	PCM I	15.0/6.0 /W1.0/22HRC	Dachay		ROOM
55	270127	24.84 129.5E 25.05 129.5E	PCN	16.074.0 /NO.5/24HR4	Deceda		RPMK PGTW
56	270127	24.74 129.3E	PCN 1		Duspay		RODN
57 58	270758	29.79 129.65	PCN I		SEASON		RODN
57	271720	24.10 120.4E	PCN I		Dach 11		PGT∉
60	271326	24.00 120.95	Prv I		DMZOSA		PGTW RPMK
61	211727	24.14 129.6E	PCN 1		Diensa		PGTW
62 63	711221	25.44 124.55	Pry I		Dachsa		RODN
64	212051	24.50 120.45 24.50 130.85	Pry 1		045437 1245937		PGT# RODN
65	176326	27.00   20.HF	Pru	14.0/5.0 /w1.1/24HRE	DACHAR		7007 #184
66	240109	27.24 127.HE	PC4 1		Onensa		PGTW
6/	240104	21.10 129.5E 21.10 129.7E	PCW I	14.1/5.0 /40.5/26HPC	Dech 10		ROUM
67	291114	27.50 129.HE	Prv		Dech 11		PGT# RODY
7 U	241.202	27.5% 120.8E	PC4 1		DACRAR		Patw
71	501501	27.50 1/2.0F	PCN 1		Duen sa		Av20
73	/41201 242031	27.46 120.7E	PON I		Onch 1,3		PGT# PoT#
1.	294025	30.7x 131.8E	Pry 3	14.074.5 /40.5/22HRs	Dadode		4KS0
/ =	2000+3	21.0. 120.4E	Prv 1	74.3/4.5 /50.0/24HRC	ひゃめち オイ		ROUN
76 11	201058 201058	24,20 120,75	Pry I	19.5/4.5	Dadasa	INII JOS	RKSO
75	201325	24.24 140.28 24.24 140.45	Pry I		Omen sy Omen sy		RPMK PGT#
1+	291325	27. 10 110.05	Pay 1		DRENSE		PG I W
90	231 130	20.20 1 10.5E	Prv 1		D+<0.14		RKSO
81	242159 242154	19.44   11.4F 30.36   11.3F	Pry 4	14.0/4.0	OMENTS	1411 792	PGTw
63	300211	11. no. 1 17.0F	Pry 1	19.5/4.5	13445 14	1411 345	ROUN
H 4	100511	11.4. 137.25	Pry 3		Dachia	·	PGT
85 86	101124	34.94 114.95	Pry 6		Dach sa		PGTW
H /	101311	14.50 114.25 14.50 115.85	Pry 5		() m < D 3 d		RPMK RODV
			• -		•		400₹

### 413CHAFT FIXES

FIA NO.	114E (2)	205111 m	FLT	700w4 461	ngs MSL₽				1171						EYÉ SHAPL			HIEY- NOITA				) (C)  P/55T		15 <b>N</b>
i	220112	12.50 110.56	15n0F1		999		250	45	150		100			10								2 >9		ı
5	و فرون د م	12.34 1 17.4F	1500F1		1002	15	>90	30	060		320			10					• 50	• 56	+ 2	:5 27	,	5
• 3	521904	11.24 1 17.2E	7044H	2077					040		310			5										3
•	5>5513	12.24 117.0E	1500F		1005		060	30	170		000			10					. 29	•25				3
•	210530	17.34 134.7E	1500F		399		150	?5	160		140			15						+52				•
•	5 30 40 1	11.10 134.4E	700:48	1041	1005	15	0		240		510			37						• •				•
	531353	14.44 135.ME	7104H	3015		_			190			150		10						-11				,
8	535519	15.20 135.0F	71848	2747	<b>39</b> 0		190	ă	170		110			,	CIRCILLAR	50			•14					?
	240509	17.44 134.2E	7nomH	1022			100	45	144		080		!		Cloc Lan					•13				•
10	2.0358	TH. THE I ME . PE	70048	1001		+2	190	30	140		050		4		CIRCULAR	4			*11	+15				•
11	541410	20.5M 131.ME	700MH	2621	•			_	180		100		5	1						• 3 5				'
15	242155	20.5N 131.2E	70048	2833	967		140	5	1 10		0.0			2					. ! #	.14	•	•		- :
13	240733	21.50 120.HE	7004M	2/01			360	8	120		080		5	5										•
1.4	240904	21.54 120.HE	700MH	2655	949		110	- 5	424				5	•	CIRCULAN	15				+15				
15	252131	22.9N 120.4E	700MH	2375	914		150	3		110		A	?	!	CIRCULAR	10			.13	• 20	٠.	,		7
10	241033	23.24 120.05	700mm	2003		100		3	310		520		2	1										•
17	500555	23.2N 120.0E	70046	2414	455		130	3	0.20		330		,	ı	CIRCILLAR	R				-18				•
1 4	240330	21.50 120.2E	7 n g mH	>34>	919		250	15	100		520		5		CIRCULAR	15				+17				10
13	242140	74.5v 1r0.4E	7.1046	2294	942		170	18	300		570			10	CONCENTRIC			180		.16		, 6		11
50	270240	24.94 120.66	710#H	2632			270	72	450		5/0			10	CIRCILLAR	15				+17				11
51	277548	25.54 120.7E	700 MB	2597			190	35	240		140			1	CIRCULAR	So			+14					12
55	240112	27.14 149.6E	7 n g m B	2648	953		>30	30	310		570		4		ELLIPTICAL			030		•15				13
53	290315	27.04 120.7E	7 1 0 ₩H	2047			090	150	360		270		5	•	ELLIPTICAL	35	15	550	- 1 -	+16				13
24	240414	24.94 129.4E	700MH	2594			040	50	130		0+0		5				_			+16				13
€2	294835	27.44 120.HE	7ngmb	2701	954		n 9 0	30	1 140		040		5		ELLIPTICAL		15	150		-17		, 3		14
56	CA2147	27.74 129.ME	70040	2682	952		040	90	120		020		2	1	CIRCILLAR	2			+15	-17				15
21	230048	31.04 120.1E	7n0#8	2081			250		DAF		200								_					13
28	500518	24. NN 1 29.7E	70048	2685			250		140		070				CIRCILLAR	15			•1•	+15				15
53	240645	24.94 129.HE	7n0×8	268A			n96		140		110				CIRCULAR					-17				16
30	200448	24.44 130.3E	710MH	7884	952		>70		340		270				ELLIPTICAL		10	310	•1•	+18				16
37	202145	30.60 171.LE	700MH	2702	956		040		150		0+0				CIRCULAR	9				.15				17
35	300006	30.44 131.4E	7 n g m tr	2707			160	15	5.40		160				CIRCULAR					+15				17
33	300500	31.74 131.HE	71048	2702	754		250	>0	160	78					CIRCULAR	10				-15				17
34	158008	32.94 133.4E	7ngmH	2094	957	90	310	5	270	60	360	12	•	5					. 16	.17	٠	ь		1.

### PASAN FITES

FIX	TIME	FIX			EYE	EYF	RAITING	COUE				HADAR	SITE
NO.	(7)	POSTTION	RADAR	<b>PCUBA</b>	SHAPE	Dlam	ASWAH				COMMENTS	POSTTTOW	MMO 40.
1	254100	22.9N 129.3E	LAND				35//6	43316				26.2N 127.8E	47937
Ž	252200	23.1N 129.3E	LAVD				34//2					26.2W 127.8E	47997
3	252300	23.2N 120.2E	LAND				34//2					26,2N 127.8E	47937
4	252300	21.34 129.2E	LAND	POOR								26.3M 126.6E	47929
č	240000	27.24 120.2E	LAVO	•			55//3	53308				26.2W 127.8E	47997
6	240100	23.14 129.1E	LAND				65//3	52005				26.2N 127.8E	47937
7	540100	30.051 MS.FS	LAND	G700		30						26.34 125.6E	47929
8	BOSUAS	23.3N 120.0E	LAVD				65//3	53416				26.2N 127.8E	47937
,	5.0500	23.3N 120.0E	LAND	PauH				• • • •	FYE	MOVA	3225	26. LN 127.7E	47937
10	240300	23.5N 129.0E	LAVO				65//2	501//				26.2m 127.8E	47937
i i	240300	21.14 129.0E	LAND	GOUD		30						26.3N 125.8E	47929
12	240400	24.54 128.0E	LAND	POUR		30			EVE	MOVE	3610	26.1M 127.7E	47937
1.3	240500	23.54 120.0E	LAND				35//1	70204				26.2W 127.8E	47937
14	240500	24.54 12R.1E	LAND	6100		30			EΥE	MOVE	3210	26.14 127.7E	47937
15	240500	23.4N 120.1E	LAVD	6200		30			-			26.1N 127.7E	47937
16	260500	23.4M 129.UE	LAHO				55//1	70202				26.2N 127.8E	47937
17	240700	21.7N 120.2E	LAND				35/41	40±01				76.2N 127.8E	47937
16	240700	23.74 129.1E	LAND	GOOU		30						26.1M 127.7E	47997
19	240900	23.4N 129.1E	LANC	GOUU		30						26. IN 127.7E	47937
20	00E0AS	33.4N 120.2E	LAHD	•			20411	70603				26.2N 127.8E	47997
21	260900	21.74 120.2E	LAND	GOUD		3.0			FYE	MOVE	0205	26.1M 127.7E	47937
2.2	261000	21.54 120.2E	AND	POR							0205	26. IN 127.7E	47937
23	261000	21.74 129.1E	LAND				20//1	53306	-			38.75 MS.65	47977
24	241100	71.94 120.3F	LAND				55/41	70504				76.2N 127.8E	47937
25	241100	23.74 120.2E	LAVO	PODR					EYE	STNP		26.1M 127.7E	47937
26	241500	23. 24 129.2E	LAND	POUN						STUR		26. IN 127.7E	47937
21	241500	23. JN 129.2E	LAND				25/11	73605	-	-		36.2N 127.8E	47937
28	241300	24.04 120.7E	LA-12	രാവ		20			FYE	MOVE	0205	26. IN 127.7E	47937
24	241300	24.04 129.2E	(Art)	****			55/11	70106	•			26,2N 127.8E	47997
30	241400	24.14 129.3E	LAug				55/11	73606				38.751 NS.85	47937
31	241400	24. 941 179. 3E	LAND	GADU		20	_		EYE	HOVE	0205	26. LW 127.7E	47937
32	241500	24.24 120.1E	Avo	GAUU		20			EVE	MOVE	3610	26.1N 127.7E	47937
زز	261500	24.24 120.7F	LAND				55/11	70105				26.2m 127.8E	47937
3.	241500	24. 34 129.2E	4410				55/11					38.781 45.85	47937
30	241700	24.34 1/9.3E	Ann				11/11					26.2W 127.8E	47937
36	241700	74.34 129.1E	A-10	ลาบบ		20			EYE	HOVE	3610	76.14 127.7E	47937
31	241900	24. 34 120. 3F	LAND	6130		20					3610	26.1M 127.7E	47937
38	241900	24.84 120.3F	AND				3//11	70204	- 1			36.2M 127.8E	47917
9.9	241300	24.54 170.4E					3//11					26.2N 127.8E	47997
			- '										•

• 0			129.38	LAND	GNUU	20			FY	F MOV	G 0510	** 1		
41		24.5	4 120.4E 4 129.4E	LAND	GNUD	20			Evi	HOV	010	26.1	4 127,7E ≈ 127,7E	47437 47937
4.3			129.5E					1 70205 1 70406				26.2	≈ 127.7E ≈ 127.8E	1997
44		24.51	129.5E	LAND	FALR	45	7///	, ,0400	FvI	F Mnw	R 0515	26.21 24.11	N 127.8E	47937
45			129.5E		FAIH	45			Evi	MOVE	6 US15	26.1	N 127.7E	47937
47			129.5E	LAND	FAIH	45	4//4	70204				26.2	≈ 127.8E	7937
48	270000	24.74	129.6E	LAND	ดายย	45			EVI	MOVE	9515	26.1	¥ 127.7E	47997
49 50		24.9	, 129.5E	LAND			6//4	73002	٠.,		. 0313	76.11 26.11	127.7E	47937 47937
51		25.0	129.5E	LAND			7////	/999/				28.40	127.56	47909
52	270100	24.94	129.6E	LAND			7////	73000				26.11	127.7E	47477
5 d 5 d		25.04	150.6E	LAND	GOOD	45			EVE	Move	050E #	(8.4)	× 127.5E × 127./£	7300
55		25.14	129.6E	LAND	GnOD		45///	53615				28.44	× 122.5€	47360
56	270200	25.11	179.5E	LAND	3.100	45	4//11	73602	EAE	Muni	3610	76.11	4 12/.TE	47937
57 58		25.24	129.6E	LAND	<b>6730</b>	45		,,,,,,,	FYF	Move	3610	76.19	₩ 127.7E	47937
59	270300 270300	25.24	120.5E	LAND			6//11	53602			. 3010	26.1	127.7E	47937 47937
60	270400		129.46	LAND				73509				78.44	4 127.5E	_79n9
61	270400	25.34	129.6E	LAND				53608				26.19	127.7E	67937
62 63	270400 270500		129.66	LAND	GADD	45			€ + €	MOVE	3610	70.4° 26.10	127.5E	477n9
64	270500		150.9E	LAND			6//41	7360+				26.1	127.7E	47937
65	270510	25.54	129.6E	LAND	G100		N3///	53003				28.4*	129.58	67909
66 67	270535 270600		154.65	LAND	6100							75.48 26.48	127.83 127.8E	47931
68	270500		129.6E	LAND			6///1	70205				26.1	127.7E	47937
69	270610		129.5E	LAND	6030		45///	50000				28.44	128.5E	4.7 ang
70	270630		129.5E	LAND	6000							26.44	121.8E	47971
71 72	270700 270700	25.5N	129.6E 129.7E	LAND	00	_	65///	50108				78.44	127.55	4791g
73	270700		124.7E	LAND	G100	45	56 (1)	70605	EVE	MUAU	3610	26.16	1 127.75	. 7327
74	270710	25.74	129.4E	LAND	GาOU		77/11	70003				26.15	127.75 127.8E 127.7E	47937
75 76	27090) 270900		129.7E	LAND	GNUD	50			EVE	MOVE	3610	26.14	127.75	47931
77	270900	25.4N	129.7E	LAND			5//11	70200				26.18	127.7E	47937
78	270910	25.74	129.3E	LAND	GOOD		n-///	53505				28.4N	129.5E	47909
79 80	270940 270900	25.7N	129.3E	LAND	GNUU							26.4N	127.85	47971 47971
81	270900		129.7E	LAND			6//41	70205				76.14	127.8E	7937
82	270900	25.74	129.HE	LAND	(in00	60	65///	50208	E-E	Maur	3615	28.44	127.58	47909
83 84	270910 270940	25.9N	129.4E	LAND	ციმს				210	H	3013	76.1M	127.75	47937 47931
85	271000	27.9N	129.4E	LAND	GJUU							26. 4N	127.8E	47931
86	271000		129.HE	LAND	Gaou	40	A5///	50000				28.48	127.8E	
87	271000	25.74	129.7E	LAND			6//41	73604	6 46	HITT	3610	26.IN	127.7E	47937 47937
88 69	271035 271100	25. QN	129.65	LAND	POR							26.4N	127.BE	47931
90	271100		129.86	LAND	6100	40	3//61	70502	£4F	MUAU	3010	26. IN	127.8E	47937
91	271100	25.34	170.HE	LAND				50602				26.1N	127.7E	47937
92	271200 271200		129.7E	CMAJ	6500	£.0			EYF	MOVE	3620	76. IN	127.7E	479n9 47937
94	271300	24.14	129.7E	LAND			6//11	70104 73507				26.1≥	127.7E	47977
95	271300	26.04	129.7E	LAND	5100	60	7//11	13301	FvF	MOVE	3615	26.1W	127.7E	47937
96	271400 271400	24.54	129.7E	CAAD	GYUU	60					3515	26.1m	127.7E	47937 47937
98	271400		120.05	LAND			5//11					26.1₩	127.7E	47937
99	271500	24.5N	129.7E	LAND			6///1	73505				28.4N	129.5E 127.7E	47909
100	271500 271600	24.3N	129.6E 129.7E	LAVO			65///	53608				28.4N	127.5E	47937 47909
105	271500	26.5N	179.6E	LAND			6///I 65///					76. IN	127.7E	47937
103	271500	26.50	129. TE	CHAJ	PODR		44///	22011	FVF	MOVE	3615	28.4N	127.5E	47709
105	271700 271700		129.7E	LAHO	00		45///	51104			3013	28.44	129.5E	479 R
106	271700	24.44	120.46	LAND LAND	PODA		6///1	<b>*</b> 0304	EYF	MUAG	0410	26.1N	127.7E	47937
107	271900	26.64	150.86	LAND	POOR		B///1	70204	FVF	MUAR	0510	26.1N	127.7E	47937
108	271900	24.40	120.78	LAND			K///3	70106	•		0310	26. IN	127.7E	47917
110	271900 271900	26.54	129.7E	CHAJ			65///	53603				78.4N	123.58	7909
111	271900	26.4N	129.66	LAND			65///					28. AM	127.5E	47909
112	271700	24.54	120.HE	LAHO	PADR		W. / / I	73300	EYF	STNR		76,1%	127.7E	47937 47929
113 114	272000 272000		129.7E 129.7E	LAVO	0000		6//11	73506				76.1N	123.BE	47937
115	272100	24.74	120.46	LAND	₽ <b>10</b> ₩					MOVG		21.4N	129.7E	47942
116	212100	24.94	120.MF	LAND	,		5//11	73605	FAF	MUAG	0310	27.4W	129.7E	47942
117 118	272200 272200			(AND	F. 10		45/11					78.4N	127.7E	47997 47909
119	272300		129.HE	LAND	FAIR GOUU	4.0 3.0				MAVE		27.AN	128.75	47742
150	272300	27.0N	120.86	LAND	3,-0	40	65///	53611	EAF	MUAU	3615	27,46	129.76	47942
122	240000 240000	27.04	170.45	LAND			45///					78.4N	129.5E	477n9 477n9
123	24000D 240035		129.HE 129.3E	LAND	ดาขบ ดาขบ	45			EvF	Move	3610	27.4N	128.7E	47942
124	SAULLO	27.3N	120.45	LAND	FAIH							26.4N	127.8E	47931
125 126	240135	27.44	179.05	LAHO	FAIR							76.4N 26.4N	127.8E	47931
0	Sw0500	77.14	120.65	LAVO			45///	53108				28.4*	127.5E	47909

1.11	3. 11. 3.1 .												_	
121	500510	27.65	1.0.05	LAND	FAIH	_							127.BE	47971
158	540510		150.1E	LAND	ดางบ	45		Lvt	MITUR	3510		26.LN	127.7E	47937
129	240300		124.6E	CAND			45/// 53	1303				78.44		47909
130	200300		150.HE	CAND	ცესს	4.0		E∀ŧ	MOVE	3610		27.4₩	123.7E	47942
131	240310	27.54	120.46	( A vD	Phuk							26.44	127.8E	47971
135	260400	27.24	129.7E	LAND	ดายย	4 D		€×F	MOVE	3205		27.4N	129.78	47942
133	290400	27.20	129.7E	LAND			21A/1 70	P01				26.2N	127.8E	47977
134	240400		129.0F	LAND			65/// 50	203				28.4H	129.56	47909
135	240500		120.8E	LAND			20711 70					26. ZN	127.8E	47937
136	290500		120.HE	LAVO			45/// 50					28.4N		
137	290500		129.HE	LAND	ცემს	E ()	50		Move	34.05		70.44	127.35	47909
138	240600					50			MOVE			27.48	128.7E	47942
		27.00	129.AE	LAND	GOUD	-0			MILLAN	3002		27.4N	159.15	47942
137	547600		120.HE	LAND			5//11 70					26.24		47937
140	240700		150.05	LAND		_	45/// 50	003				28.4₩	129.5E	47984
141	240700	27.64	120.HE	LAND	5100	40			MOVE			27.4N	129.7E	47942
142	280900		129.9€	LAND	GNUU	40		EVE	MOVA	0305		27.4N	128.7E	47942
143	280900		150.45	LAND			45/// 53	<b>&gt;04</b>				28.4N	127.5E	47909
144	200935		120.7E	LAND	ცისე							26.48	127.8E	47931
145	29090p	27.5N	120.4E	LAND			55/// 50	103				28.4M	129.5E	47909
146	240300	27.54	129.4E	LAND	6100	20			SIND			27.44	128.7E	47942
147	290710	27.54	38.051	LAVO	FAIR							26.48	127.BE	47931
148	290935		129.8E	LAND	FAIR							26.4M	27. RF	47931
149	281000		150.95	LAND	G200	25		FVE	MOVE	0505		27.4M	128.75	47942
150	241000	27.5v	120.95	LAND	0 /00		55/// 53		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0303		28.4N	123 65	47909
151	2.1010		129.5€	LAND	POOR							26.4M	127.35	47931
152	201035	27.57	120.75		910D							26.48	127.05	4/911
153	241100		129.7E	LAND		25						26.4N	127.06	47931
			150.AE	LAND	6000	77		FAE	MOVG	3610		27.4N	153.75	47942
154	241110		120.7E	LAND	FAIR							26.4N	127.BE	47991
155	SHISOR		150.85	LAND			55/// 52					28.4W		47989
156	241510		120.9E	LAND	GADU	25			STNR			27.4N	128.7E	47942
157	241300		120.HE	(AND			55/// 52	003				28.4M	129.5E	47709
158	201330	27.54	129.9E	LAND	6า0ม	25		EYE	MOVE	3205		27.4N	128.78	47942
159	241400	27.54	129.9E	LAND	GOUD	70		EVE	MOVE	3605		27.4N	128.7E	47942
160	291400	27.44	129.HE	LAND			55/// 51					28.48	123.5F	47909
161	241535		129.4€	LAND	GOUD	30			HOVE	3605		27.44		47942
162	291500		129.9E	LAND	0 100	***	55/// 53			3002		28.4N	153415	
163	291615			LAND	c=00	90	17/// 33							47909
164	2A1700		129.9E		GnOD	10			STNR			27.4N	150.15	47962
			150.BE	LAND			55/// -53					28.44		47989
165	2R1700		120.9E	CAND	6n0D	30			STHR			27.4N	129.7E	47942
166	Se1800		150.HE	LAND	GNUD	30			MUAB	3610		27.4M	128.7E	47942
167	241900		150.85	LAND			55/// 53	604				28,4№	127.5E	47989
168	291915	27.94	129.HE	LAND	600D	30		EYF	STNR			27.4N	128.7E	47942
169	292000		129.BE	LAND			55/// 53	403				28.4N	129.5E	47989
170	2A2100		129.75	LAND			45/// 53					28.4M		47989
171	242110	27.RN	120 HE	LAND	6100	30			STND			27.44	128.7F	47942
172	245500		129.7E	LAND	0,140		55/// 53		•			28,49	123 55	47909
173	545500	27.44	129.8E		6900	30	17/// 53		STNR			27.44	127.36	
174	242300			LAND	Grion	*0	EE CO		3144			27,44	125,76	47942
			150.8E	CIAAJ			55/// 50					78.48	154.26	47989
175	500000	24.1N	129.RE	LAND	Gn00	30		EVE	MOVG	3610		27.4H 28.4H	128.7E	47942
176	290000		129.BE	LAND			55/// 53					28.48	129.5E	47969
177	290100		129.75	LAND	GnOD	70			MOVE	3210		27.4W	128-7E	47942
176	500500		129.7E	LAND			55//2 53					28.44	129.5E	47909
179	200200	28.1K	129.7E	LAND	GNUD	30		E۷E	MOVE	3605		27.4M	128.7E	47942
180	290300	24.24	129.7E	LAND			10382 50	205				28.4M		47909
181	290300		129.BE	LAND	6 <b>10</b> 0	70			MOVE	3605		27.4W		47942
162	290400		120.BE	CHAJ	6000	70		FVF	MOVE	3615		27.4N	128.75	47742
183	290400		129.BE	LAND	0.1		10412 50	105		3017		28.4N	22 55	47909
184	290500	28.44	129.7E	LAND			11512 53							
185	290500		129.8E	LAND	GOUU	30	11312 33		MOVE	2614		28,4%	127.35	47989
186						***				3010		27.4N	150-15	47942
	290520		150.BE	LAND	FAIR				STHR		TAKAHATA			
187	290500		129.RE	LAND			11722 50	208				28,4N	129.5E	47989
100	290510		129.9E	LAND	GnOD	20		EYE	STHR		TAKAHATA			
189	290700	29.5N	129.8E	CAND	G100	20		EYE	STNR		TAKAHATA			
190	290700	24.54	129.HE	LAND	GOUD	30		EVE	MOVE	3610		27.4M	128.7E	47942
191	290700	29.54	129.BE	LAND			5///1 5/	///				30.6M	31.06	47849
192	200700		120.HE	LAND			11712 53					28.4N	122.5F	47909
193	290900		120.4E	LAND			11312 50					28,4N	100 SE	
194	290900		130.0E	LAND	6100	30	30		MOVA	3616		27 44	. 27.JE	47909
195	290800	28.4	129.9E	LAND	Gn00	25					74-444-4	27,4M	. CD. FE	47942
196	290800				9:100	/7	E / / / 1	505 EVE	MUAd	A210	TAKAHATA	30 44		
197	200900		129.88	LAND			5///1 53					30,6M		47869
		28.7N		LAND			5///1 50					30.6M	131.0E	47849
198	290900		130.0E	LAND		_	11412 50	003			_	28,48	129,5E	47989
199	290300	24. TN		LAND	GnOD	>5		EYE	MOVE	0310	TAKAHATA			
200	201000	24.84		LAND			11412 50					28.48	1 29.5E	47909
201	241000		13n.lE	LAND	G10D	20		EVE	MOVE	0820	TARAHATA	-		
505	291000	24.9N	130.0E	LAND			5///1 50	508				30.68	131.05	47969
203	2-1100		130.1E	LAND			11572 50					28.48		47989
204	291100		131.TE	LAND	gn0u	20	_ 30		MOVE	0215	TAKAHATA			41707
205	201100	24. AN		LAND	6100	30			MOVA	2020	.=7=0=1=	27 42	38.75	47942
206	241100	24.44		LAND	J.,	***	E///1 en		A 4 14			27.4H		47942
207	501500	20.00	130.25		conn	30	5///1 50		Maria	A216		30.60		
		24.04	1 77 4 6 6	LAND	6000	30		EAE	MUAS	4512		27.4N	125.7E	47942
	201500	29.14		LAND			5///1 50					30.6	31.0E	47569
209	501500		130.16	LAND			11412 50					28.4N		47909
510	501300	29.14		LAND			5///1 50					30,6N	131.0E	47969
511	201300		130.2E	LAND			11412 50					28.48	29.5E	47909
515	291400	24.2N		LAND	<b>G</b> n0D	25	3-	EYE	HOVE	0520		27.4H	28.7E	47942
213	291400	29.24		LAND			11511 50					28.4H		47909
214	291400		130.3E	LAND	<b>G</b> 100	20			MUAU	0315	TARAHATA		DE.	4
215	291400	20.24		LAND		- •	204/1 50		.,			30 44		. 7844
216	291-00	20.34	130.3E	LAND	6200	20	· 1 30.		Maya	4315	74-444-	30,6M	11.0E	47849
					Undu	>0	21411		MOAK	A212	TAKAHATA			
217	291500	20.34	130.36	LAND			21411 50					28,4H	27.5E	47989
218	291500	29.6N		LAND			5///1 530	Bud				30.68	31.05	47969
519	201500	29.4N		LAND	6n0D	25			MUAU	3625		27.49	28.7E	47942
550	291600	20.54		LAND			5///1 50					30.60	31.0E	47869
551	501900	24.54		LAND			51441 50	107				28.4W 1	29,58	47989
555	291500	24.54	34.nf	LAND	GOUD	25		E×€	MOVE	3625		27.48		47942
553	291700	27.54		LAND	6n00	15		EYE	MOVE		ATAMAPAT			
224	201700	29.7N		(A-10			21411 502	211		-		28,4N	29.5E	47909
225	291700	20.74		LAND	Gา00	25			MOVR	0325		27,48		47942
556	201700	29.74		LAND			5///1 //							
221	201900	74.44	130.5F	LAND	GOUD	15		FUE	MOVA	0320	****	30,68	31.45	47869
				AND	5 100	' 7	21431 50	311	·	- 160	TARAMATA	28 44	20 55	. 3000
,,,,,,	20100-						~19 TL 50.	<b>311</b>				28.44	78.45	47909
558	501900	29.94	1 31. 4	10				• .				•	67,32	41707

224	201900	23.4. 130	30.5	L A - 10			217/1						30,6™	131.05	47964
230	291900	24.9N 13n	.7E	LAVD			21771	50511					30.6	131.0E	47449
155	501400	27.34 [10		LAND	ดาบบ	20	21661	50306	CUE	Move	0320	TAKAHATA	/8.4~	123.56	67+09
533	545000 541400	30.00 130 30.10 130		LAND LAND	3100	20					0420	TAKAHATA			
234	5 3 2 0 0 0	30.1M 130	.HE	(A-40)	3.00		44//1	50216	-					129.5E	47709
235	505000	30.24 130	.9E	LAND			21571	50314					30.6%	131.0E	47969
236	505100	34.3N 130		LA:ID			215/1	50108						131.05	47869 47909
237 23a	292100 292100	30.3N 131	.OE	LAND GMAJ	ดายม	20	65///	50211	CVF	MOVE	0420	TAKAHATA	/O. **	123.5E	474119
239	505500	30.3N 131	. 1 F	LAND	9.100	- "	65///	50506					28.48	127.5E	47909
240	505500	30.4N 131		LAND			21571	50614					30.6N	131.08	47969
241	292300	30.5N 131	.2E	LAND			65///	-0313					28.44	129.5E	47909
242	505300	30.4N 131	• <b>+</b> E	LAND		20	10401	50419		Maa	0520	STHOKOSIKI	30.6₩	131.08	47849
243	292300 300000	30.6N 131		LAND LAND	6100 6100	20			FVF	MOVE	0520	\$1404051KI			
245	300000	30.Av 131	-6E	LAND	(4 100		5///1	50414					30,6№	131.0E	47869
246	300100	31.04 131	.7E	LAND	Gaud	20			EYE	MOVE	0524	514047SIK1			
241	300500	31.34 131	.4E	LA 1D			20371	50316					30.6N	131.0E	47869
248 247	3nu200	31.4M 131	1 • ME	LAND	6100	20	65/12	5////	FVF	Hove	0530	STHOKOSIKI	33.44	130.3E	47906
250	300300	31.64 132		LAND	(1100	- "	6////	11111	_,,_	7.70.1	.,,,,		33.3№	134.2E	47899
251	300300	31.54 131	1.4E	LAND			65/12						33.4N	130.3E	47806
252	300300	31.34 132	>.2E	L AND									32.1₩	131.5E	47854
253	300300	31.59 132		LAND	ดาวบ	10	5///1		EAF	MOVE	0530	STMOKASIKI	30 64	131.0E	47949
254 255	3nu300 3nu400	31.5N 132 31.7N 132		LAND		30	5///1	20412	FUE	Move	0645	KJ5414010	30.0	131.00	41777
256	300400	31.9N 132	. 4E	LAND		•••	5///1	50419	£ • c	7	0043	433777010	30.6₩	131.0E	47969
257	300400	31.4N 132	> 5E	LAND	670U	20		-	E∀E	MOVE	0550	SEBURI			
258	300400	31.94 132		( A-ID			55/72							130.3E	47806
259	300400	31.7∿ 137		CAAJ			5////	50424					33,3№	134.2E	47999 47969
260 261	300500 300500	32.04 132 32.14 132		LAND	ดายบ	20	3////	50222	EVE	Nova	0540	SFOURI	30.00	131.02	41203
595	300500	32.04 13:		LAND	(4-100		10501	50524	2		0340		33, 3₩	134.2E	47999
263	300500	31.9v 13:		LAND		25			EYE	MOVE	0440	KJ541MDTO			
264	300500	32.24 13:	.RE	CA-10			44145	50430					33,4N	130.3E	47806
265	300520	12.2N 132		LAND	ดาขบ		10611	=0532					32.18	131.5E	47854
266 267	300600 300600	32.3M 13:	7.7E	LAND			5///}						30.6N	131.0E	47969
568	300500	32.2N 13:		LAND	GNJU		•	,,,,,					32,18	131.5E	47954
269	300500	32,24 13	7.0E	LAND			246/3	50322					34.3N	132.6E	47792
270	300500	35.34 13.	3.0E	LAND	GnOU	25					0540	SFBURI KJSHTMOTO			
271	3nu600 3nu700	32.24 13:	2.7E	LAND LAND	รายย	45 20					0155 0540	SrBuR1			
273	300700	32.4N 13	3.2F	LAND	3-100	· "	10511	50522			• • • • • • • • • • • • • • • • • • • •	0	33,3N	134.25	47599
274	300/00	32.5N 13		CPAL		40			€×F	Move	0150	KJSHIMOTU			
275	300700	72.5N 13		LAND			246/3	50419					34,3N	132.6E	47792 47792
276	002UnE 802AnF	32.94 [3		LAND LAND			246/3 2076[							132.6E	7999
278	300900	33.0N 13	7.7	(ANI)	ดายง	20		1054.4	EYE	MOVE	0540	SEBURI			•
279	300900	33.1N 130	4 . PE	(AvD		45					0345	KJ54TMOTO			
280	300400	31.19 13		LAND			20441	50522			05.0	660.407	73. 3₩	134.28	47999
282 185	304700 304700	33.1N 131 33.1N 134		LAND	Pjuk	20	65//2	50526	FAF	MUAR	0540	SFBURI	34 38	132.66	47792
587	301000	33.4N 136		AND			20541							134.2E	1999
284	301000	31.34 13	3.2E	LAND		65			EYF	Move	0540	KJ41MOTO			
285	301000	37,44 130	4.4E	LAHD			44115							132.6E	67792
286 785	3n1000 3n1100	73.2N 13		(AND		4.0	64///	50/16	r., E	ма	0645	KJSHIMOTO	35,3₩	139.7E	47539
288	301100	37.5N 134 37.8N 134	6 - MF	FWA		• 11	65//2	50421	646	MILL OF	0045	K35717010	34.3N	132.6E	£7792
587	301100	33.5N 134	3 . 6E	LAND			20541	50524					33. JN	134.2E	47999
240	3-1100	33.6N 134		CIVAJ			65///	50032						138.7E	47539
291	301100	31.4N 134	7E	LAND		45	105//	/////			44.35	4.547001	34.hN	135.7E	47773
292	301500	33.7V 130		LAND		47	65///	70/24	FAL	HUAC	0435	KASATORI	35. 44	139.7E	47639
294	301500	34.0N 134		LAND			30541	54024						134.2E	47999
295	301500	34.1V 139	5.0E	LAND			1244/	11111					34.68	135.7E	47773
296	301300	33.4N 139	5.0E	LAND			65///	70522						138.7E	47539
297 298	3n1300 3n1300	34.24 13	4.2E	LAND		30	30443		e ~ E	House	0345	KASATORI	76.24	127.86	47937
299	301300	34.2N 131		LAND LAND		•"	7277/	11111	C 41	H118 (4	0343	75 1-1081	14.6N	135.7E	47773
300	301400	34.3N 130		LAND			1186/						34.6N	135.78	47773
301	301400	14.4M 130	s.6E	CMAJ			35///						35.3№	139.7E	47539
302	301400	34, 54 134		AND		20	30444		EYF	MUAE	0445	KASATORI	34	126.75	. 77**
303	3n1500 3n1500	35.04 13/	4.2E	CEAJ OHAJ		4.5	20440	3////	6 v 6	Move	0445	KASATORI	54.04	135.7E	47773
305	301500	34.24 130	. 0E	AVO			15///	10330	2.0	-4.14			35, 3N	135.7E	47539
306	311600	35.04 17/	4.6E	LAND		75			Evf	MOVG	3635		37.4M	135.9€	47600
307	301500	35.64 13/	4.7E	LAHD			IAUAL	50532					34.6M	135.7E	47773
30 B	3n1700 3n1700	35.94 13: 35.54 13:	7 + EE	CHAJ		75	IAPAF	20232	FUE	Mouc	0455		19.6N	135.7E	47773 47500
310	301700	35.5N 13		LAND		, ,	35///	70432	5 41	A11844	0433		35.3N	139.75	47639
311	302300	30.14 141	1 • 3E	LAND	ดาขอ	20	•				0595	YAMADA		,	
315	010020	40.5N 15	, . ME	LAND	P1UH	9.0			EAL	MUAG	3110	YAMADA			

STHOOTIC FIRES

FIL	TIME	FTX	INTENSITY	NFAREST	
NO.	(2)	HC171205	FSTIMATE	DATA (NH)	COMMENT
	190000	15.04 149.0E	0 1	200	•
ż	141500	11.54 147.55	iŭ	500	
3	200000	13.04 144.0E	io	150	
	501500	12.00 147.0E	10	200	
5	210000	11.5N 100.5F	לו	200	
6	2,1200	11.9M   134.0E	15	150	
7	211500	17.74 1 19.ME	15	150	

### TROPICAL STORM PAMELA

### CATELLITE FIRES

FIA	1145	K 1.8														
40.	(2)	POSTTIUM	ACCAY	DAJ4VK	Con	Ē	SATFII	1 1 E		CJ	44FN	15			SITE	
1	235520	14.50 144.38	PCN 5	TU.0/0.	a		0=51	AF	I٨	[1 ]	15				PGTW	
2	242732	14. 24 147. YE	PCW 3	T2.0/2.	0 /11	2.1/24485	DMS	24	Łĸ	アレンミ	) 1 L	CC			PGT#	
د		13.00 [41.4F	Pry n				Orce								PGTW	
4	251314	14.00 142.JE	Pry 5				0-51	14							PGT d	
2	252137	20.54 130.2E	PCM 6				Duci								PGIW	
6		21.24 1 4K.4E	Pru s			0.5/27485				PUSE		.cc			PGTW	
,		21.20   136.HE		Tl.n/1.	0		DMSI		IN	11 )	15				RPMK	
5		23.24 £37.9F	Pry 1				Dr.21								PGT₩	
4	241246	24.31-117.6E	PCN 3				Dws	74							PGI#	
							1 30-4		IrES							
	11ME (2)	€ 7 X ≥0\$11100	FLT		DAS	MAX-SFC-								EYE SHAPE	FYE ORIEN-	EYF TEMP (C)
	***		. • •			4:E. mo.	- 10		• (			****		3.12.	014-1141	
• 1	250927	17.40 142.15	710MH	3151	004	60 100		160	54	100	35		1			.14 + 7
		74.5x 140.1E	1500F1		004	25 n50	30	110		050	30	4	5			15. 52. •?•
ذ		29.54 140.1E	700414	712a		50 JEO		120	50		60					+11 + 7
•		21.24 134.5E	1500F [		003	25 060					60	5				
5	240504	21.4N 117.4E	1500F1	1	003	15 150	50	220	51	110	40	10	5			·2* ·25 · 8   30

### TROPICAL STORM ROGER

## CATELLITE FIXES

FIX	TIME	FTX					
NO.	(7)	P0511ft#	ACCRY	DAJSAK CODE	SATFILITE	CJAMENTS	SITE
• 1	0 > 1 2 3 3	13.5× 135.7E	Prw 5		DMSP39		PGTW
5	031513	14.1. 138.6E	PCN 5		DMSP36		PGTW
3	n 32036	20.9% 134.9E	PCN 5		D45631		PGT⊎
•	032313	20.54 136.4E	Pry 5	T1.0/1.0 /50.0/24HR9	DMSP36		PGTW
5	040055	21.94 135.7E	PCN 5		DMCH30		PGTW
6	040055	20.74 135.6E	PCM 5	11.5/1.5	DMZD34	INI 1 345	RPMK
1	040317	21.94 135.2E	PCN 5		DUSPRT		PGT#
ь	041154	34.FE MT.15	PCN 5		Decase		RODN
ÿ	041155	21.5N 133.5E	PCN 5		DMSP36		PGT#
10	042157	19.90 137.1E	PCN 6	12.0/2.0 /01.0/22HR9	DMSP37		PGTW
ii	046158	20.34 137.6E	PCN 5	T:1.5/3.5	DMSP37	IN1 Jds	RODN
15	050036	20.04 133.8E	PCN 6		DUCDZA		PGTW
13	050217	20.24 133.3E	PCN 6		DMSP39	EDGE OF DATA	PGTW
1.	050217	20.04 133.5E	PCN 5		DMSP14		RPMK
15	050317	21.34 131.3E	PCN 5		DMSP34		RODN
16	051317	21.74 135.6E	PCN 3		DMSP39	EXPUSED   LCC	PGTW
17	051317	21.74 135.6E	PCN 3		DMSP39		RODN
lø	051317	21.4N 135.7E	PCV 5		045939		RKSD
1+	051314	21.94 135.4E	PCVS		DMSP36		RPMK
20	051319	21.4N 135.7E	Pry 3		DMCD 34		PGT
21	052137	23.4N 134.4E	Pry 5	T1.0/2.0 /W1.0/24HR	BMSP37		PGTW
2.2	06-019	23.9N 135.0E	PC4 '5		DMSP36		PGTW
23	060158	24.4N 135.0F	PCN 5	F3.1/3.0	DMEDJO	INII J4S	RPMK
24	060158	24.14 135.1E	PCN 5	, , , ,	045939		PGTW
25	060158	24.24 175.0E	Prv 5	T3.0/3.0	Despay	INII JOS	RK\$0
26	061017	26.54 134.5E	Pry 5	1 3 • 0	DMSP37		RKSD
21	061018	24.84 134.2E	PCN 5		Duspa7		RPMK
5.9	041015	75.14 1 .0E	Pry 5		DMSP37		PGTW
24	041257	27.34 1 5.4E	PCN 5		DHSP39		RKSD
30	041301	27.1% 1 15.1E	PCN 5		DHSP34		PGT
31	061301	24.90 135.4E	PCN 5		DMSP36		RPMK
32	066117	29.00 136.3E	PCN 6		Dusp37		PGTW

## ATRCHAFT FIXES

FIA NU.	T1ME (7)	F7X 2051710H	FL¶ I,¥L		085 45LP										EYE SMAPE	-M31HO 3YA MOLTATIWAJC	PER TEMP (C)	45 <b>%</b> 40.
1	020220	14.14 140.28	15n0f		998	40	180	50	A 411	30	180	60	5	5			٠/١ ،24 ٠24 علام	,
5	040308	21.16 176.7E	15nBFI		382	35	080	10	150	35	080	10	1	4			+5+ +53 +54	3
	044305	21.2N 135.1E	1500F1		4A7	.0	130	25	100	40	030	Ž٩	2	5			AC 65. 65. 65.	•
•	041450	20.34 133.5E	700MM	3003					430	32	210	60	4	•			-15 -11	>
•	044125	20.44 133.7E	70046	1015	992	35	160	10	040	36	320	45	5	3			.13 .19 . 6	5
ь	951040	24.14 1 14.5E	TOOMM	3001		40	>20	10	140	48	120	85	5	5			+15 +15 +10	н

## SYMPOTIC FIXES

	ı.	T T M E (7)	F14 P0511100	INTENDITY ESTIMATE	NEAREST Data (N4)	COMMENTS
	ı	010000	13.0v 1+1.1F	20	120	
٠	2	011500	13-14 130-0F	20	240	
	3	020000	12.74 142.0F	ن خ	510	
	٠	044040	24.04 134.5E	40	10	
	ź	061200	27.0N 135.5F	45	70	
	ô	070000	11.54 137.0F	35	190	

### TYPHOON SARAH

## SATELLITE FIRES

FIA NO.	1145 (7)	505171(IN	*CC44	UVORAK CONE	SATELL 11E	CJMMFNIS	SITE
• 1	012259	16.20 121.0E	PCN >	71.0/1.0	Dadn 11	INIT JES	RODN
• 2	020131	17.54 122.8E	PCN 5	TU-0/0-0	DHZh sk	INIT DOS	RPMK RPMK
: :	021134	14.44 120.4E	PCN 5		D#2534 0#4540		RPMK
• 5	021414	14.00 120.1E	PCN 5		Dechia		RODN
6	025538	15.54 121.75	PCN 5	10.0/0.0 /SU.0/21HRS	DMCHII		RPHK
7	6110F0	14.54   110.HE	PCN 5	11.0/1.0 /50.0/26HRS	045634 046634		RODN
- ;	010235	14.64 11A.9E	PCN 5		PERPO		ROUN
• 1u	071355	15.4M 119.2F	PCY 5		DHEPTA		RPMK
• 11	014518	15.34 119.0E	PCN 5	TU.0/0.0 /50.0/24HRS			RPMK RODN
• 13	040055 040235	14.39 110.1E 15.1M 118.ME	PCN 5	12.0/7.0 /01.0/24HRS	DMZD10		RPMK
1.4	041958	11.34 119.0E	PC4 5		Dac 17		RODN
• 16	066140 766140	14.4H 111.6E	PCN 5		Dece se		PGT# RPMK
10	044157	15.0H 110.ME 13.5H 110.JE	PCN 5		Decede		PGTW
18	050036	12.84 119.1E			DAZBAV		PGTW
1 4	0503b	12.44 119.1E	Pru 5 Pru 5		D#45611	INI Jes	PGT# PGT#
51 50	050217	17.5N	PCN 5	T2.0/2.0 T1.5/1.5 /N1.5/2AHRS		[4]1 305	RPMK
55	050217	12.50 119.IE	PCN 5	12.5/2.5 /00.5/25HKS	DMED 14		RODN
23	051036	12.14 119.25	PCW 6		Dusp 17 Dusp 19		PGTW
24	051317 051317	17.3% 119.0E	PCN 5		044514		PGT# RODN
26	051319	12.34 119.25	PCN 5		DUSPIA		PGTW
21	051319	12.34 119.2E	PC4 5		DMCDAM		RPHK
58	052319	12.3N 114.9E	PCN 5		D45P37 D45P37		RODN RPHK
J.	040016	12.34 119.98	PCN 5		DMSPRA		PGTW
31	040159	12.44 110.7E	PCN 5	T2-0/2.0 /50-0/24HRS	DHEBRO		PGTW
32	0640158 064018	12.34 119.5E 12.24 119.3E	PCN 5	T1.0/1.5 /WU.5/24HRC	() MSP34 () MSP37		RPMK RPMK
33	041018	12.5% 119.9E			DMSP37		PGTW
35	041301	12.20 [19.1F	Při		DMSPRA		APMK
36 37	106140	17.44 110.6E	PCN 5		DMEDAV		PGTW RODM
36	041434	12.1N 119.4E	PCN 5		Dechia		RPHK
39	645240	12.24 110.28	PCN 3	T2.0/2.0 /11.0/21HRS	DUSPAA		RPMK
40	0455240	17.0N 120.0E	PCN 3	12.5/2.5	DMSP37 DMSP39	INI Jes	RODN
41	070138 070137	12.24 119.3E	PCN 3	12.5/2.5 /00.5/24HRS	Daceia		PGT# RODM
4 3	074143	12.24 119.38	PC4 5		DWSPRA		RPMK
44	070240	11.4"   11H.1E	Pry 5		D= <p39< td=""><td></td><td>RPMK RPMK</td></p39<>		RPMK RPMK
45	071139	12.14 110.3E	PCN 5		DMSP37		RODN
47	071242	11.5N 118.4E	PCN 5		DMCP3A		RPHK
48	071243	11.94 119.3E	PCN 5		DMSP IA		PGTW
<b>4 →</b> 50	071420 072238	17.0N 119.3E	PCN 5	13.0/3.5+/00.5/24HRS	DMCP19 DMCP17		RODN
51	072238	35.011 will	PCN >	15000 31 30000 30 20000	DMSP37		RODN
52	040124	11.2N 119.3E	PCN 5		AFGPHO		RPMK
5 ) 5 4	0#0301 0#1118	11.74 119.5E	PCN 5	13.0/3.0 /D0.5/2AHRS	PFGPMG :	PSN CYTE OF COO	RODN RPMK
55	041118	10.31 114.36	PCN 5		DMCP37	NO LYE/PON BASED ON 2 CR BANDS	RODN
56 57	041406	10.9N 119.2E	Pru 5		0m263V	CI UP/JUTFLOW INCREASED	RPMK
51	044518	10.9% 119.3E	PCN 5	74.074.0 /01.5/21HRS		}	PGTW
54	084518	11.00   118.1E	PCN 5	T4.0/4.0 /01.0/24HRS	DMSP37	,	RPMK
50	090107	11.24 ITA.0E	Prv I	T4.5/4.5 /D1.5/22HRS	AFGPHU		RODN
62	091058	11.10 118.0E	Pry J Pry J		D#4654		RPMK RPMK
6.3	091059	11.4N 117.4E	PCH 1		DHSP37		RODN
64	091342	11.6W 117.1E	Prw 1 Prw 1		Dece sa		PGTW
65	091342 091348	11.40 117.4E 11.40 117.3E	PCN 1		DR4534		RODN RPMK
67	092158	11.40 114.5E	PCN 1		DMSP37		RPMK
68	100049	35.411 Weell	PCN I	15.0/5.0 /D1.0/26HRS	AFGPWG :		RPMK
69 7u	100049	11.3N 116.4E	PCW I	15.0/5.0 /01.0/26HRS			PGT# RODN
71	101038	11.74 116.1E	PCN I	12017113 7111101 231111	DMSP37		RPMK
72	101038	11.5M 116.0E	PCN 1		Decased		RODN
73 74	101038	11.96 11A.1E	Pry I		045P37		PGT# RPMK
75	101331	11.5N 115.9E	PCN C		DMSP3A	_	RODN
76	101504	11.96 116.0E	PC4 6		DM49 14	ESTIMATE CHTH OFF EDGE OF DATA	RPMK RPMK
77 78	1n2319 1n2319	12.1N 115.7E	Prn 3	T5.0/5.0 /S0.0/27HR9			RODN
79	110031	17.04 115.5E	PCN 3		DMZBJY		RPMK
80	110504	12.0H 115.2E	Pry 3	14.5/5.0 /WO.5/25HRS	DMSP14		PGTW
H2	111018	12.34 114.HE	PCN 5		DMCD17		PGTW RPMK
83	111312	12.4N 114.7E	PCN 3		DMSP36		PGTW
64	111445	12.4% 114.3E	Pry 3		DHED 34		RPAK
#5 #6	111445	12.5N 114.3E	Pry 5		Decase		RODN
87	120154	13.0%   114.0E	PCN 5	14.5/5.0 /#0.5/26HRS	DMSP3A		RPMK
8 B	120154	12.34 114.36	Pry 5	13.5/4.5 /W1.0/26HRS			RODN
84	120356	13.0% 113.9E	FEN 3		D=45 14		454

90	121139	13.30 117.0E	PCW 3			45037				RPMK			
91	121426	13.44 112.48	PCN 3			45034				RPMK			
92	121426	13.44 112.8E	PCN 5			44b 30				ROUN			
93 96	122538	13.00 112.3E	PCN 5			45037				RPMK			
95	8655¢[ 8610F1	13.2N 112.5E	PCN 3 PCN 5 13.5/			45037 45034				4004			
96	130307	13.IN 112.4E	PCH 1	4.5 /#1.0		4650 10				RPMK RPMK			
97	130307	17.3N 117.4E		5.0 /01.5		45039				ROOM			
96	171119	13.60 111.7E	PCN 3	3.0 /(/1.2		45037				RPMK			
99	131119	13.4N 111.7E	PCN 3			45037				RODY			
100	131401	13.4N 111.6E	PCN 3			W 837				RODA			
101	131407	13.7N 111.1E	PCN 3			45034				RPMK			
102	140118	13.5N 110.7E	PC4 5 T2.5/	3.5 /41.0	/24HRS D	AFUZA				RPMK			
103	140248	13.4N -110.7E	PCN 3		0	45750				RP4K			
10+	140248	13.34 110.7E		5.0-/41.0		M&6 3.4				ROUN			
	141058	15.34 TUO.0E	PCN 3			45027				ROUN			
+106	141058	17,34 109.5E	PC4 3			45037				RPMK			
107	141348	13.50 Tud.SE	PCN 5			450 30				PGTW			
108	141348	13.04 109.5E	PCN 5			45 D 3 G				RODY			
110	141359	13.1v 100.2E	PCN 3 PCN 5 TL-5/	141 4		4503K				RPMK			
111	150229	13.2N 10A.7E	PCN 5	7.5 /W1.0		45977 45970				XM4X			
iiż	140227	13.34 107.9E		3.0-/42.0		45030				ROOM			
-11	140567	scele foresc	764 - 14407	3.0-/45.0	, E 4411 - D-	- 1- 14				#004			
					A1 3C	PAFT FIXES							
FIX	TTME	FTX	FLT 70043	DBS MA	X-SEC-WVD	MAX-FLT-LYL-	- MMD	ACCRY	EYÊ	FYE DRIEN-		101 4	٠.
NO.	(7)	P051T10H	LVL HGT			DIN/VEL/SHO			SHAPE		C 741 74110 .		
									• • • • • • • • • • • • • • • • • • • •	•••			-
1	051001	12.6N 119.3E	700MH 3017	991 4	5 360 50	340 35 Z/U	30	₹ 4			*1* *17 *	7	1
2	040342	12.4N 119.7E	700MB 3055		0 010 50	130 35 010	30	ત્ર ♦	CIRCILLAR	Su	·14 ·13 ·		ŝ
3	070203	12.24 110.4E	700HB >994		0 030 11	n4n 50 360	15	3 5	CIRCILAR	50	•15 •		٠
•	070431	15.5H 110.3E	100MH 2970		5 130 10	340 73 2/0	10	7 4	CIRCILLAR	5u	+11 +19 +		٠
5	01200	11.3N 110.5E	700MB 2920		5 300 >0	120 78 360	50	9 5	CIRCULAR	10	•f1 •f5 •		5
5	090512 090405	11.1w 110.2E	700MB 2922 700MB 2761		5 n80 5	052 04 ncr	30	3 4	CIRCULAR	R	111 115 1		5
ų,	100142	11,3N 117.9E	700MB 2496		Q 140 10 Q 060 5	15n 93 060	20	5 2	CIRCULAR	20	*11 *19 *		7
ű	100172	11.7N 114.4E	700MB 2489		0 180 7	070 115 020	1"	3 1	CIRCILLAR	15	10 65. • 65. 11.		΄,
10	110131	12.0N 115.4E	70046 >737		0 070 50	12n 73 geV	12	. 2	COMPILENCE	17	*11 *63 *	•	ė
ii	110343	12.04 115.2E	7ng46 2/33		5 130 25	040 74 320	15	4 2	CIRCILLAR	12	+14 +13 +1	1	ø
12	120700	12.9N 117.6E	700MB 2784		5 080 20	240 70 140	50	š ,	CIRCILAR	• •		•	ÿ
13	120923	13.1N 113.4E	700MB >784		5 180 30	110 63 040	5.0	5 6			+14 +15 +	6	ý
					RAJAH	FIXES							
Fix	TIME	F 1 X		EYF	EY⊧	RANNH-CODE					PAGAP	SITE	
	(7)	POSITION	RADAR ACTRY	SHAPE	DIAM	ASWAH TOOFF			COMMENTS		POSTTION	W40 40.	
	.,,	P03111104	MADA- ACTAI	SHAPE	D1				COMMENTS		-0311134	#40 40.	
1	041208	14.1N 119./E	LANO								16.3m 120.6E	98321	
Z	041300	13.8N 119.8E	LAND	CIRCULAR							16.34 120.6E		
3	041308	14.0N 119.5E	LAND								16,3M 120,6E		
•	041800	13.4N 119.2E	LAND								16.34 120.6E		
5	040000	13.5N 119.0E	LÀND								13,74 100.6E	48455	
					EYMAST	IC FIXES							
					31-4(1-)	1463							
	TTHE	FTX	INTENSITY NE	AREST									
NO.	(7)	POSTTION	ESTIMATE 1	TA (NM)		COMMENIS							

1 011200 14.5N 120.5E 2 020000 15.0N 121.0E 3 030000 15.0N 121.0E 4 041200 14.0N 119.8E

## SUPER TYPHOON TIP

## SATELLITE FEALS

FIA NO.	17ME (2)	F1X P051710H	*CUBA	DAUSEK CODE	SATFII ITE	CJ4MFNTS	SITE
	041154	5.9%   152.9E	PON 5		Duspay		PGTW
2	042016	4.5" 154.7E	PCN 6	T1.0/1.0	DMCD37	INI Das	PGTW
•	りとりょうり	4.3× 154.7E	PCM 6		DWSDJA DWSDJ7		PGTW PGTW
>	051137	4. 34 [ H7.4E	Pru 5		DWCh31		PGTW
7	056537 056537	7.24 152.8E	Prv 6	T2.0/2.0 /01.0/26HRS	Dugu 37		PGTW PGTW
	040016	1.04 157.86	Pry 4	Transcap Solida	DWZBSA		PGTW
1 u	041116	7.44 157.05	Pry b		0 m 5 D 7 T		PGTa
ii	611140	7.64 152.4E 7.64 152.8E	Prv 6	12.5/2.5 /00.5/25HRS			KG#C PgT#
15	045513	7.5% 153.7E	Prv 6		DMZHAV	FOR COMPTDENCE	PGTW
13	070416	7.30 152.1E	PCN 6		Dachay		PGTW PGTW
15	012338	7.64 151.4E	Pru 5	13.0/3.0 /01.0/24MRs	0ゃとちょう		PGTW
16	040755	7.611 152.1E 9.14 151.2E	PCN 5		Dwsp34 Dwsp37		PGTW
io	041043	4.4M 151.0F	PcN 4		DWZDSY		PGT# PGT#
19	092037	11.5M 140.HE	E MUS	-2	DMSP37		PGTW
51 50	000101	11.7N 14H.7E	PCN 3 PCN 3	13.5/3.5 /00.5/24HRC	0 45 45 MG		PGT# PGT#
22	002016	12.9" 142.7F	Prn +	_	DMSP37		PGTW
23	5+0uni	13.24 142.7E	PCN 3	15.0/5.0 14.5/4.5	0m263a 0m263a	INI 198	RODN
55	10042	13.04 142.48	Pry 3	T4.5/4.5 /D1.0/25HRC		1411 202	RPMK PGT₩
26	100457	13.74 141.4E	PCN 6		DMSP 17		PGTW
• 21 25	101144	14.29 ]41.0E 13.90 ]+1.1E	Pru b Pru 2		TEGPMO AFGPMO		RODN PGT w
29	1.1149	13.94 141.3E	PON 2		DHSPRA		RPMK
30 31	101149	13.1. 141.0E	PCN P		DMSP36		RODN
32	110031	14.1% 130.7E	PCN 1 PCN 1	16.0/6.0 /01.5/24HRS	AFGPHQ AFGPHQ		RPMK PGTW
33	111018	14.9, 130.38	PCN I		DMSP 17		RODY
34 35	111131	15.0% 130.1E	Prn 4 Prn 1		DMSP36		PGTW
36	112117	14.44 130.2E	Pry	17.5/7.5	Dwenss Dwenss	INII Jas	RPMK Roun
31	114117	14.14 138.5E	Pry I	F7.0/7.0	DMSP37	INII Jas	PGTW
9 F	120012	14,24 130.2E 14,44 134.3E	PCN I	77.0/7.0 /01.0/25HHS	DMGD34		PGTW
40	120145	16.54 148.0E	PON I	TITOTION TO THE	DMCD44		RPMK PGT#
41	120957	14.94 137.3E	PCN I		DACESI		PGTW
42	121524	17.04 137.2E 16.94 137.2E	PCN 1 PCN 1		DMCBJY		PGT# RODN
44	1 > 2 0 5 7	14.74 134.3E	PCN 1		DWSP37		PGTW
40	122354	15.54 136.1E	Prv 1 Prv 1	10.5/7.0 /w0.5/27HRs	DMEBSA		PGTW
4.7	130126	16.54 136.1E	PCN I	17.0/7.5 /WD.5/29HRC	DMChia		PGT# Rodn
45	130337	14.50 135.4E	Pow 1		DMSP37		PGTW
50	141530	14.7%   194.4F 14.7%   195.4E	PCN 1		DMSP39 AF92MO		RODN PGTW
51	172036	16.9N 134.0E	PCN 5		DMSP37		PGTW
52 53	172336	16.9N 137.9E	PCN I	T5.0/6.0 /W1.5/24HRS	045834 046834		PGTW
54	140107	17.0% 133.8E	PCN I	16.0/7.0 /W1.0/24HRS	DMERSA		PGT# Rodn
55	140717	17.15 132.58	PON L		DMEDAT		PGTW
56 57	141206	17.39 132.2E 17.18 132.2E	PCN 1 PCN 1		04563A		PGTW RODN
58	141348	17.64 132.1E	PCN 1		DHEP19		PGTW
54 60	142157	17.91 131.2E	PC4 1	T5.0/5.0 /50.0/22HRs	DUSP 17 DUSP 19		PGTW PGTW
61	150048	14.14 131.7E	PCN 1	15.5/6.0 /WO.5/24HRC	Dadban		RODN
62 63	150059	14.0% 130.7E	PCN 2		DMCD34		PGT⊯
64	151038	14.2N 130.6E 14.2N 120.5E	PCN 5		D#45540		RODN PgTu
65	151200	13.64 129.3E	Pru 5		DHEBSH		PGTW
66 67	151329	18.54 129.2E 18.54 129.2E	PCN 5		OMED 10		PGTW RODY
68	152137	19.3N 129.2E	PCN 1	15.0/5.0 /50.0/24HRS	DMSP 17		PGTW
6 <del>7</del> 0	140041	19.44 129.1E	PCN 3		DMZB34		PGTW
71	140210	10.44 120.1E	PCN 3	15.0/5.5 /40.5/25HRC	Duchia		PGTW Rodn
72	141018	20.2H 12H.7E	Pru J		DMSP37		PGTW
73 74	141324	20.34 128.6E 20.34 128.7E	PCN J		7.F 42MQ		PGTW PGTW
75	170024	31.84 158.1E	PrN 3	15-0/5.0+/50-0/27HRS	DMSH36		PGT#
76 77	170151	21.4m 128.0E	PC4 3	*5. n.e. n	Duchia	TNTT 340	PGTW
78	170151	21.6N 128.0E 21.6N 127.9E	PCN 1	15.0/5.0 15.0/5.0 /50.0/ZAHRS	DMebia	INIT 365	RPMK RODN
79 60	170957	27.74 127.BE	PCW 3		DMSP37		PGTW
81	171751	21.04 127.8E	PCN 3 PCN 3		Dechie Dechie		RODN PGT#
82	112056	34.14 158.0E	Pry J		DMSP37		PGTW
H 3	172057	24.40 127.7E 25.00 128.3E	PCN 5	14.5/5.0 /W0.5/24HR4	D#4617 D#4614		RODN
85	140131	25.2N 12R.2E	PCH 3	T4.5/5.0 /W0.5/24HRS	Dwen in		PGTW RPMK
86 87	140132	25.24 129.0E	PCN 3		Duspay		PGTW
88	140132	24.44 128.0E 27.24 129.4E	PCN 3	13.5/4.5 /W1.5/24HRC	044P74 044P77		RODN PGTW
87	1AU+37	27.5v 120.4E	PCN 4		DMSP 37		RODN
90	141118	29.2. 129.6E	Prw 3		045937		RODN

91 94 93 95 96 97 98	141231 141248 142036 142348 140112 140112 141212 141212 142016	29.6N 130.5E 24.7N 130.5E 30.6N 131.8E 32.7N 134.8E 37.8N 134.6F 37.3N 135.2E 41.1N 145.6E 41.1N 145.5E 43.7N 146.4E	PON 5 PON 3 PON 3 PON 5 PON 5 PON 5 PON 5 PON 5	3 3 T3.0/4.0 /W1.5/24HRS ( 5 T4.0/4.0 ( 6 )					EXPSU	.ucr	:				RPMK PGT# PGT# PGT# RK>O PGT# RODN RKSO RKSO				
							4 F 7C+	PAFT /	IXES										
FIX NO.	TTME (7)	FIX POSTTION	FLT	70043 HGT	OBS MSLP				-FLT-LVL- 'VEL/BNG				EYE SHAPE		ORIEN- FATION	₽¥F	TEMP		45N 40•
1234567890100000000000000000000000000000000000	040 146 050030 050810 050810 050810 051989 052222 0402111 0703017 0703017 0703017 0703017 0703017 0703017 0703017 0703017 071928 071926 0902621 090621 090621 090621 090621 111023 091201 111023 1111029 11110	4.24 153.0E 5.44 154.5E 5.44 154.5E 7.24 155.4E 7.24 155.4E 7.24 155.4E 7.44 157.3E 6.94 157.3E 6.94 157.3E 6.94 157.3E 6.94 157.3E 8.94 144.3E 8.97 144.3E 8.97 144.3E 8.97 144.3E 8.97 145.6E 8.97 1	15.00F I 70.00E	7095 7117 7124 7117 7124 7117 7127 7117 7127 712	1004 1003 1003 1003 1005 997 995 995 989 989 989 989 989 989 999 999	25 276 25 270 25 270 25 270 25 270 25 270 25 270 25 270 25 270 26 270 270 28 270 270 270 270 270 270 270 270 270 270	400 122 300 205 155 300 555 30 201 105 105 105 105 105 105 105 105 105 1	790 1 140 1	29 180 33 360 37 360 37 27 360 36 010 26 010 31 270 32 310 31 270 32 310 33 350 35 350 36 310 44 130 48 130 49 100 100 100 110 100	167000000000000000000000000000000000000	5778457454565555777771	56425240555554	CINCILAR CINCILAR CINCILAR CINCILAR CINCILAR CINCILAR CINCILAR CIRCILAR	15 to	130	- 1   - 1	12 · 12 11 13 11 11 11 11 11 11 11 11 11 11 11		1 2 3 3 4 4 4 5 6 7 7 7 7 8 8 8 9 9 9 9 10 11 11 12 2 13 3 1 1 4 4 1 1 1 1 2 2 1 1 3 3 1 1 4 4 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2
	TIME	Ftr			EYE			8 FTY	s-cope							нара		<b>6] }</b> F	;
NO.	(7)		HADAR A	CCHY	SHAP				TOUFF			1	COMMENTS.			POSTT	04	#40 <b>4</b>	10.
1 2 3 4 5 6 7 8 10 11 12 13 13	094410 090435 090510 090510 090635 090710 090735 090810 090835 090935	12.04 145.8E	LAND LAND LAND LAND LAND LAND LAND LAND	FAIR FAIR FAIR G100 G100 G100 G100 G100 G100 G100 G10	CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH CTRCH	LAR LAR LAR LAR LAR LLAR LLAR LLAR	277711727711			WAL	L ne	PFN !	5E-54-N4-N			13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1 13,64 1	44.9E 44.9E 44.9E 9.9E 9.9E 44.9E 9.9E 9	0121 0121 0121 0121 0121 0121 0121 0121	6 8 6 8 6 8 6 8 6 8 6

10	041110	12.74	144.7E	LAND	6700	CIRCULAR	15					13.60	144.9E	91518
17	c+11+0	12.8"	144.5E	LAND	6700	CIRCILAR	15						144.9E	91518
14	021510	12.44	144.5E	LAND	670U	CIRCULAR	15 15						144.9E	91218
20	041310	12.90	144.3E	LAND	FAIR	CTRCILAR	15						144.9E	91218
51	001335	12.40	144.2E	CHAJ	GOUD	CIRCULAR	15					13.64	164.9E	91518
25	001410	12.40	144.15	LAND	6700	CTRCULAR	15					13.6N	144.9E	91218
23 24	091435	12.40	143.ME	LAND	6200 6200	CTRCHLAR	15						144.9E	91716
52	041510	12.7	143. ME	LAND	ดาบบ	CIRCILAR	15					13.64	144.9E	91518
26	021200	12.70	147. NE	LAND	GOOD	CTRCHLAR	10					13.69	144.9E	91516
27	001535	12.64	143.6E	LAND	670D	CIRCIILAR	10					13.6	144.9E	91516
58	091710	12.74	141.NE	LAND	6000	CIRCHLAR	10					13.68	164.9E	91216
30	041410	12.40	143.5E	(AH) CAND	6700 6700	CIRCHLAR	10					13.00	144.9E	91518
31	0-1-35	12.9.	147.3E	LATIO	6100	CIRCULAR	7					13.6N	144.9E	81510
35	041910	12.40	143,3E	LAND	6700	CIRCHLAR	10		HUY	ATTENVATION		13,6N	144.9E	91518
وو	しのようろう	12.44	143.3E	LAND	GADU	CTRCHLAR	10					13.64	144.9E	91518
34	045010	12.34	147.1E 127.RE	LAND LAND	FAIR G100	CIRCHLAR	10 45			MOVR 3410		13,6N	144.9E	9121 <b>8</b> 47927
35 36	171230	33 344	127 7E	LAND	6100		45			MOVE 3210		24. HM	25.3E	47927
37	171500	23.50	127.7E	LAND	GOUU		45		Eve	MOV6 3420		24.8N	125.3E	47997
38	171500	23.74	127.7E 127.6E 127.6E	LAND	6200		45			MOVE 3450		24.8N	125.3E	47927
39	171700	24.34	127.6E	LAND	GOUD		45			MOVG 3420		24.84	125.3E	47927
*1	171708	54 ° U /1	127.36	LAND	POOR			3///3 53/10		MOVE 3205			127.8E	47937
- 22	171700	24 14	127.4E 127.5E	LAND	POON					Mnve 3615		26.3H	125.3E	47929
4.5	171900	24.3.	127.8E 127.6E 127.7E	LAND				6///2 7031	1			26.2N	127.BE	47937
44	172000	24.2.	127.6E	LAND	POUR					MOVE 0115		26.34	126.BE	47929
45	172000	24.51	127.7E	LAND				6///3 7021	ı			20.2	127.06	47997
46	172035	24.94	127.5E	LAHD QMAJ	FAIR				F	MOV6 3415		26.48	127.BE	47991
48	172100	24.51	127.7E	LAND	PIJOR			6///3 7011		H.141. 3413		26.2N	127.BE	7937
49	1-5500	24.54	127.4E	LAND	6500				EVE	MOV6 3520		26.3N	126.BE	47929
50	172200	24.74	127 AE	LAHD				A///3 7360	3			26,2N	127.8E	47997
51	17235	25.00	127.58	LAND	POUR			5///1 7020				26.4N	127.8E	47937
25	174310	24. RN	127.9F	LAND	POUN			4///1 /020	•				121.0E	47991
54	172320	24.94	127.7E	LAND	POOR				FvF	MOVR 3520		24.AN	125.38	47997
55	172335	24.94	127.8E	LAND	POOR							26.4H	127.8E	47931
56	10000	24.9W	129.0E	LAND	GNUU		40		EVE	MOVR 0220		26.3M	126.85	47979
57	140000	25.14	127.4E	LAND				3//19 7011				26.2N	127.8E	47997
58 57	140010	25.14 25.24	127.86	LAND	POOR							26 AN	127.8E	47941
60	180100	25.2N	124.0E	LAND	PHOR			3//12 70300	1			26.2N	127.8E	7937
61	140120	25.24	12A.1E	LAND	6100		40		EVE	MOVR 0420		26.3₩	126.8E	47999
65	140135	25.54	127.9E	LAND	POUR							26.44	127.8E	47931
63	140200		124.0E	LAND	6000		45	3//12 70111	FUE	Mnva 3430		26.2M	127.8E	47937 47929
65	140510	25.5N	124.1E	LAND	PhOR		• • •		EAE	MUAH 3430		26.AN	120.0L	47931
66	180235	25.7N	129.16	LAND	POUR							26.4N	127.8E	47931
67	1 RU 300	25.7N	124.5E	LAND				3//42 70514	,			26.2N	127.8E	47937
68	140300	25.7N	124.3E	LAND	GOOD		45		E∀€	MOVR 0320		26.3N	126-85	47979
• 69 70	1#0310 1#0335	25. 7N	127.3E	CHAJ	POOR POUR							26.4M	127.8E	47931
71	180400	26 14	128.5E	LAND	POR			6//42 7021				26.2M	127.0E	47997
72	190400		124.1E	LAHD				65/// 5///				28.4N	129.5E	47909
73	190400	26.04	129.4E	LAND	6200		44		EVE	MOV8 0335		26.3N	129.5E	47999
74	100410	24.2N	124.5E	LAND	POOR							26,48	127.8E	47931
75 76	140435	24.4N	128.7E	LAND	POOR GOOD							26,6M	127.8E	47991
77	140445	24.44	12R.4E 178.4E	LAND	6100				FVE	MOVE NNE		26.2N	127.7E	47930
78	140500	26.4N	12A.4E	LAND	0.,-5			65/// 5032		•		28.44	127.5E	47909
79	190500	26.5N	12A.5E	LAND				///4 7022	?			26.2M	127.8E	47997
40	10000	26.3N	124.5E	LAND	GAOD		6.0		EVE	MOVG 0235		26,3N	150.BE	47999
81 81	190510	26. 9	128.4E	LAND	POOR POOR							26.44	127.8E	47991 47931
83	180545		128.6E	LAND	POOR							26 24	. a. 75.	47970
84	190545	24.54	124.6E	LAND	PODR					MOVE NE		26.2N	127.7E	AT990
85	1 AU 600	24.60	124.7E	LAND	FAIR		45		EVE	MOVA 0330		26.3₩	126.8E	47999
86	190600	24.6N	129.7E	LAND				6///4 7021	<u>'</u>			26.24	127.8E	67937
87 88	140500	26.34	128.5E	LAND	POOR			AS/// 50509	•			26.4	129.5E	47909 47931
89	140700	27.0N	129.0E	LAND	/ 471			A///2 7032	•			26,2₩	127.BE	47937
90	140700	24.9N	128.7E	( AND	POOR				EYE	MOV8 0230		26.3W	126.8E	47999
91	190700	24.94	128.9E	LAND				A5/// 50436		Maua 5:25		28,4W	124.5E	47969
92 93	180800	27.1N	128.9E	LAND	POOR			4 4 4 4 2 9 9 9 4 4 4		MOVR 0435		26.3N	126.8E:	47999
94	180900 180900	27.1N 27.2N	129.6E	LAND LAND				6///3 70616 64/// 50321				28.44	129.5E	47909
95	180700	27.54	129.3E	LAND	POOR				FVF	MOVR 0445		27.44	129.7E	47942
96	140900	27.74	129.5E	LAND				////3 70516 65/// 50519 65/// 50316	,			26,20	129.7E	47997
97	140900	27.5N	129.3E	LAND				65/// 50519	•			28,41	29.5E	47909
98 99	141000	27.7N 27.7N	129.55	LAND	POUR			nn/// 50316	FVE	MOVR 0335		27.44	127.3E	47909
100	141000	27.9N	170.85	LAND	POOR					MOVR 0640		27.4M	28.7E	47942
101	1 = 1 100	29.0N	120.7E	LAND	. ,			65/// 50324	,			28.4N	129'-5E'	47989
105	101200	29.3N	129.85	LAND				55/// 50316	,			28,40	129.5E	47909
103	141300	24.44	130.0E	LAND				45/// 5042 45/// 5052	:			75.40	123-86	47989
104	1=1500	2H. AN	130.4E	LÂND LÂND				6///2 8///	,			38.6	129.5E	47869
106	181500	29.14	130.96	LAND				45/// 50629	,			28.4N	129.5E	47989
107	141600	29.4M	131.3E	LAND				6///1 5062	•			30,64	131.0E:	47569
108	141700	29.6N	131.6E	LAND				A///1 50524	:		KUSHIMOTO	30.64	131.08	47849
109	142330	3/a?N	134.2E	LAND	POOR						- V371MU10			

## SUPER TYPHOON VERA

## SATELLITE FIXES

FIX NO.	1145 (7)	FIX POSTTION	ACCRY	OVORAK CODE	SATFIE TE	CJ4MFNTS	SITE		
	.,,	P0311104		OVOVER CONE			22		
	372316	6.2N 149.0E	PCN >	Ti.0/1.0	AFGPMG	INII Jas	PGf#		
į	010026	6.24 148.9E	PC4 5	7	Dechad	2	PGT∉		
3	010814	6.04 14A.3E	PCN 6		045037	CI UP	PGT#		
•	011126	6.3N 147.0E	PCN 5		PF GRMG		PGT# PGT#		
5	011158 012055	6.3N 147.2E 6.9N 146.7E	PCN 5		Dechis		PGIW		
7	012258	6.9N 14A.DE	Pry 5	T2.0/2.0 /01.0/24HH			PGT		
8	020007	6.6N 145.7E	PCN 5		044654		₽GĨ₩		
9.	020935	7.2N 163.4E	PC4 >		Duchil		PGT#		
10 11	021140	7.2N 143.6E	PCN 5		045974 045974		PGT# PGT#		
iż	8451<0	7.1N 143.4E 6.9N 143.2E	PCN 6		Duspay		RPMK		
13	022034	7.54 141.5E	PCN 3		DMSP37		PGTW		
14	120060	9.3N 141.0E	PCN 3	13.5/3.5	DMGB36	SPC 11NI	RODN		
15 16	150020	7.9N 161.1E R.2N 161.7E	PCN 3	T3.0/3.0 /01.0/25HRS	PERSENG :		PGI# PGI#		
17	030914	9.0N 137.8E	PCN 6		DMSP37		PGT#		
18	8551F0	4.24 137.1E	PCN P		DMSP39		PGTW		
19	0.41558	9.4N 137.2E	PCN 5		DMSP39		RODN		
20	011302	9.24 136.9E	PCY 6		DWSP34 DWSP37		PGT# PGTW		
25 51	032155 040003	10.5% 133.8E 10.5% 133.0E	PCN 1 PCN 1	T5.0/5.0+/02.0/24HRs			PGT#		
23	040110	10.54 132.7E	PCV I		Dwebsd		PGT#		
24	040110	10.54 132.6E	PC4 I	T5.0/5.0	DMCB39	INII Jes	RPMK		
25	041035	11.44 129.7E	PCA S		0wsp37		PGT#		
26 27	041244	11.9N 120.0E	PCN 2		DHERTA		PGTM RODN		
28	041351	11.4N 12A.7E	PCN 2		DMSP39		PGTW		
29	042135	12.44 126.6E	PCW 1	15.5/6.5 /DO.5/22HR			PGTW		
30	042135	12.5N 126.5E	PCN I	-4	TF4PMG :		RPMK RPMK		
35 31	050126 050232	12.9N 125.9E 13.1N 125.9E	PCN 1	16.0/6.0-/01.0/24HR	DWZD3A	INIT DOS	RODY		
33	050232	13.14 125.8E	PCN I	100371123	Duchsa	1.11 5-3	<b>ЯРН</b> Х		
34	051915	14.14 124.4E	PCN 2		DMSP37		PGTW		
35	05 226	14.44 127.9E	PCN 1		DMSP34		PGTW		
36 37	051332 051332	14.64 123.6E	PCN 1		D#4630		RODV PGT#		
38	051408	14.5N 123./E 14.5N 124.1E	PCN 1		DMSP36		RPMK		
39	052256	15.4N 122.9E	PCN J		DMSP39		RODN		
40	040108	15.6N 123.1E	PCN 3	14.5/5.5 /W1.0/27HRS			PGTW		
41	0A0109 0A0213	15.44 122.9E 15.78 122.3E	PCN 3	15.5/6.5-/W1.0/23HR	AFGPMG :		RODN RODN		
43	040513	15.9N 127.5E	PCN 1	76.0/6.0-/50.0/24HR			RPMK		
44	040754	14.7N 122.2E	PCN 3		DMCD37		PGTW		
45	041312	17.14 122.2E	PCH >		Dechar		PGTW		
46	061350 061351	17.2N 122.3E	PCN 5 PCN 3		AFGZMU		RPMK RODN		
48	045534	18.30 121.5E	PCN 3		OMSP37		RODN		
49	070050	18.5N 121.7E	PCN 5		7£ 45m0		PGT#		
50	070153	17.9N 121.7E	PCN 5	74.0/5.0 /W2.0/24HR	DMSP34 DMSP34		RPMK PGTu		
51 52	070154 071116	18.6N 121.7E 18.7N 122.1E	PCN 5 PCN 1	T3.0/4.0 /W1.5/25HR	DMCD37		RPMK		
53	071332	16.90 117.8E	PCN 5		AFGPMO		PGTW		
54		16.1N 114.5E	PCN 5		DWSP3A	APRNT LLCC	PGTW		
				•	TROPART F	xES			
	TTME	FTX	FLT			LT-LVL-4NO ACCRY	EYE EYE ORIEN-	FYF TEMP (C)	MSN
NO.	(7)	P051110H	FAF	HGT MSLP VEL/ARG	446 HINN	EL/BHG/HNG HAV/MET	SHAPE DIAW/TATION	TPPLEC AND ARING	40.
	0-0635	- A. AA. E-	1545EY	204 40 : 34	7 160	65 060 2n 5 2		.21 .24 .22	s
1	020625 030500	7.44 144.5E R.5N 139.3E	15nofT 7nomm	994 50 130 2971 70 090	5 350	46 240 30 5 7		•14 •10	•
5	030753	9.94 13A.4E	700MB	7946 7AZ	150	73 020 A S ?	CIRCULAR 17	+11 +15 + B	•
•	031933	10.14 134.7E	700MH	>720	120 1		CIRCULAR 20	•14 •11	5
5	032049	10.2N 134.3E	70046	2643 945 130 270 2399 130 110		125 270 In 5 3	CIRCHLAR A CIRCHLAR A	8 + 61+ ni+ 14 + 55+ 13	5
6 Z	040507	11.0N 131.5E	700mH 700mH	>399 130 110 >349 915		100 000 in 4 2	CIRCULAR	19 -14	ž
6	042125	12.5N 126.5E	70048	2372 919 120 330	3 240	[]] ]80 ]4 . 7	CUNCENTRIC 25 70	-14 -15 -14	7
9	050418	13.20 125.1€	7nomm	2413 130 n50	7 120 1	116 050 17 R S	0100 / 00 -	+15 +12	
10	507020	13.64 124.8E	700MH	2410 130 340	4 340		CIRCULAR 7 CIRCULAR 10	•1n •15 •15 •15 •15	8
11	710520 St5520	14.1N 127.3E	700MH 700MH	2557 2587 941 55 060	40 1An	103 110 30 4 2 85 070 25 5 1	CIRCILLAR 30 120	-15 -15 -15	ý
13	050000	16.3N 122.3E	700MH	2647 100 050	35	10	CIRCULAR		10
1+	042001	17.94 121.6E	70048		1 70	52 020 6n 5		+15 • •	11

#### RAJAN FIRES

Fla Nu.	[ †#E (7)	FTX POSTTION	HaUAR	ACCAY	EYE SHAPE	EYF Dlam	MAININ-COUE	COMMENTS	RADAH Vot11409	417F
1	0.0715	11.2N 130.7F	ACFI							
٤	050500	11.24 174.6F	L AHD				204/1 ////		10.3W 124.0E	54445
3	040505	13.54 125.5E	LAND				11255 301//		14.IM 123.0E	98446 98446
•	040500	14.74 125.3E	LAND				10111 53400		14.1m 123.0E	98440
5	050500	14.54 125.0E	LAND				2060/ ////		14.0m 124.3E	98447
b	040500	14.4N 172.7E	Į A:IĐ				10543 53515		14.14 123.0E	98446
7	054630	11.7H 124.7E	(A-ID				206// 53026		16.UM 126.3E	98447
5	05u70u	11.94 174.5E	LAND				257/0 54535		10.3M 124.0E	98446
*	044700	13.9N 175.1E	LAND				20211 53313		14.1M 123.0E	98440
1 0	1150800	11.41 124.4E	(AND				20211 53309		14, LM 123.0E	98440
11	050900	11.94 124.0E	LAVD				2045/ 53325		14.04 124.3E	96447
15	0 < 0 > 0 0	14.04 124.5E	LAND				2061/ 53125		14.0N 124.3E	98447
13	050300	17.94 174.68	( Avin				20211 52921		14.1M 123.0E	98440
14	0 = 0 + 0 0	13.3N 144.NE	LA-IO				21211 52921		14.UN 124.3E	08447
15	951000	14.14 124.5E	( A 40				202// 53314		14.0% 124.3E	98447
16	051100	11.34 175.5E	LAVO				301// ////		14.1# 123.06	96440
16	141300	16.34 12.0E	LAHD				20231 54714		14.1m 123.0E	98440
14	051400 051500	10.5V 121.HE	LAND				20211 53214		14.1# 123.0E	98440
50	041300	14.74 123.7E	LAND				10132 53414		14.1m ;23.0E	98440
51	051340	14.14 127.3E	LAND	Paux			10012 53414		14. IN 123.0E	98440
55	051300	15.00 123.6E	LAND						15.20 120.6E	98 7>7
22	051445	15.00 127.5E	LAND	POUR POUR					15.2N 120.6E	98327
24	062005	15.14 123.2E	LAND	PODR					15.24 120.6E	98327
وَجَ	042035	16.19 123.16	LAND	POR					15.24 120.66	98327
36	052110	15.24 123.1E	LAVD	POUR					15.2N 120.6E	98327
51	054135	14.24 123.0E	LAND	POUR					15.2N 120.6E	98327
20	0 6 6 2 1 5	12.34 122.9E	LAND	HUGA					15.2N 120.6E	48327
24	052235	14.34 122.9E	LAND	POUK					15.2N 120.6E	98327
. 30	952300	14.24 121.4E	LAND				1//////////		15.2M 120.6E	98327 98321
* 31	052300	19.64 122.HE	LAND				10543 53504		14.1N (23.0E	98440
35	052300	16.44 122.7E	LA-vi)	POUR					15.2M 120.6E	98327
33	040000	15.50 127.0E	LAND				1022/ 5////		16,3M 120.6E	983>1
34	06100	15.14 122.6E	LAHID				10543 53204		14. LN 123.0E	98440
JŚ	040100	14.74 122.48	LAND				202// 5////		16.3# 120.6E	98321
36	060500	15.94 122.5E	LAND				10543 53520		14.1M 123.0E	98440
37	040500	15.96 177.9E	(LA10)				1021/ 5////		36.05; WE.6E	98371
38	060300	14.44 152.4E	LAND				10543 53410		14.1M 123.0E	98440
39	040300	14.04 155.AE	LAND				1021/ 5////		36, 3M 120,6E	98321
40	040400	14.24 182.3E	LAND				10543 53411		16.3M 120.6E	98371
41	064440 064440	14.24 127.3E	Ann				10443 53411		14.1≈ 123.0€	98440
• 5	040500	14,34 172,HE	LAND				1083/ 43606		30.65; WE.DI	98321
••	040500	16.34 122.2E	LAND				10543 53409		14.1M 123.0E	98440
45	040500	14.60 122.6E	LAND				1074/ 43408		16.3W 120.6E	98371
+6	040700	14.54 122.5E	LAND				10543 53513		14.1W 123.0E	98440
•7	066679	14.5M 122.3E	LAND				1081/ 5321U 21253 527//		16.3H 120.6E	98371
48	041500	14.70 122.1E	LAND				15000 52705		16.3M 120.6E	98321
49	041500	17.34 122.1E	LAND				45/// 728//		16,34 120,6E	98321
50	944500	17.4N 122.0E	LAND				45/// 728//		16.34 120.6E	98321
51	041900	17.44 171.4E	LAND				45/// /////		16.34 120.65	98321
52	041300	14.7V 122.4E	LAND				1021/ 53406		16,34 120,6E	983>1
53	070100	17.94 121.1E	LAVO				207H1 52713		16.34 128.6E	98321
5+	070200	18.0N 120.7E	LAHD				20341 52915		16.3M 120.6E	98321 98321
55	070300	14.14 [20.6E	LAND				20341 52913		16.3M 120.6E	983>1
56	070300	THOTA IZACHE	LAND				45/11/11/11		16.3W 128.6E	983>1
5/	074540	34.05 MS.PE	LAND				45/11 /////		16.3N 120.6E	98321
58	070500	14.34 150.1E	LAND				53/// /////		16.3N 128.6E	98321
59	070700	14.44 120.2E	LAMD				75742 242//		16.3N 120.6E	98371
60	074300	14.34 110.4E	LAND				40/// 728//		16.34 120.6E	983>1
									(23444	

## SYMM-THE FIRES

FIX	TIME		********		
		FfY	INTENSITY	<b><i>YFAREST</i></b>	
NO.	(7)	P0577104	FSTIMATE	CHM) ATEC	COMMEN IS
	290000	4.0% 15A.5E	<b>n</b> 5	60	
2	501500	4.84 154.5E	65	120	
3	300000	5.0% 158.0E	ĵū	225	
	301500	30.04 157.0E	ō5	320	
5	310000	4.04 151.0E	ĨO	90	
6	314200	6.0N 149.UE	i5	75	
7	071200	17.04 110.DE	30	30	
8	040000	15.50 117.5F	20	an .	
4	091200	15.0W 117.UF	າ້າ	130	

## TROPICAL STORM WAYNE

1 070012 17.74 160.7E PCN 5 2 070935 13.00 137.5E PCN 6 3 071256 14.56 130.8E PCN 6 6 004091 14.56 130.8E PCN 5 0 040032 15.64 130.6E PCN 5 8 001236 16.40 130.5E PCN 5 8 001236 16.40 131.5E PCN 5 8 001236 16.40 131.5E PCN 5 10 004114 14.50 131.5E PCN 5 10 004114 16.50 131.5E PCN 5 10 004114 16.50 131.5E PCN 5 10 004114 16.50 131.7E PCN 5 10 004114 16.50 131.7E PCN 5 11 004115 16.50 131.7E PCN 5 12 004014 16.40 170.7E PCN 5 13 000115 15.74 170.7E PCN 5 14 004115 15.74 170.7E PCN 5 15 004015 15.74 170.7E PCN 5 16 004256 16.40 170.7E PCN 5 17 004255 16.40 120.7E PCN 5 18 004155 16.74 170.7E PCN 5 19 00415 15.74 170.7E PCN 5 19 00415 15.74 170.7E PCN 5 10 00415 15.74 170.7E PCN 5 11 004255 16.40 120.7E PCN 5 12 004014 170.14 170.7E PCN 5 13 00415 170.74 170.7E PCN 5 14 00415 15.74 170.7E PCN 5 15 004035 16.60 120.7E PCN 5 17 004256 17.54 170.7E PCN 5 18 004256 17.54 170.7E PCN 5 18 004256 17.54 170.7E PCN 5 19 004256 170.7E PCN 5 10 004256 17	\$116
3 071254 [4.36.130.HE Pru b DMKD30 DKD37 D	PG[₩
4 072034 14.70 134.8E Pru b 5 040032 134.6E Pru b 6 040314 14.30 134.5E Pru b 7 080934 14.30 137.5E Pru b 8 041234 16.50 131.8E Pru b 9 081234 16.50 131.8E Pru b 10 04134 14.50 131.5E Pru b 11 04135 16.50 131.5E Pru b 12 04014 14.50 131.5E Pru b 13 04015 15.70 120.6E Pru b 14 04015 15.70 120.6E Pru b 15 04015 15.70 120.6E Pru b 16 041256 16.50 120.7E Pru b 17 041256 16.50 120.7E Pru b 18 041256 16.50 120.7E Pru b 19 041256 16.50 120.7E Pru b 17 041256 16.50 120.7E Pru b 18 041256 16.50 120.7E Pru b 19 041256 16.50 120.7E Pru b 19 041256 16.50 120.7E Pru b 10 041256 16.50 120.7E Pru b 11 041256 16.50 120.7E Pru b 12 041256 16.50 120.7E Pru b 13 04135 17.70 120.2E Pru b 14 04135 17.70 120.3E Pru b 15 041350 17.70 120.3E Pru b 16 041256 17.70 120.3E Pru b 17 041356 17.70 120.3E Pru b 18 041356 17.70 120.3E Pru b 19 04136 17.70 120.3E	PGT# PGT#
D 040032 15.44 135.6E PCN D 71.5/1.5 /01.5/24HRC DMCQAT  O 040314 14.54 137.5E PCN D DMCQAT  O 040314 14.54 137.5E PCN D DMCQAT  O 041234 16.44 137.5E PCN D DMCQAT  O 041234 16.44 137.5E PCN D DMCQAT  10 041314 14.44 137.5E PCN D DMCQAT  11 04155 16.0H 130.1E PCN D DMCQAT  12 040014 16.0H 170.1E PCN D DMCQAT  13 040115 15.74 120.6E PCN D T2.5/2.5-/01.0/24HRC DMCQAT  14 040115 15.74 120.4E PCN D T2.0/2.0 DMCQAT  15 041035 16.44 120.7E PCN D T2.0/2.0 DMCQAT  16 04125 16.24 120.4E PCN D DMCQAT  17 041255 16.24 120.4E PCN D DMCQAT  18 04135 16.44 120.3E PCN D DMCQAT  19 04134 17.41 120.3E PCN D DMCQAT  20 04235 17.74 120.3E PCN D DMCQAT  20 04235 17.74 120.3E PCN D DMCQAT  20 04235 17.74 120.3E PCN D DMCQAT  DMCQ	PGT#
6 0 0 0 0 1 1 1 1 2 1 1 2 1 2 1 2 1 2 1 2	PGT#
B 0q1234 16.40 131.5E PCN 5 DMCQ1U 10 0q1314 14.50 131.7E PCN 5 DMCQ1U 11 0q1314 14.50 131.7E PCN 5 DMCQ1U 12 0q1014 16.60 170.7E PCN 3 T2.5/2.5-/01.8/24MKC DMCQ1 DMCQ1 13 0q0115 15.7N 170.7E PCN 3 T2.5/2.5-/01.8/24MKC DMCQ1 DMCQ1 DMCQ1 DMCQ1 DMCQ1 DMCQ1 TMI JS DMCQ1 DM	PG1#
J 081234   A.4 131.5E   PCN 5   DMCDAT   10 081314   A.4 131.5E   PCN 5   DMCDAT   11 082155   A.001 130.1E   PCN 5   DMCDAT   12 08016   A.601 130.1E   PCN 5   PCN 5   DMCDAT   13 080115   15.7N 120.5E   PCN 5   T2.5/2.5-/01.0/24MKK   14 080115   15.7N 120.5E   PCN 5   T2.0/2.0   DMCDAT   15 081255   A.601 120.7E   PCN 5   DMCDAT   16 081255   A.601 120.4E   PCN 5   PCN 5   DMCDAT   17 081255   A.601 120.3E   PCN 5   DMCDAT   18 081350   A.601 120.3E   PCN 5   PCN 5   DMCDAT   19 08134   17.01 120.2E   PCN 5   PCN 5   DMCDAT   20 082154   17.7N 120.3E   PCN 5   DMCDAT   21 10055   17.4N 120.3E   PCN 5   DMCDAT   21 10055   17.4N 120.3E   PCN 5   DMCDAT   21 10055   17.4N 120.2E   PCN 5   DMCDAT   21 10055   17.4N 120.2E   PCN 5   DMCDAT   22 10055   17.4N 120.2E   PCN 5   DMCDAT   23 10055   17.4N 120.2E   PCN 5   DMCDAT   24 10055   17.4N 120.2E   PCN 5   DMCDAT   25 10056   17.4N 120.2E   PCN 5   DMCDAT   26 10056   17.4N 120.2E   PCN 5   DMCDAT   27 10056   17.4N 120.2E   PCN 5   DMCDAT   28 10056   17.4N 120.2E   PCN 5   DMCDAT   28 10056   17.4N 120.2E   PCN 5   DMCDAT   29 10056   17.4N 120.2E   PCN 5   DMCDAT   20 10056   17.4N 120.2E   PCN 5   DMCDAT   20 10056   17.4N 120.2E   PCN 5   20 10056   17.4N 120.2E   PCN 5   DMCDAT   20 10056   17.4	ROUN
10 041314 ja.4 131.7E Pry 5 11 04135 ja.6 131.7E Pry 5 12 04016 ja.6 130.7E Pry 3 13 04016 ja.7 120.6E Pry 3 14 04015 ja.7 120.7E Pry 3 15 04015 ja.7 120.7E Pry 5 15 04035 ja.6 120.8E Pry 5 16 041256 ja.4 120.8E Pry 5 17 041256 ja.4 120.8E Pry 5 18 04135 ja.8 120.8E Pry 5 19 04136 ja.8 120.8E Pry 5 19 04136 ja.8 120.8E Pry 5 19 04136 ja.8 120.8E Pry 5 20 04235 ja.7 120.3E Pry 5 20 04235 ja.7 120.3E Pry 5 21 10055 ja.8 120.3E Pry 5 22 10055 ja.8 120.3E Pry 5 23 10055 ja.8 120.3E Pry 5 24 10055 ja.8 120.3E Pry 5 25 10055 ja.8 120.3E Pry 5 26 04235 ja.8 120.3E Pry 5 27 10055 ja.8 120.3E Pry 5 28 10055 ja.8 120.3E Pry 5 28 10055 ja.8 120.3E Pry 5 29 10055 ja.8 120.3E Pry 5 20 04235 ja.8 120.	PGT#
11 042155   in-in   13n.1E   Prin   120.4E   Prin   120.72   P	RODN PGIW
12 04014 14.0n 170.7E PCN 3 12.5/2.5-/01.0/24MRC DMGDA 13 040115 15.7n 170.7E PCN 3 12.5/2.0 14 040115 15.7n 170.7E PCN 3 12.0/2.0 DMGDA 15 041035 14.0n 170.7E PCN 5 DMGDA 16 041256 14.0n 170.7E PCN 5 DMGDA 17 041256 14.2n 170.7E PCN 5 DMGDA 18 041356 14.0n 170.7E PCN 5 DMGDA 18 041356 14.0n 170.7E PCN 5 DMGDA 19 04136 17.0n 170.7E PCN 5 DMGDA 20 042355 17.7n 170.7E PCN 5 DMGDA 21 100556 17.6n 170.7E PCN 5 DMGDA 22 100556 17.6n 170.7E PCN 5 DMGDA 22 100556 17.6n 170.7E PCN 5 DMGDA 23 100556 17.6n 170.7E PCN 5 DMGDA 24 100556 17.6n 170.7E PCN 5 DMGDA 25 17.7n 170.7E PCN 5 DMGDA 26 17070 170.7E PCN 5 DMGDA 27 100556 17.6n 170.7E PCN 5 DMGDA 28 17070 170.7E PCN 5 DMGDA 29 17070 17070 170.7E PCN 5 DMGDA 20 17070 17070 17070 170.7E PCN 5 DMGDA 20 1707	PGT
13 000115 15.7% 120.6E PCN 3	PGT#
15 001035 14.0m 124.7E Prn h	PGTW
16 091256 14.641 129.4E PCV 5 17 091255 14.24 129.9E PCV 5 18 091255 14.24 129.3E PCV 6 19 092134 17.04 124.2E PCV 6 20 092355 17.74 120.3E PCV 5 20 190355 17.74 120.3E PCV 5 21 17.0556 17.64 120.2E PCV 5 21 17.0556 17.64 120.2E PCV 5 22 17.0556 17.64 120.2E PCV 5 23 18.0556 17.64 120.2E PCV 5 24 18.0556 17.64 120.2E PCV 5 25 18.0576 18.057	RPMK
17 031255 16.20 120.9E PCN 5 0M4036 18 001356 16.60 120.3E PCN 6 72.0/2.5 /W0.5/21HRQ DM4039 19 032134 17.0N 120.2E PCN 6 72.0/2.5 /W0.5/21HRQ DM4037 20 032355 17.0N 120.3E PCN 5 0M4036 21 17.0055 17.60 120.2E PCN 5 0M4030 EUGE JF NATA	PGT# PGT#
18 001350 14.6m 120.3E PCN 0 19 002134 17.6m 120.2E PCN 0 72.6/2.5 /wn.5/21MRR DMCD37 20 002355 17.7m 120.3E PCN 5 21 17.0056 17.6m 120.2E PCN 5 21 17.0056 17.6m 120.2E PCN 5	RPMK
14 092134 17-04 124-2E PC4 6 72-01/2-5 /40-5/21HRQ D4C937 20 092355 17-74 129-3E PC4 5 D4C934 21 174056 17-64 129-2E PC4 5 D4C934 EUGE JF NATA	RPHK
20 002355 17.74 120.3E PCN 5 04444 21 10055 17.44 120.2E PCN 5 04444 EUGE JF NATA	PGTW
	PGT#
22 10 00 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RODN
23 101015 19.74 128.3E PCN 5 000077	PGI# PGI#
24 101238 19.4N 177.5E PCN 5 DMSP74	PGTW
• 25 1n1337 17.5N 127.6E PCN 5 OMSN29	PGT⊎
* 26 101337 17.50 127.6E PCV 5 DMSU36	PGTW
27 1/2113 14.60 124.6E PCN 4 DMCN47 EARSD 4LCC 28 1/2337 14.60 124.5E PCN 3 DMCRDA	PGT#
28 162337 19.5M 128.5E Pcy 3 045P36 29 110218 19.7N 128.4E Pcy 3 71.6/1.0 045P INTI Jd5	PGT# PGTW
30 110218 14.44 124.4E PCN 3 TL.0/1.5 /w1.0/27HRC DMCD79	PGIW
31 110756 1A.AN 12A.2E PC4 5 DNGD71	PĠT#
35 111519 14-4n 150-5E BCA 5 DW2034	PGTW
33 111318 14.74 128.18 PCV 3 DMSD30 34 111318 14.34 128.58 PCV 3 DMSD34	PGTW
34 111318 14.3M 124.5E PCN 3 DMCO34 35 112234 14.4M 127.2E PCN 3 Tl.n/1.0 /50.0/2nMRc DMSH27	RK50 RODN
36 170100 14.34 127.2E PCN 3 DMG046	PGT#
37 176216 17.1N 125.2E PCN 3 DMPD77	PGTW
38 120043 16.40 184.6E PCN 3 T3.0/3.0 DMFD3K INTI J45	RPMK
39 170043 1700 174.65 PCN 3 UPSPYA 40 170140 1407N 124.55 PCN 3 DMSPYA	PGTW
00 171140 14.75 PCV 3 Theorem Omega INIT 245	RPMK PGTW
42 111056 15.3N 121.0E PCN 4 DMCD17	PGT#
43 171324 15.40 127.46 Pry 5 Dwebra	PGTW
44 131352 15.6W 152.3E PCN 3 DMCNAW	RODN
PLACABL FIXE?	
	**************************************
i na2027   15.44   13n.18   7nn4H   2047   11n   32 080   15   1n   3	+13 +12 5
2 082153 15.4N 130.1E 700MD 3044 993 40 330 15 104 37 300 15 5 3	+12 +14 +11 5
3 000928 15.44 120.HE 700HH 3024 990 55 270 10 160 51 070 12 5 4	•14 •15 •11
♦ 091747 17,30 129.2€ 700MH 2004 170 35 090 30 5 5 5 092140 17.40 129.2€ 700MH 2010 50 060 20 140 38 060 30 5 5	*10 *14 *11 7
3 002140 17.60 120.2E 7n0MH 301n	*14 *11 7 *19 *10 9
7 104213 14.50 128.60 700MH 307] 35 140 75 230 30 140 90 4 5	.19 .19 . 8
8 110540 14.44 124.4E 700MH 1465 35 210 30 NAN 30 324 9N 5 10	+15 +11 10
9 110945 14.4M 120.5E 700HH 1079 995 20 180 30 150 17 010 30 5 5	+15 +15 +10 10
10 120015 14.1N 126.4E 1500FT 1003 40 220 30 040 48 010 480 4 5	+24 +25 +24 11
11 1 34.751 14.761 34.751 MM 124 1001 A 10	11
SYNOTTIC FIXES	
FIX TIME FIX INTENSITY NEAREST NO. (7) -OSTITUM ESTIMATE SATA (NM) COMMENTS	

1 070000 9.9% 141.5E

# TROPICAL DEPRESSION 26

	T1ME (7)	F1X P0511104	&CCRY	DV19AK CODE	54	TFII 1TE	COMMENTS	SITE		
*	3n1137 3n2238 010056 010907 011119 011156 012048 012219	11.24 154.6E 15.14 154.5E 14.74 152.6E 20.34 152.0E 20.34 151.0E 20.54 151.0E 22.54 150.6E 22.54 151.6E	PC# 3 PC# 3 PC# 3 PC# 6 PC# 6 PC# 5 PC# 5 PC# 5	T2.0/2.0	.D/24HRC	Duspan Duspan Duspan Duspan Duspan Duspan Duspan Duspan	LL th' ULCC IMII J#S	PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
10	014519	23.34 149.ME 24.34 149.7E	Pry 5 Pry 3			045634 046634	RELUCATED LLCC	PGT# PGT#		
	T1ME (7)	FTK POSTTION	FLT I VL		Max-SFC-Wy		XES LI-LUL-WNN ACCRY EL/BMG/WNN MAV/MFT	EYE FYF ORIEN- SMAPE DIAM/TATION	byf TEMP (C) OUT/ IN/ JP/SST	45M 40•
		23.94 149.8E	7n0=15 7n0=15	1091 SOIL	40 n90		27 200 40 4 4 35 200 20 4 1		+11 +14 + 6	3
					SYND	TIC FIXE	s			
FIA NU.	T1ME (7)	FTX ₽OSTT1UN	INTENST ESTIMAT			co	MMENIS			
1	021500	24.24 152.1E	15	120						

### TYPHOON ABBY

## SATELLITE FIRES

Fla NU.	[1M5 (7)	6.1X (405.11.1%)	ACCRY	SALSAK CODE	SATHILLIE	CJAMENTS	SITE		
• ;	172238	5.50 157.0F	0,· y 5	fl+4/1+5	DHENSA	INII Jas	P61#		
• 2	010407	4.00 1-1-2t	P 4 6		Umen 37		PGT⊯		
	011119	5.7 (111.9E 5.50 (152.2E	PC4 5		ひゃくりょう		PGT#		
,	015514	7. 11 100.2E	Pry 5	13.073.0 /01.5/24HH			PGT# PGT#		
b	029746 921101	7.11 170.7E	Penn		Durn 12		PGTW		
á	021135	5.90 150.4F 5.36 150.5E	Pry n		ひゃくりょり		PGIW		
*	005501	7.40 150.0E	PCV 5		Duchsv		PGTW PGTW		
10	031045	5.7% 150.2E	PC4 "	11.5/7.5 /00.5/26HR			PGT#		
12	0 11117	n.75 150.45	Prun		ひゃくひ しゅ		PGIW		
• 13	031514	SAR ISHABE	Prv b		TTHUSN		PGT⊯ KG≌C		
1+	りょくょくり	3.00 150.4E 3.05 154.5E	Pry 3	T9.074.0 /00.5/24HR	0460 14		PGT⊌		
16	041024	4.3 ISA.1F	Prvh	14-1174.U 7110.5724HR	DACHIN PERDAG		PGT#		
17	041056	1.24 156.0E	PCV 6		Duensa		PGT# PGT#		
• 15	042305 042333	4.64 153.4E	PCN 5	T4-044 0 150 0131444	Dadota Dadota		PGT∎		
ن ج	051147	7.74 152.HE	Prys	T4+0/4.0 /S0-0/24HR	Oncolv		PGTM		
۲,	0-1720	1.34 177.58	PCV 6		Dech in	APRNT WEC INDICATED TO N	PGI# PGI#		
23	051739 052249	7.74 154.7E 4.48 151.1E	PCN D		TTHOSN		KG#C		
24	096317	4.4x 1>1.2F	Pry 5	14.074.0 /SU-0/24HHS	AFG24G PFG24G	34CEL MARN TA SELS UNS	PGT# PGT#		
5.5	071153	4. 3. 150.4E	Prys		DMCDAN	UL UNIN AT 105N 1479E	PGTW		
70	041459	1454 150.5E 10.25 140.0E	Prw h		DARBSA		PGT⊌		
25	070011	10. 10 14m.7E	PCN 5	T3.5/4.0 /w0.5/25HRS	TTHICA AFGPWD		KG#C PG1#		
64	171042	10.04 145.05	Pry 5		DACHIA		PGI		
روف ا ا	071141	11,34 146,3E 10,31 146,2F	PCN T		Decade		PG1d		
32	072352	11.44 144.5E	Pry 5	14.5/1.5 /W1.0/24HRS	Duch se		PG F# PG F#		
وو	040055	11.5% 149.7F	PCN 5	17.5/2.5	Duchia	INII Jas	ROUN		
34 35	001536	11.50 144.3F 12.3: 141.ME	PCN 5		Dado ta		PGTW		
J h	041303	12.19 130.6F	Pry 5		Dadbis	UPR LVL	PGT# RODN		
31	0A1303	12.24 151.ME	Prv 5		PERPAG	01 11 11 11 11 11 11 11 11 11 11 11 11 1	PG f e		
. e e. V E	092334	11.50   140.46   11.40   144.86	PCN 5	13.0/3.0 /00.5/2*HRC			PGTW		
40	021515	10.0:135.48	Prys		Dwen sy Dwen sa		PGTW		
* 1	0.51544	7.94 1.14.46	Pris		Dach sa		PGT⊯ RoDN		
4 ¿	156169	10.00 145.28	PCW S		Dachia		PGTW		
44	100000	11.30 133.58	Prys		11005A		KGMC PGTW		
• >	100125	11.30 133.4F	Prv 5	T4+1/4.0 /111-1/24HRS			PGT#		
4/	101157	17.24 147.6E 17.24 147.5E	PCN 5		DHZD 14		PGT#		
44	101224	12.44 132.35	PCN 5		Decase		RODY		
47	1 11 426	14.90 131.3F	Pry 4		TTHOSH		PGT∉ KG₩C		
50 51	110039	14.44 140.68	PCN 5	** *	DMCDSW		PGIW		
Šż	110105	Li. w Lin. 4E	PCV 4	T0.5/4.5	Duch sa Duch sa	INII Jas	RPMK DC Tw		
53	111320	14.24 13n.4E	PCN I		Direct to		PGTW PGTW		
54	111345	15.18 130.4E 15.28 140.3E	PCY /	T7.0/5.0	Deceda		PGIW		
56	120021	15.38 130.75	PCN I	1	Datesia	INII 748	RODN PGT #		
57 58	120046	15.50 130.08	Pry	T3+0/5.0 /50.0/23HHE			PGTW		
24	120221	19.54 130.48 16.74 130.48	Pry 1	13+0/5.0 /10.4/24HKC	Dado ta Dado to		RPMK		
עם	120700	17.30 130.2E	PCV 2		116024		RPMK KG#C		
95	121307	14.29 132.4E	PCY 1		Deco se		PGTW		
63	121327	19.44 132.1E	Pry 3		Dach 14 Dach 14		RPMK		
0.	120003	1 2.9M 1 44.7E	PCN 3	14.5/5.0 /HO.5/24HKS			PGT# PGT#		
65 66	6020E	21.14 134.3E 21.14 134.2E	PCM I		Dechid		PGT#		
6/	141244	21.40 144.55	PCN 5	14.0/5.0 /41.0/SAHHS	Dade se Dade sa		RODN		
0.5	171305	21.45 [34.5E	PCY 5		Duco to		PGTW PGTW		
64 70	141705	21.40 140.26 21.40 140.46	Pru 5		Dachia		ROOM		
/1	136345	22.00 142.5E	Prv 1	T4.0/4.0 /50.0/22HRS	AF 924()		KGWC		
12	132345	27.1 + 142.18	Pry 5	7 10 10 10 10 10 10 10 10 10 10 10 10 10	DAZATA		ROUN PGT #		
/ 3	1 4 4 0 0 7	22.1" 142.5E	PCVS	14.0/4.5 /W0.5/24HRS	OMCBSA		PGTW		
				Α'	TRCDAFT FT	xE5			
	•								
	1 (7)	5 1 X 20 S 1 T [199	FLT	TOUTH OHS MAX-SEC-1	140 441-F	T-LVL-END ACCOY EYE	FYE ORIEN-	RYF TEMP (E)	WSN
	• •			~ moth A≜F\MMR\	- 40 OF #/VI	EL/BRG/ANG NAV/MET SMAPE	POTTATION	UNTY THE SPIRET	40.
1	012215	4.9H 160.4E	70046	***					
į	010250	N. 341 150.1E	70040	796 45 050 7075 50 050		36 UZU 50 1 5 99 JOU 12 2 5		.52 .52 .53	į
3	0.10.350	6.50 150.2E	7 n 0 mm	App 490k	1.40	34 360 24 1 4		. 4 .11	3
•	011305	5.50   50.0E 7.80   50.4E	700MH 700MH	1049 295 1050 292 55 030	1 40	38 110 Su > >	7	·10 ·14	ŝ
5	040104	4.24 150.2E	70046	1050 392 55 030 1050 394 50 010		10 0/U 6n 5 5 11 34U 9n 5 5		. 4 .14 +10	•
1	040718	4.14 156.4E	7ngmm	1019 987 50 140	10 360 9	50 270 54 A A		· # · 14 · 10	•
	050157 050740	4.24   144.4E 7.54   147.4E	7004H	386 90 270 3101		3 330 20 2 5		·1+ ·18 ·10	6
lu	051 100	7.74 157.48	7 numm	7084		53 330 60 3 9 59 050 15 4 3		14 -13 -15	,
11	051021	1.14 152.56	7 nomm	1070 1001	150 6	30 350 6n 7 4		13 . 9	,
12	052150	H. 74 151.4E	7 n 0 mm	3134 1000 50 non	10 070	15 314 50 2 4		.18 .14 . 6	н

1.	060051	H. RV 151.4E	7n0MH	3135		35	170	35	494	41	360	90	2	3					
14	040215	1.04 151.7E	7 n 0 MH	3123	1002	30	250	30	120	41	360	90	-	4			+14 +14	• 7	ь
1:	040935	1.4N 151.9E	700MB	1094	1000	4.0	790	30	050	47	240	150	10	4			+10 +13		¥
16	061205	3. 34 140.7E	700MH	1099	• • • •				136	10	240	30	-				•13		ý
• 17	961402	9.44 140.4E	70040	3099	1002				260		160		5	20			*14 *11		į.
• 16	062030	9.44 146.1E	700MH	3080		25	150	25	090	51	350	120		5				••	10
15	064127	10.00 146.AE	700MH		995		050	25	140		050	22		20			.25 .25	22 27	10
. 20	071503	10.24 144.7E	710MH	1059	396			-	230	30	150	20	5	5			+12 +13		12
ž į		10.7N 144.HE	700MH	1051					140	33	090	90	5	,			+15		12
22	074128	11.1N 144.8E	7nomH	3062	996	35	020	50	150	4.3	040	Ř0		5			+14 +15		12
23		12.24 143.6E	700MH	3084			020	30	110		020	35	6	-			******	• • •	13
24	090958	11.9v 142.4E	710MB	3092					180	27	100	410	10	5			+14 +13	- 10	13
25	091938	11.3N 139.7E	70048	3045					150		0/0		ĩ٩	10			+13		14
26	082126	11.6V 139.9E	700MH	1084		25	230	15	140		070	60		4			115		1.
27	090617	11.24 137.6E	Thomas	3064			300	10	100	39		40	•	_			+15		15
21	090812	10.54 136.3E	7ngmm	2992	988		360	5	110		360	10	9	5	CIRCHLAR	15	4 4 1 5		15
27	091934	11.9N 134.4E	700MB	2425	,	•		-	OMB		330	30	5	5		••	•15		16
30	092207	11.1N 134.7E	700MH	2935		6.0	190	25	150		090	30	5	3			*1.5	•	16
31		13.5N 130.4E	7ngmH	2747	964		120	35	179		120	35		5			+14 +21		18
36	110554	14.34 13n.2E	700MH	2792	,,,	75		10	310		210	61	4	5			٠ ذ ١٠		19
3.3	110927	14.44 130.1E	70048	2174	963		030	13	250		140	76	4	5			+15 -15		19
34		15.9v 13r.3E	700MB	2682	954		110	30		105		30	5	Š			. 14 . 19		20
3:	122105	14.4N 133.HE	7n0MH	2681	,,,,	-00				84		15		3				••	25
36		14.5N 134.0E	TOOMB	2669	951	20	310	30		106		30	5	•				-14	25
37		20.7N 136.8E	700MH	2762	962		180	20		118		25	4	7	CIRCULAR	30	+13 +19		23
3 8		22.14 141.4E	700MH	2934	766	-10	,	- •	180		060	30	5		J = J() E =	•	+17		24
3,		22.20 142.0E	70048	1002		20	₹50	50	230		080	30		10			+ + 17		24
4.1		23 74 146 46			1001									, ,,			+ +17		- (7

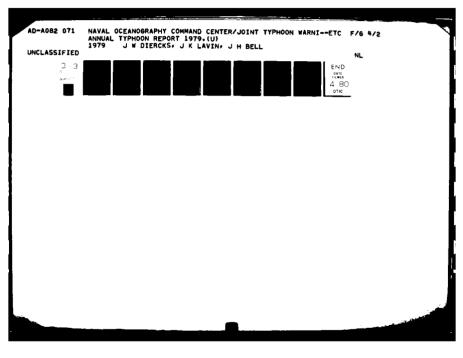
## SYMPOTIC FIRES

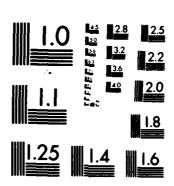
FIX NO.	TTME (7)	0021110m	INTENSITY ESTIMATE	NEAREST Data (NM)	COMMENIS
ı Ç	290000	7.04 164.0E 7.04 164.5E	15 15	100	
	141500	21.0x 148.0E	20	200	

## TROPICAL STORM BEN

## SATELLITE FIXES

	TTME (7)	FIX POSTTION	ACCRY	DVna.	AK COO	€		SATFI	LTTE		c	и зирс	rs			SITE				
1	260134	11.74 132.0E	PCN 5					Ous	of u							PGTw				
•	201217	11.74 130.9E	PCN 5						454							PGTW				
3	210059	11.5% 127.0E	PCN 3	T2.0/	2.0-				AFG	IN	1 1	Jes				PGTW				
•	210114	11.54 124.9E	Prv s						PFU	•	•					PGT#				
>	210114	11.54 126.7E	PCN D	12.0/	2.0			Dws	464	IN	111	JdS				RPMK				
6	211340	11.74 123.8E	PCN 5					D**	AFG							RODN				
7	211355	11.64 123.ME	PCN 5					Dws	PRO							PGTW				
4	211355	11.54 123.7E	PON 5					Dws	10.10							RPMK				
+	211356	11.54 123.HE	PON 5						1 P 3 4							RODN				
10	2>00+1	12.4N 121.4E	PC4 5		3.5-/1	11.5/6	4HRS		4605							₽GŤ∎				
11	220236	30.151 MI.FE	Pry 5	73.5/					6F45	1	110	JdS				RODN				
15	220237	12.54 120.9E	PC# 5	T3.0/	7.0 /n	1.0/2	SHRS		1030							RPMK				
13		13.6N 119.4E	PC4 h						1024							KGMC				
14		13.9N 119.1E	PCN 5						MEG							PGTW				
Гэ	521336	13.4H 119.PE	PCN 5						1010							PGTW				
10	530053	15.94 110.3E	PCN	12.5/	3.5 /₩	1.0/0	* HH C		1934							PGTW				
17		15.74 119.6F	PCN						46.45							RODN				
18	230217	16.34 L10.7E	PONT						1014							PGTW				
19	210217	15.54 110.3E	Pry 5	16.5/	3.0 /w	0.5/0	AHRC		5(1 <i>6</i> M							RPMK				
51	231304	19.00 121.3E	PCN D						50 3A							KGWC PGTW				
		30.04 127.95							1010											
2.0	231317	20.0N 124.1E	Pry 5					0								PGT₩				
							٨	1350	AFT P	1×E5	•									
	T1ME (7)	F1X P05111794	F C T I, VL	70043 461	ORS MSLP							-4ND			EYE SH4PE	-WEIRG BYB WOITAT\WAIG				45N 40.
1	210520	11.5% 125.HE	7 n 0 M B	3047	992	50	ი 30	÷0	100	40	3 2 0	60		5			•11	+11		1
2	212225	12.54 122.3E	7n0MB				360	10	210	38	120	60	3	•						5
	220313	13.4N 119.ME	7n048	3013	996		350	10	l >u	72	000	15	- 1	3			•13			•
•	22239	15.5N 119.4E	7 n 0 MH	3052	995	70	020	12	170	56	040	15	7	,	CIRCHLAR	25	+14 *	• 9		6
							0	A JAN	Fjre	s										
	TIME	Fix			EYF		EYF		Anne								FACAH		SITE	
NO.	(7)	40511170	HADAR A	*C~4Y	SHAP	·Ε	DIA	<b>4</b>	PCAVH	TOU	FF				COMMENTS		POSTTION		40 40.	•
i	210710	12.0M 1/5.2E	LAND						1857/	111	"						10.3m 124.0	OE :	98546	
2	210340	12.04 124.26	CHAJ						4510								10.3N 124.0		98546	
3	2:110#	12.04 124.2E	LAND					1	2013	527	14						10.3% 124.0		98546	
	511500	11.74 127.45	LAND						0340								10.3N 124.0		98546	
2	211300	11.9N 123.4E	(GI/A)						ママンり	526	50						10.3₩ 124.0		98546	
6	220700	13.5" 110.4E		FAIR	CIRCU		,	A									15.24 123.6		98327	
,	521300	15.24 119.4E	LAND		Claci	LAR											15.24 120.0	6E (	98327	





MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

# 2. NORTH INDIAN OCEAN CYCLONE FIX DATA

TC 17-79

## SATELLITY FERES

FIA	TIME	FTX					
NO.	(7)	P0111504	acr qy	DAUSAN CODE	SATFI I TE	COMMENTS	SITE
	052354	4.5N 89.7	E PCH N	T1-0/1-0	044917	CHTH #45FD ON HER LYL BUTFLOW	Kenc
2	041240	7.74 87.6	E PON 6	T1-0/1-0	045937	POSIT MAKED HOW LVL ANTICYCLONE	KOWC
وَ	041705	9.5N BR.5	E PCN 6	71-0/1-0	045735	[NIT 365	KBdC
•	074121	7.44 BR.4	E PCH H	T1.0/1.0	045937		KOMC
	070549	4.94 H7.8	E PCH 6	72-5/2-5 /01-5/38HR	E DWSP		KOWC
. i	071220	NOON HAUM	E PCH 6		Dug# 17	EDGE OF NATA MISST BASED CURV	KOUC
7	071647	7.04 MA.7	E PCN 6		044914		Kewc
i i	080100	5.44 86.1	E PCN 4	73-0/3-0 /D0-5/19HR	1 DWSP17	APPRINT LOW LVL CIRC	Keuc
9	044528	5.74 MA.3		T0.9/4.0 /D1.5/Z4HR	C DMSP35		KOVC
10	041341	6-14 B6-4			Dusp 17	STORM UN EAST FORE OF PICTURE	Kedc
11	081510	7.24 HA.T			OMSP		KOUC
ĬŽ	004840	7.74 86.3			Dugpay	EVE COMEMED AV THIN CI CANDOV	KOUC
ĬĬ	000540	7.94 57.5			TROSN	EYE ULSTONTED	FJDs
14	091321	4.7M 44.0		T3-5/4-0-/HG-5/Z4HR	045937	CTR BASER ON CH BANDS	KONC
Ìŝ	091751	10.7N H5.5			DHSP	EYE RAMAFD	KOUC
16	100921	10.74 84.6			045937		KOUC
17	100451	11.64 84.5		T5.0/5.0 /01.0/24HR		EYE EMMENDED	KOUC
is	101302	12.14 #3.6		1000/300 ///200/00/	Dues	SOOU EYE SOON OT OUTFLOW	KOUC
19	101734	12.4W H3.4			Duse	EYE WELL DEFINED	KOWC
+ 20	104115	13.04 H7.2			TIBOSN	EVE WELL DEFINFO EST. DIS	FJDS
+ 51	102124	9.6N H4.3			TTHOSY	EYE NOT VSGL	FJDG
55	110001	12.54 A2.5		75.0/5.0 /Dl.s/24HR		EYE DY ENGE OF DATA	KOUC
53	110142	12.74 81.3		10-07 300 7.750 37.00	D#SP37	EYE WELL DEFINED	Kewc
24	110615	13.34 82.7		T6-0/6-0 /D1-0/26HR		EYE WELL DEFINED AND EMBEDDED	KOWE
Žš	111001	14.3N B0.5		100071100 701007100.00	TIROSH	EYE HELL DEFINED	FJDS
26	111241	14.14 RZ.0		T0.0/6.0 /D1.0/24HR		EYE NOT USEL MIE TO CI CAMOPY	KOWC
27	111715	13.94 81.2		1000,450 ,41100,504	Dusp	W EDGE OF DATA CI CAP OVER EVE	Xewc
28	120122	14.34 #1.0			Duse 17	CDO MORE DYAL	KOUC
29	120356	14.7M 80.8			Dusp 15	EVE NOT USBL MOOD CI OUTFLOW	KeMC
• 30	121135	15.5W 78.9			TIMOSA	EYE DEFINABLE FST. DTG	7,06
31	121405	16.2N 79.1			Dws#37	EYE HOP WELL	KOWC
32	120105	15.94 7A.A			045937	UPR LUL ANTICYCLONE	Kerc
33	110538	14.0N 77.4		T3.0/4.0-/WZ.0/Z4MR		A. v. and and Dividence	KOWC
,,,	. 14370	47404 7767		1			

## TC 18-79

### SATELLITE PEXES

FIX	TIME	FIX					
NO.	(7)	POSTTION	TCCSA	DAOSUK CODE	SATFLLTTE	COMMENTS	SITE
,	170645	18.6w 69.2E	PCN 6	71-0/1-0	D44914	INIT DOS/ANTICYCLONE ALOFE	KOME
• ż	171349	19.7N 71.1E			DeSP37	and ought and the same magnet	conc
3	171927	17.64 66.0E			DWSP35		2000 2003
•	100230	18.24 65.0E			044017	UPR LUL ANTICYCLONE CI OUTFLOW	KOMC
5	140627	17.74 64.2E		TZ-0/2.0 /D1.0/24MR			Kewc
	101100	18.14 68.0E			TIROSH		KNSS
ĩ	101511	18.2N 62.9E			045237		COUC
i	101909	14.5N 67.6E			045935	POSIT GARED ON EXTRAP	KONC
9	100000	18.04 59.9E	:		TIROSH		ICHOS
10	146510	18.84 68.7E			Duspyt		Kenc
11	140608	19.2N 60.18	PC4 5	12.5/2.5 /D0.5/24HR	2 000035		KOUC
12	190750	19.3N 59.3E	PCN 5		Dugpas	ON EDGE OF DATA	KOUC
• 13	191139	14.74 57.0E			TIMOGN		KNOS
14	191450	19.04 59.5E	PCN 5	T2-5/2-5 /D8-5/24HR	1 0HRP17	BASED ON EXPORED LLC	KOUC
15	191950	19.1N 59.7E	PC4 6	- · · · · - · · · · · · · · · · · · · ·	Drithid	POSIT MARED ON EXTRAP	Kenc
10	142300	19.00 5A.00			Trange		<b>1008</b>
17	200150	19.1N 57.00	PCH 6	72-0/2.5 /WO.5/24MR	t 049277		KOUC
18	200731	19.3N 54.0E			Duse 14		Kenc
• 19	201430	21.44 54.9E			04SP37	POSIT GAGED ON EXTRAP	KOWC
• 20	218419	10.44 57.15	Prw 5	71.8/2.8 /H1.8/27MB	1 0wees7		KANC

## SYMPOTIC FIRES

F1		TIME (7)	F11 P0511		INTENSITY ESTIMATE	VEAREST DATA (MH)	COMMENTS
	1	171200	17.50	67.0E	30	40	
	Ž	171800	19.0N	65.5€	30	20	
•	3	190608	19.04	59.0E	45	60	
	٠	191200	19.04	40.0E	35	80	
•	5	211900		56.5E	19	200	

### TC 22-79

## SATELL TIF FERES

F14		T (#E- (7)			DAUSAK COUE	SATFI I ITE	COMMENTS	SITE
	1	211200	A.Sn 84	. OE		TIRNS		KNSS
	ž	211340		SAE PCH	•	Dusp 17	INII 345	Kewic
	3	211602		SE PCH		Dwgp 34	20C 11N1	KOUC
٠	ĕ	2>0039		P.ZE PCH		Dug# 17	* * *	Kenc
	Š	2>0100		1.1E		TTROSN		KNSS
-	ī	2>0443		LOE PCH	<b>.</b>	Duceso		KBCC
	7	2>1320			11.5/1.5	044917	INI Jes	KOUC
		2>1543		PAR PON		Ouspan	INII DOS	KOUC
	- 1	210413		SE PCH		DMEPAA	INIT DOS/PSN MARED ON CONV	KOUC
	10	\$40454		.3E PCH			PSH BASEN ON CENTER OF CONV	KOUE

## SYMBOTIC FIRES

11ME (7)	POSTTI	04	INTENDITY ESTIMATE	MEAREST DATA (NM)	COMMENTS
501500 500000	9.8v 10.8v		50 50	25¢ 200	

### TC 23-79

## SATELL TOP PEXES

	F1X 40.	TIME: (7)	#11 POS1710	m,	ACCRY	DADSWK COOE	SATFLI TTE	COMMENTS	3116
	1	140559	12.44 7	38.1	Pc4 5	71-9/1-0	D= <p39< td=""><td>INII DOS/CENTFO BASED ON LLCC</td><td>KOWC</td></p39<>	INII DOS/CENTFO BASED ON LLCC	KOWC
	Ž	181441		0.1E	PCH 6		Duge 17		KOUC
	Ĭ	199140		0.4E	PCN 5	TZ.8/2.8 /D1.8/24HR	4 O44P37		KOWC
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## **APPENDIX**

i. conti	PACTIONS		
		ICMO	International Civil Aviation Organisation
ACEN	Aircraft Control and Warning System	IR	Infrared
ACCRY	Accuracy	KM	Kilometer(s)
ACFT	Aircraft	KT	Knot (s)
AIREP	Aircraft Weather Report(s) (Commerical and Military)	TTCC	Low Level Circulation Center
ANT	Antenna	LVL	Level
APT	Automatic Picture Transmission	M	Meter(s)
ARWO	Aerial Reconnaissance Weather	M/SEC	Meters per Second
AMO	Officer	MAX	Maximum
ATT	Attenuation	MB	Millibar(s)
AVG	Average	MET	Meteorological
AWN	Automated Weather Network	MIN	Minimum
BRG	Bearing	MOHATT	Modified Hatrack
CDO	Central Dense Overcast	msn	Mission
CI	Current Intensity	NAV	Navigational
CLD	Cloud	NAVPGSCOL	Naval Postgraduate School
CLSD	Closed	NEDN	Naval Environmental Data Network
CNTR	Center	NEDS	Naval Environmental Display Station
CONF	Confidence (number)	NEPRF	Naval Environmental Prediction
CPA	Closest Point of Approach		Research Facility
DEG	Degree (s)	NESS	National Environmental Satellite Service
DIAM	Diameter	NET	Near Equatorial Trough
DIR	Direction	NM	Nautical Mile(s)
DMSP	Defense Meteorological Satellite Program	NOAA	National Oceanic and Atmospheric Administration
EASTPAC	Eastern Pacific	NRL	Naval Research Laboratory
ELEV	Elevation	NTCC	Naval Telecommunications Center
FLT	Flight	OBS	Observation(s)
GOES	Geostationary Operational Environmental Satellite	PCN	Position Code Number
HATRACK	Hurricane and Typhoon Tracking (numerical forecast)	PE	Primitive Equation
нст	Height	PSBL	Possible
HPAC	Mean of XTRP and Climatology	PTLY	Partly
HU	Hurricane	QUAD	Quadrant
HR HR	Hour (s)	RADOB	Radar Observation
nk.	House (4)	RECON	Reconnaissance

RNG Range RPD Rapid SAT Satellite SFC Surface SLP (MSLP) Sea Level Pressure (Minimum Sea Level Pressure) Synchronous Meteorological SMS Satellite SPOL Spiral Overlay SRP Selective Reconnaissance Program STNRY Stationary SST Sea Surface Temperature ST Super Typhoon TC Tropical Cyclone TCARC Tropical Cyclone Aircraft Reconnaissance Coordinator TCM Tropical Cyclone Model TD Tropical Depression TIROS Television Infrared Observation Satellite TS Tropical Storm TY Typhoon Tropical Upper Tropospheric Trough (Sadler, 1976) TUTT VEL. Velocity VIS Visual VSBI. Visible WESTPAC Western Pacific WMO World Meteorological Organization WND Wind

### 2. DEFINITIONS

WRS

XTRE

BEST TRACK - A subjectively smoothed path, versus a precise and very erratic fix-to-fix path, used to represent tropical cyclone movement.

Extrapolation

Weather Reconnaissance Squadron

Zulu Time (Greenwich mean time)

CENTER - The axis or pivot of a tropical cyclone. Usually determined by wind, temperature or pressure distribution.

CYCLONE - A closed atmospheric circulation rotating about an area of low pressure (counterclockwise in the northern hemisphere)

EPHEMERIS - Position of a body (satellite) in space as a function of time. When no geographical reference is available for gridding satellite imagery, then only ephemeris gridding is possible which is solely based on the theoretical satellite position and is susceptible to errors from satellite pitch, orbit eccentricity and the nonspherical earth.

EXPLOSIVE DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 2.5 mb/hr for 12 hrs or 5.0 mb/hr for 6 hrs (ATR 1971).

EXTRATROPICAL - A term used in warnings and tropical summaries to indicate that a cyclone has lost its "tropical" characteristics. The term implies both poleward displacement from the tropics and the conversion of the cyclone's primary energy sources from release of latent heat of condensation to baroclinic processes. The term carries no implications as to strength or size.

EYE - "EYE" is used to describe the central area of a tropical cyclone when it is more than half surrounded by wall cloud.

FUJIWHARA EFFECT - An interaction in which tropical cyclones within about 700 nm of each other begin to rotate cyclonically about one another. When intense tropical cyclones are within about 400 nm of each other, they may also begin to move closer to each other.

MAXIMUM SUSTAINED WIND - Maximum surface wind speed averaged over a 1-minute period of time. Peak gusts over water average 20 to 25 percent higher than sustained wind.

RAPID DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 1.25 mb/hr for 24 hrs (ATR 1971).

RECURVATURE - The turning of a tropical cyclone from an initial path toward the west of northwest to the north then northeast.

SIGNIFICANT TROPICAL CYCLONE - A tropical cyclone becomes "significant" with the issuance of the first numbered warning by the responsible warning agency.

SUPER TYPHOON/HURRICANE - A typhoon/hurricane in which the maximum sustained surface wind (1-minute mean) is 130 kt or greater.

TROPICAL CYCLONE - A nonfrontal low pressure system of synoptic scale developing over tropical or subtropical waters and having a definite organized circulation.

TROPICAL CYCLONE AIRCRAFT RECONNAISSANCE COORDINATOR - A CINCPACAF representative designated to levy tropical cyclone aircraft weather reconnaissance requirements on reconnaissance units within a designated area of the PACOM and to function as coordinator between CINCPACAF, aircraft weather reconnaissance units, and the appropriate typhoon/hurricane warning center.

TROPICAL DEPRESSION - A tropical cyclone in which the maximum sustained surface wind (1-minute mean) is 33 kt or less.

TROPICAL DISTURBANCE - A discrete system of apparently organized convection--generally 100 to 300 miles in diameter--originating in the tropics or subtropics, having a non-frontal migratory character, and having maintained its identity for 24 hours or more. It may or may not be associated with a detectable perturbation of the wind field. As such, it is the basic generic designation which, in successive stages of intensification, may be classified as a tropical depression, tropical storm or typhoon (hurricane).

TROPICAL STORM - A tropical cyclone with maximum sustained surface winds (1-minute mean) in the range of 34 to 63 kt, inclusive.

TROPICAL UPPER TROPOSPHERIC TROUGH (TUTT)

- "A dominant climatological system, and a
daily synoptic feature, of the summer season
over the tropical North Atlantic, North
Pacific and South Pacific Oceans," from
Sadler, James C., Feb. 1976: Tropical
Cyclone Initiation by the Tropical Upper
Tropospheric Trough. (NAVENVPREDRSCHFAC
Technical Paper No. 2-76)

TYPHOON/HURRICANE - A tropical cyclone in which the maximum sustained surface wind (1-minute mean) is 64 kt or greater. West of 180 degrees longitude they are called typhoons and east of 180 degrees they are called hurricanes. Foreign governments use these or other terms for tropical cyclones and may apply different intensity criteria.

WALL CLOUD - An organized band of cumuliform clouds immediately surrounding the central area of a tropical cyclone. The wall cloud may entirely enclose the eye or only partially surround the center.

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